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Comparing Computer Experiments for Fitting High-Order Polynomial Metamodels

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Comparing Computer Experiments for Fitting High-Order Polynomial Metamodels

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The use of simulation as a modeling and analysis tool is wide spread. Simulation is an enabling tool for experimenting virtually on a validated computer environment. Often the underlying function for a computer experiment result has too much curvature to be adequately modeled by a low-order polynomial. In such cases, finding an appropriate experimental design is not easy. We evaluate several computer experiments assuming the modeler is interested in fitting a high-order polynomial to the response data considering both optimal and space-filling designs. We also introduce a new class of hybrid designs that can be used for deterministic or stochastic simulation models.

Key Words: Optimal Design; Response Surface; Space-Filling Design.

Computer simulation models are often used in place of or in conjunction with physical experi-

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ments. Simulation is an extraordinarily powerful tool that allows the study of a system virtually. If the computer-simulation model is a valid representation of the real system, the experimentation and analysis with the model can lead to results and conclusions that are valid for the real system. It is as desirable to experiment with computer simulation models as it is to experiment with physical systems. This requires the choice of an experimental design and analysis technique. The issues associated with the creation of design and analysis of computer experiments are sometimes different than those encountered in the physical domain.

Usually computer simulation models have no stochastic component so the result for any particular set of conditions is deterministic. Examples of deterministic computer-simulation models include

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finite-element analysis (FEA) models and circuitsimulation (or SPICE) models. Experimental designs intended for use on a deterministic model are often associated with several desirable properties that are not encountered in traditional design of experiments literature. First, the design should span or fill a large portion of the design region. Filling the design region is important because little is known about what portions of the region will provide the most informative or interesting results. Also, responses from computer experiments can be complex, and space-filling designs are robust in the sense that they allow a variety of models to be fit. Second, if factors are deemed insignificant or removed from the model, the resultant projected design should span or fill a large portion of the lower dimension design region. In physical experimentation or stochastic simulation, when factors are removed from the model after they are found to provide no contribution to the response, the projected design frequently results in replicated design points. For example, a 23 factorial design projected into two factors results in a replicated 2^2 design. In a computer simulation, this projection of the factorial design would result in a loss of half of the information because replicated points provide no new information in a deterministic setting. These properties have driven new research on experimental design for computer simulation. Designs that aim to fulfill these properties are called space-filling designs.

Computer experiments can be computationally expensive in terms of time required to run a single simulation—a single input. Therefore, surrogate models are used to mimic the input-output relationship in the form of a simpler mathematical expression that can be quickly computed. Surrogate models encompass a broad range of techniques ranging from parametric to nonparametric analysis. As previously stated, the response surface in a deterministic model can be very complex. Determining which modelfitting technique to use is dependent on several factors, such as the problem, the goal of the model, and the knowledge of the analyst. The use of high-order polynomials is only one of many techniques available as a surrogate modeling choice. Polynomial regression models of order two are commonly encountered; however, models of order greater than two can also be found in the literature. Allen et al. (2003) use secondorder response models to fit test functions that mimic computer-simulation models. Fang et al. discuss the application of polynomial regression as a surrogate modeling technique. In Danehy et al. (2002) and Tedder et al. (2007), second- through sixth-order polynomials are used to fit flow-field data (such as temperature) from a combustion experiment. This paper presents a comparison of experimental designs for computer-simulation models when the expected form of the surrogate model is a high-order polynomial. Note that the sample size requirements for polynomials become large as the order of polynomial increases and the dimension of the design increases. In some cases, these sample sizes may not be feasible for extremely computationally intensive simulations.

We compare experimental designs based on their prediction variance with respect to the polynomial model. The results drive the motivation for a new class of hybrid designs that are a combination of space-filling and optimal designs.

Next a literature review of design comparison for computer simulations is presented, followed by a discussion of the method that will be used to compare the designs in this paper. The designs that will be compared are then presented, followed by the results, the introduction to a new class of hybrid designs, a case study that evaluates robustness of the design and model-selection criterion, and finally conclusions and future work.

Literature Review

Three articles that evaluate experimental designs for computer simulations are reviewed. Allen et al. (2003) compares combinations of experimental design classes with respect to second-order response surfaces and Kriging modeling methods. They find that there was inconclusive evidence as to which modeling method performed the best, due to the dependency on the experimental design used. They also observed that unavoidable bias errors constituted a large source of prediction error in regression modeling and estimation errors dominated prediction errors in Kriging modeling.

Hussain et al. (2002) present seven two-dimensional functions that were used to test two metamodels. The metamodels tested were a radial basis function, which was originally developed to fit irregular topographic contours of geographical data, and quadratic polynomial models. Factorial designs and Latin hypercube designs (LHDs) were used as the experimental designs. The paper concludes that the factorial design had the best performance with respect to the polynomial surfaces and the LHD has the best performance with respect to the radial-basis functions. Also, the radial-basis functions were shown

to have better performance (in terms of model fit to the response surfaces generated by the test function and prediction capabilities) than the polynomial models.

Bursztyn and Steinberg (2004) develop a new method of design comparison based on a Bayesian interpretation of an alias matrix. They use this new alias sum-of-squares design-comparison method and three other comparison methods—entropy criterion, minimum-distance criterion, and integrated meansquare error (IMSE) criterion—to compare designs for computer simulations. In the paper, the comparisons are motivated by random field-regression models and low-degree polynomial approximations with some terms considered as bias. They compared Latin Hypercube designs, U-designs, lattice designs, rotation designs, and fractional factorial designs. The results demonstrate that the new alias sum-of-squares criteria developed in the paper tends to favor the rotational designs. The fractional factorial designs perform best in terms of the entropy and minimumdistance criteria. While this makes sense mathematically, the authors point out that these designs may not be the best choices due to their lack of good coverage and tendency to replicate points when projected. The IMSE criteria favored the space-filling designs with the best particular covariance model and demonstrated consistently low performance for the two-level fractional factorial designs.

None of the three papers investigates higher than second-order-polynomial terms. This paper evaluates experimental designs based on their prediction performance for second-order- through fifth-order-polynomial models. The next section presents a discussion of the comparison method used in this paper followed by a section containing the designs that will be used for the comparison.

Evaluation of Designs

The prediction variance is a standard criterion for comparing designs when modeling physical systems with a stochastic component. The scaled prediction variance (SPV) normalizes the prediction variance over the design region and is computed as

$$\frac{NV[\hat{y}(x_0)]}{\sigma^2} = Nx_0'(\mathbf{X}'\mathbf{X})^{-1}x_0, \tag{1}$$

where X is the model matrix and x_0 is the point being evaluated. Zahran et al. (2003) introduce fraction of design space (FDS) plots that graph the empirical distribution function of SPV over the design region.

FDS plots are used in the assessment of prediction capability for response surface designs. This is done by generating a large number of design points in the region and evaluating their scaled prediction variance based on Equation (1). These values are then sorted and plotted versus their order expressed as a proportion. Tables containing percentiles based on the scaled prediction variance over the regions and fraction of design (FDS) plots are used as methods for comparing designs for computer experiments where the expected response is a high-order polynomial.

Because deterministic computer experiments have no stochastic component, it is necessary to justify the use of scaled-prediction variance as a performance criterion. Suppose that a given computer experiment is adequately modeled using a polynomial fit. The difference between the observed and fitted values in a deterministic computer model, however, is not stochastic error, it is model bias. If the polynomial model adequately describes the response surface of the true underlying function, the model bias of the β s is negligible. The model bias of an individual prediction is also fairly small because the fit is adequate. Assume that the source of this bias is due to multiple high-order terms. Thus, deviations between the observed and predicted values will behave like the sum of a number of independent small quantities. Appealing to the central limit theorem, as the number of these quantities get large, these deviations will converge to the normal distribution. We then justify the prediction variance criterion as a measure of the sum of a large number of small biases.

Designs Used for Comparison

Numerous space-filling designs have been proposed in the last 30 years. We investigated sphere-packing, Latin-hypercube, uniform, and maximum-entropy designs. We compared the prediction performance of the space-filling designs to the *I*-optimal and *D*-optimal designs. These designs have low prediction variance with respect to polynomial models. The *I*-optimal designs minimize the average variance of prediction over the design region. While they do not satisfy desirable properties of computer simulation experiments—for example, projections of these designs result in replicate points—they can act as a baseline for good performance in terms of the prediction variance criterion. A description of the designs used follows.

The sphere-packing design, also known as the maximin design, maximizes the minimum distance

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between pairs of design points. This design was developed in Johnson et al. (1990). The maximin design maximizes the minimum intersite distance and is specified by

$$\max_{D} \min_{u,v \in D} d(u,v) = \min_{u,v \in D_0} d(u,v),$$
 (2)

where d(u, v) is a distance that is greater than or equal to zero and D represents the design points. Examples of applications of the maximin designs can be found in Jank and Shmueli (2007), Liefvendahl and Stocki (2006), Chen et al. (2006), Roux et al. (2006), and Bursztyn and Steinberg (2006).

The Latin-hypercube design was developed by McKay et al. (1979). The Latin-hypercube design is defined in Fang et al. (2006) as, "A Latin Hypercube design (LHD) with n runs and s input variables, denoted by LHD(n, S), is an $n \times s$ matrix, in which each column is a random permutation of $\{1, 2, \ldots, n\}$." Examples of applications of LHDs can be found in Bayarri et al. (2007), Welch et al. (1992), Mease and Bingham (2006), Tyre et al. (2007), and Storlie and Helton (2008). The maximin criterion is used as a secondary criterion for creating the LHDs. All of the LHDs generated in this paper are maximin Latin-hypercube designs.

The uniform design was created by Fang (1980) and Wang and Fang (1981). The uniform design tries to generate a set of points in the design space to be uniformly scattered, as in the uniform distribution. The uniform design is a design created such that the discrepancy, a measure of uniformity, of the design is the smallest (the distribution closest to that of the uniform). Fang et al. (2006) detail several measures of discrepancy, where F(x) is defined as a uniform distribution on C^s (the unit cube) and $F_{D_n}(x)$ is the empirical distribution of the design D_n . Thus,

$$F_{D_n}(x) = \frac{1}{n} \sum_{k=1}^n I\{x_{k_1} \le x_1, \dots, x_{ks} \le x_s\}, \quad (3)$$

where $x = (x_1, \ldots, x_s)$ and $I\{A\} = 1$ if A occurs, or 0 otherwise. In this paper, the software used to create the uniform design uses the centered L_2 discrepancy found in Hickernell (1998). The L_2 discrepancy can be treated as an objective function that can be minimized in continuous space. An example of the application of a uniform design is found in Bursztyn and Steinberg (2006).

The maximum-entropy design, developed in Shewry and Wynn (1987), uses entropy as the optimality criterion, where entropy is a measure of the amount of information contained in the distribution of a data set. In their paper, they show that the expected change in information is maximized by the design D that maximizes the entropy of the observed responses at the points in the design. If the data is assumed to be from a normal $(m, \sigma^2 R)$ distribution, where R is

$$R_{ij} = e^{\left(\sum_{k} \theta_{k} (x_{ik} - x_{ji})^{2}\right)},\tag{4}$$

which is the correlation of responses at two design points, then the design maximizes the determinant of R (|R|) (Sacks et al. (1989)). Note that this criterion requires the specification of the values in the θ_k vector, which, in practice, is not known prior to experimentation. To create maximum-entropy designs in this paper, we made the assumption that the values of θ are all equal. An application of this design can be found in Ko et al. (1995).

Optimal-design theory for experimental design emerged following World War II and was motivated by many authors. I-optimal designs, or integrated variance designs, minimize the average scaled prediction variance over the design region. A D-optimal design minimizes the generalized variance of the model coefficients. This is done by creating a design that maximizes $|\mathbf{X}'\mathbf{X}|$ (Myers and Montgomery (2002)). Examples of optimal designs can be found in Atkinson and Donev (1992). A specific application of the D-optimal design for stochastic computer simulation models can be found in Park et al. (2002).

Examples of each of the designs are presented in Figure 1. Note that the I-optimal and D-optimal designs are the same for 2 factors in 10 runs fit to a second-order polynomial. These designs are seen to only have nine points because they each have a replicated point. The I-optimal design replicates the center point and the D-optimal design replicates a corner point.

Results

Here we compare four types of space-filling designs (sphere packing, LHD, uniform, and maximum entropy) and two types of optimal designs (*I*-optimal and *D*-optimal) using percentiles of prediction variance over the design region and graphical evaluation via FDS plots (Zahran et al. (2003)).

In order to test the predictive capabilities of spacefilling designs and optimal designs when fitting a high-order polynomial, we generated designs ranging from two to five factors and used second-order to

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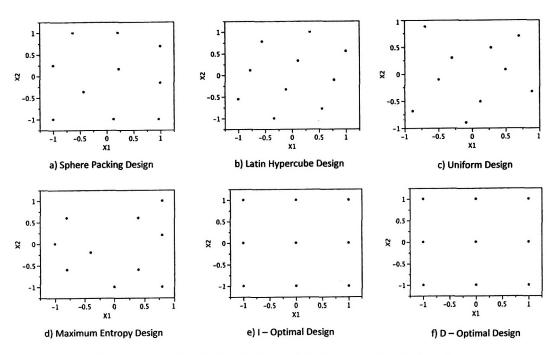


FIGURE 1. Examples of 2 Factors, 10-Run Designs for Each of the Designs Being Evaluated.

fifth-order polynomials to generate the X model matrix. To generate a sphere-packing, Latin-hypercube, or uniform space-filling design, no model specification is necessary, only the required number of points (sample size) is needed. To generate a maximum-entropy design, one must specify prior estimates of the values in the θ vector. In this paper, we assumed equal values of the θ 's. To generate an optimal design, a model must be specified as well as the number of design points required. Table 1 illustrates the minimum number of design points needed to fit a given polynomial with two to five factors.

For all 16 cases (four separate factors levels and four increasing degrees of polynomial), four sets of

TABLE 1. Minimum Number of Design Points Needed (n = p) to Fit a Given Polynomial for a Specified Number of Factors

Order of polynomial						
2	3	4	5			
6	10	15	21			
10	20	35	56			
15	35	70	126			
21	56	126	252			
	6 10 15	2 3 6 10 10 20 15 35	2 3 4 6 10 15 10 20 35 15 35 70			

designs were generated using an increasing sample size. One design contained a minimum number of design points, the second design contained the minimum design points plus two additional points, the third design contained the minimum design points plus four additional points, and finally the fourth design contained double the number of minimum points needed. Table 2 illustrates all of the designs generated with their respective number of runs.

For each of the designs illustrated in Table 2, we generate percentiles of prediction variance and FDS plots a uniform random sample of 10,000 points from the hypercube $[-1,1]^p$. As an example, Figure 2 illustrates FDS plots for each of the designs evaluated for a second-order model in two factors and 10 runs. Figure 2 shows that the *I*-optimal design dominates the other by having the lowest prediction variance across 99.9% of the region. The *I*-optimal design is followed by the *D*-optimal and sphere-packing design, which have equivalent prediction variance performance in this example. The worst design in the example is the maximum-entropy design.

Tables 3 and 4 demonstrate the prediction variance percentiles for the second-order of the space-filling designs and the optimal designs, respectively. The space-filling designs are labeled as SP (sphere packing), LH (Latin hypercube), U (uniform), and

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							O	rder o	f poly	nomial						
Runs →		2nd	order			3rd	order			4th	order			$5 ext{th}$	order	
Factors	p	p+2	p+4	2p	p	p+2	p+4	2p	p	p+2	p+4	2p	p	p+2	p+4	2p
2	6	8	10	12	10	12	14	20	15	17	19	30	21	23	25	42
3	10	12	14	20	20	22	24	40	35	37	39	70	56	58	60	112
$\frac{4}{5}$	15 21	17 23	$\frac{19}{25}$	$\frac{30}{42}$	$\frac{35}{56}$	37 58	39 60	70 112	$70 \\ 126$	72 128	74 130	$\frac{140}{252}$	$\frac{126}{252}$	$\begin{array}{c} 128 \\ 254 \end{array}$	$130 \\ 256$	$\begin{array}{c} 252 \\ 504 \end{array}$

TABLE 2. Number of Runs Required for Each of the Designs Analyzed

ME (maximum entropy). The dark-gray boxes represent the percentiles corresponding to the minimum-prediction variance and the light-gray boxes corresponding to the percentiles with the maximum-prediction variance. Of the space-filling designs in Table 3, the sphere-packing design tends to have the best performance with respect to prediction variance for the second-order design. In 9 out of the 16 designs shown, the sphere-packing design has the lowest prediction variance for more than 50% of the design region. Table 3 also illustrates that the uniform design tends to have the worst performance when compared with the other space-filling designs.

Results from Table 4 indicate that the *I*-optimal design has the best performance in terms of prediction variance with respect to the second-order designs. We expected this because the *I*-optimal designs minimize the average prediction variance of a design with respect to the hypothesized model form. It is not surprising that, in general, the percentiles

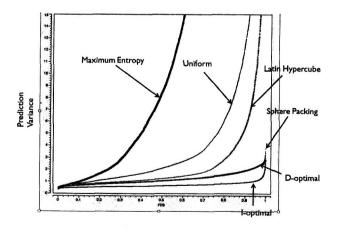


FIGURE 2. FDS Plot for Designs with 2 Variables and 10 Runs Fit to a Second-Order Polynomial Model.

of prediction variance for the I-optimal design would be lower than the competitive designs. In many of the designs shown in Table 4, the D-optimal design has a higher prediction variance at every percentile value recorded, with the exception of the maximum prediction variance. This result is also somewhat intuitive because the D-optimal design tends to spread points to the outside regions of the design, where the joint confidence regions for the unknown betas are influenced the most.

Similar results are demonstrated for the third-, fourth-, and fifth-order cases. The tables for all of these cases can be found in Appendices A, B, and C, which correspond to results from the third-, fourthand fifth-order polynomial cases, respectively. The best overall performance for the space-filling designs is not consistent as polynomial order increases. The sphere-packing designs generally perform better than the Latin hypercube. The uniform and maximumentropy designs demonstrate the worst performance. As for the optimal designs, in almost all cases, the I-optimal design illustrates superior prediction variance properties to the D-optimal, by having the lowest overall prediction variance across most of the design space (the p-dimensional hypercube $[-1,1]^p$). Additionally, when comparing all of the designs together, the I-optimal and D-optimal have a lower prediction variance than the space-filling designs.

A New Class of Hybrid Designs

From the results presented in the previous section, it is clear that space-filling designs are clearly inferior to optimal designs with respect to their prediction variance using a polynomial model of any order. We wished to determine if augmenting space-filling designs with points chosen specifically to reduce prediction variance with respect to a polynomial model would result in a satisfactory compromise.

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TABLE 3. Prediction Variance Percentiles for Second-Order Models for Space-Filling Designs

		n = p = 6	6 runs	$\overline{}$		n = p +	2 = 8 runs				1 = p + 4 =	10 runs				n = 2p =		
2 Factors	SP	ILH IU		ME	SP	LH	U	ME	SP	L	1 1	J	ME	SP	LH	+ ι)	ME
min	3.24		3.24	2.82	2.9	6 2.9	2.96	2.88		3.1	3.4	2.4	2.9		3	2.88	3.12	2.52
5%	3.3		4.32	3.18	3.	2 3.1	3.36	3.12		3.2	3.5	2.7	3.2		3.12	3.12	3.24	2.88
25%	3.72	60	6.24	4.14	3	.6 3.7	3.92	3.52		3.6	3.8	3.3	3.6	101 HOLD 20 HOLD 20	3.36	3.6	3.6	3.36
50%	4.38	5.16	9.3	5.82	3.9	2 4.7	5.12	4.08		4	4.5	5.7	4.1		3.72	4.32	4.56	3.72
75%	5.4	6.48	14.82	8.82	5	.2 8.0	9.52	4.96		4.6	6.1	10.8	4.6		4.56	6.48	8.4	4.68
90%	6	9.66	31.32	13.74	6.0	13.0	1 15.44			5.4	10	15.8	5.4		6	9.84	13.2	6.12
95%	6.84	12.84	48.66	17.16	7.	17.6	3 20.56	7.12		6.3	14.4	19.2	6	COMO (01/10/04/10	7.32	13.2	18.48	7.32
max	15.84	40.32	175.62	25.62	9.0	42.2	50.48	12.72		13.3	40.9	40.6	11.9	1:	5.84	36.48	47.88	13.56
					-							- 100						
		n = p = 1	0 runs			n = p + 2	2 = 12 runs				n = p + 4 =					n = 2p = 1		45
3 Factors	SP	LH I		ME	SP	LH	U	ME	SP	L			ME	SP	LI			ME
min	5.€	4.7	4.8	4.4	5.	3000	177			3.92	4.9	4.34	4.62		4	4.4	3.8	4
5%	6.9	5.7	9.9	7.8	5.	1000	ESSENCE OF RESTREET	100		4.62	5.74	5.74	5.6		4.8	5.2	6.6	4.6 5.2
25%	8.9	7.3	19.6	17.8	100000000000000000000000000000000000000	.6 6.8	100000000000000000000000000000000000000	100		5.18	6.58	8.26	7		5.2	8	9.8	6
50%	11.2	9.5	36.1	45.2	7.	1000	STATE OF THE PARTY			5.74	8.12	12.88	8.4		1100000	13.2	16	8
75%	15.3	15.1	89.7	93	8.		THE RESIDENCE OF THE PARTY OF T			7.14	12.18	22.54	10.92		8.6	21.2	24.6	10.4
90%	20.5	100	203.6	173.8	10.	2000	Constitution of the Consti	000		8.54	19.88	38.5	14.98 20.02		9.8	28	31.6	12.8
95%	23.4		311.7	236.7	12.	2000		20		9.52	25.48	53.06	84.14		20.8	82.6	85.8	38.4
max	87.9	154.5	1672.1	1313.3	28.	112.0	319.9	131.4		16.38	67.76	207.48	84.14		20.0	02.0	63.0	30.4
												10		_		n - 2n -	20 rupo	
		n ≈ p = 1			CD.		2 = 17 runs	IME	SP		n = p + 4 =		ME	SP	TL	n = 2p =		ME
4 Factors		LH	U	ME	SP	LH	U	ME 7.65	SP	L	н ।	U	ME 6.46	SP	5.7	Н	J	ME 5.7
min	8.55	LH 8.1	U 8.25	9.9	7.	LH 48 10.0	U 3 6.2	9 7.65	SP	6.27	7.22	0 6.27	6.46	SP	5.7	H 6.9	J 5,1	5.7
min 5%	8.55 88.05	LH 8.1 12.75	8.25 14.7	9.9 54.6	7.	LH 48 10.0 6.6 13.2	0 3 6.29 6 13.0	9 7.65 6 13.26	SP	6.27 8.55	7.22 8.93	9.69	6.46 9.88	SP	5.7 6.6	H 6.9 7.8	5.1 6.6	
5% 25%	8.55 88.05 441.6	8.1 8.1 12.75 19.05	8.25 14.7 25.8	9.9 54.6 224.55	7. 13 29.	LH 48 10.0 6.6 13.2 07 20.7	0 3 6.2 6 13. 4 25.6	9 7.65 6 13.26 7 21.76	SP	6.27 8.55 11.78	7.22 8.93 10.83	9.69 15.77	6.46 9.88 15.01	SP	5.7 6.6 7.5	H 6.9 7.8 9.9	J 5,1	5.7 7.5
5% 25% 50%	8.55 88.05 441.6 995.55	LH 8.1 12.75 19.05 27.9	U 8.25 14.7 25.8 41.55	9.9 54.6 224.55 484.95	7. 13 29. 66.	LH 10.0 48 10.0 6.6 13.2 07 20.7 13 37.0	U 3 6.2 6 13. 4 25.6 6 50.6	9 7.65 6 13.26 7 21.76 6 36.04		6.27 8.55 11.78 17.1	7.22 8.93 10.83 13.49	9.69 15.77 25.46	6.46 9.88 15.01 21.47		5.7 6.6 7.5 8.7	H 6.9 7.8	5.1 6.6 10.2	5.7 7.5 9
min 5% 25% 50% 75%	8.55 88.05 441.6 995.55 1925.7	8.1 12.75 19.05 27.9 43.5	U 8.25 14.7 25.8 41.55 69.6	9.9 54.6 224.55 484.95 902.4	7. 13 29. 66. 138.	LH 10.0 6.6 13.2 07 20.7 13 37.0 21 75.6	U 3 6.2 6 13. 4 25.6 6 50.6 5 100.	9 7.65 6 13.26 7 21.76 6 36.04 3 57.12		6.27 8.55 11.78 17.1 27.93	7.22 8.93 10.83 13.49 20.52	9.69 15.77 25.46 43.7	6.46 9.88 15.01 21.47 31.54		5.7 6.6 7.5	H 6.9 7.8 9.9 13.8	5.1 6.6 10.2 16.5	5.7 7.5 9 11.4
min 5% 25% 50% 75% 90%	8.55 88.05 441.6 995.55 1925.7 3381.75	8.1 8.1 9 12.75 8 19.05 6 27.9 7 43.5 6 67.2	U 8.25 14.7 25.8 41.55 69.6 132.45	9.9 54.6 224.55 484.95 902.4 2265.15	7. 13 29. 66. 138. 252.	LH 10.0 6.6 13.2 07 20.7 13 37.0 21 75.6 28 127.1	U 3 6.2 6 13.1 4 25.6 6 50.6 5 100.3 6 189.8	9 7.65 6 13.26 7 21.76 6 36.04 3 57.12 9 96.39		6.27 8.55 11.78 17.1 27.93 43.32	7.22 8.93 10.83 13.49 20.52 31.54	9.69 15.77 25.46 43.7 72.39	6.46 9.88 15.01 21.47 31.54 47.88		5.7 6.6 7.5 8.7 10.5	H 6.9 7.8 9.9 13.8 21.6	5.1 6.6 10.2 16.5 26.4	5.7 7.5 9 11.4 17.1
5% 25% 50% 75% 90% 95%	8.58 88.05 441.6 995.55 1925.7 3381.75 4552.05	LH 8.1 6 12.75 6 19.05 6 27.9 7 43.5 6 67.2 97.35	U 8.25 14.7 25.8 41.55 69.6 132.45 215.85	9.9 54.6 224.55 484.95 902.4 2265.15 3914.25	7. 13 29. 66. 138. 252.	LH 10.0 1.6 13.2 107 20.7 13 37.0 21 75.6 28 127.1 18 163.3	U 3 6.2 6 13.4 25.6 6 50.6 5 100.6 189.8 7 28	9 7.65 6 13.26 7 21.76 6 36.04 3 57.12 9 96.39 9 152.83		6.27 8.55 11.78 17.1 27.93 43.32 55.86	7.22 8.93 10.83 13.49 20.52 31.54 40.09	9.69 15.77 25.46 43.7 72.39 100.89	6.46 9.88 15.01 21.47 31.54		5.7 6.6 7.5 8.7 10.5 13.2	H 6.9 7.8 9.9 13.8 21.6 33.3	5.1 6.6 10.2 16.5 26.4 39.6	5.7 7.5 9 11.4 17.1 25.2
min 5% 25% 50% 75% 90%	8.58 88.09 441.6 995.59 1925.7 3381.79 4552.09	LH 8.1 6 12.75 6 19.05 6 27.9 7 43.5 6 67.2 97.35	U 8.25 14.7 25.8 41.55 69.6 132.45	9.9 54.6 224.55 484.95 902.4 2265.15	7. 13 29. 66. 138. 252.	LH 10.0 1.6 13.2 107 20.7 13 37.0 21 75.6 28 127.1 18 163.3	U 3 6.2 6 13.4 25.6 6 50.6 5 100.6 189.8 7 28	9 7.65 6 13.26 7 21.76 6 36.04 3 57.12 9 96.39 9 152.83		6.27 8.55 11.78 17.1 27.93 43.32	7.22 8.93 10.83 13.49 20.52 31.54	9.69 15.77 25.46 43.7 72.39	6.46 9.88 15.01 21.47 31.54 47.88 64.79		5.7 6.6 7.5 8.7 10.5 13.2	H 6.9 7.8 9.9 13.8 21.6 33.3 42.3	5.1 6.6 10.2 16.5 26.4 39.6 49.8	5.7 7.5 9 11.4 17.1 25.2 32.1
5% 25% 50% 75% 90% 95%	8.58 88.09 441.6 995.59 1925.7 3381.79 4552.09	LH 8.1 12.75 19.05 6 27.9 43.5 6 67.2 97.35 608.4	U 8.25 14.7 25.8 41.55 69.6 132.45 215.85 1067.7	9.9 54.6 224.55 484.95 902.4 2265.15 3914.25	7. 13 29. 66. 138. 252.	LH 10.0 1.6 13.2 1.7 20.7 13 37.0 21 75.6 127.1 18 163.3 769.4	U 3 6.2: 6 13.4 25.6 50.6 50.6 189.8 7 28: 2 1250.1	9 7.65 6 13.26 7 21.76 6 36.04 3 57.12 9 96.39 9 152.83 8 895.22		6.27 8.55 11.78 17.1 27.93 43.32 55.86 106.97	H 7.22 8.93 10.83 13.49 20.52 31.54 40.09 137.37	0.27 9.69 15.77 25.46 43.7 72.39 100.89 636.88	6.46 9.88 15.01 21.47 31.54 47.88 64.79		5.7 6.6 7.5 8.7 10.5 13.2	H 6.9 7.8 9.9 13.8 21.6 33.3 42.3 125.4	5.1 6.6 10.2 16.5 26.4 39.6 49.8 133.5	5.7 7.5 9 11.4 17.1 25.2 32.1
min 5% 25% 50% 75% 90% 95% max	8.55 88.05 441.6 995.55 1925.7 3381.75 4552.05 9812.7	LH 8.1 12.75 19.05 27.9 43.5 6 67.2 5 97.35 608.4	U 8.25 14.7 25.8 41.55 69.6 132.45 215.85 1067.7	9.9 54.6 224.55 484.95 902.4 2265.15 3914.25 23638.5	7. 13 29. 66. 138. 252. 332. 843.	LH 10.0 16.6 13.2 10.7 20.7 20.7 13 37.0 21 75.6 28 127.1 18 163.3 769.4	U 3 6.2 6 13.4 4 25.6 6 50.6 5 100.6 6 189.8 7 28 2 1250.1	9 7.65 6 13.26 7 21.76 6 36.04 3 57.12 9 96.39 9 152.83 8 895.22		6.27 8.55 11.78 17.1 27.93 43.32 55.86 106.97	H 7.22 8.93 10.83 13.49 20.52 31.54 40.09 137.37	0.27 9.69 15.77 25.46 43.7 72.39 100.89 636.88	6.46 9.88 15.01 21.47 31.54 47.88 64.79		5.7 6.6 7.5 8.7 10.5 13.2 15 28.8	H 6.9 7.8 9.9 13.8 21.6 33.3 42.3 125.4	5.1 6.6 10.2 16.5 26.4 39.6 49.8 133.5	5.7 7.5 9 11.4 17.1 25.2 32.1
min 5% 25% 50% 75% 90% 95% max 5 Factors	8.55 88.05 441.6 995.55 1925.7 3381.75 4552.05 9812.7	LH 8.1 6 12.75 6 19.05 7 43.5 6 67.2 9 7.35 7 608.4	U 8.25 14.7 25.8 41.55 69.6 132.45 215.85 1067.7	9.9 54.6 224.55 484.95 902.4 2265.15 3914.25 23638.5	7. 13 29. 66. 138. 252. 332. 843.	LH 10.0 1.6 13.2 1.7 20.7 13 37.0 21 75.6 28 127.1 18 163.3 769.4 n = p +	U 6.2° 6 13.4 4 25.6° 6 50.6° 5 100.6° 6 189.8° 7 28° 2 1250.1° 2 = 23 runs	9 7.65 6 13.26 7 21.76 6 36.04 3 57.12 9 96.39 9 152.83 8 895.22		6.27 8.55 11.78 17.1 27.93 43.32 55.86 106.97	H 7.22 8.93 10.83 13.49 20.52 31.54 40.09 137.37	0.27 9.69 15.77 25.46 43.7 72.39 100.89 636.88	6.46 9.88 15.01 21.47 31.54 47.88 64.79 305.33	SP	5.7 6.6 7.5 8.7 10.5 13.2 15 28.8	H 6.9 7.8 9.9 13.8 21.6 33.3 42.3 125.4	5.1 6.6 10.2 16.5 26.4 39.6 49.8 133.5	5.7 7.5 9 11.4 17.1 25.2 32.1 94.8
min 5% 25% 50% 75% 90% 95% max 5 Factors	8.55 88.05 441.6 995.5 1925.7 4552.0 9812.7	LH 8.1 12.75 6 19.05 6 27.9 43.5 6 67.2 6 97.35 7 608.4 n = p = 2 LH 14.28	U 8.25 14.7 25.8 41.55 69.6 132.45 215.85 1067.7 21 runs U 9.03	9.9 54.6 224.55 484.95 902.4 2265.15 3914.25 23638.5	7. 13 29. 66. 138. 252. 332. 843.	LH 10.0 13.2 13.2 13.2 13.2 13.2 13.2 13.2 13.2	U 33 6.2 6 13.4 25.6 6 50.6 5 100.3 6 189.8 7 28 2 1250.1 2 = 23 runs U 9 11.	9 7.65 6 13.26 7 21.76 6 36.04 3 57.12 9 96.39 9 152.83 8 895.22		6.27 8.55 11.78 17.1 27.93 43.32 55.86 06.97	H 7.22 8.93 10.83 13.49 20.52 31.54 40.09 137.37	U 6.27 9.69 15.77 25.46 43.7 72.39 100.89 636.88	6.46 9.88 15.01 21.47 31.54 47.88 64.79 305.33	SP	5.7 6.6 7.5 8.7 10.5 13.2 15 28.8	H 6.9 7.8 9.9 13.8 21.6 33.3 42.3 125.4	5.1 6.6 10.2 16.5 26.4 39.6 49.8 133.5	5.7 7.5 9 11.4 17.1 25.2 32.1 94.8
min 5% 25% 50% 75% 90% 95% max 5 Factors mir 5%	8.55 88.05 441.6 995.5 1925.3 3381.7 4552.0 9812.3 SP	LH 8.1 12.75 19.05 6 27.9 7 43.5 67.2 6 97.35 7 608.4 n = p = 2 LH 3 14.28 5 27.72	U 8.25 14.7 25.8 41.55 69.6 132.45 215.85 1067.7 21 runs U 9.03 30.87	9,9 54.6 224.55 484.95 902.4 2265.15 3914.25 23638.5 ME 9.87 23.52	7. 13 29. 66. 138. 252. 332. 843.	LH 10.0 10.6 13.2 10.7 20.7 13 37.0 21 75.6 28 127.1 18 163.3 769.4 n = p + LH LH 1.5 12.1 48 17.2	U 6.21 6.22 6.33 6.22 6.33 6.32 6.3	9 7.65 6 13.26 7 21.76 6 36.04 3 57.12 9 96.39 9 152.83 8 895.22 ME 5 8.28		6.27 8.55 11.78 17.1 27.93 43.32 55.86 106.97	H 7.22 8.93 10.83 13.49 20.52 31.54 40.09 137.37	0 6.27 9.69 15.77 25.46 43.7 72.39 100.89 636.88 = 25 runs U	6.46 9.88 15.01 21.47 31.54 47.88 64.79 305.33 ME 9.75	SP	5.7 6.6 7.5 8.7 10.5 13.2 15 28.8	H 6.9 7.8 9.9 13.8 21.6 33.3 42.3 125.4 n = 2p = H	5.1 6.6 10.2 16.5 26.4 39.6 49.8 133.5	5.7 7.5 9 11.4 17.1 25.2 32.1 94.8 ME 6.72
min 5% 25% 50% 75% 90% 955% max 5 Factors mir 5% 25%	8.55 88.05 441.6 995.51 1925.3 3381.7! 4552.09 9812.3 SP 21.6:	H 8.1 12.75 19.05 27.9 43.5 6 67.2 6 97.35 608.4 n = p = 2 LH 14.28 3 14.28 5 27.72 4 64.47	U 8.25 14.7 25.8 41.55 69.6 132.45 215.85 1067.7 21 runs U 9.03 30.87	9.9 54.6 224.55 484.95 902.4 2265.15 3914.25 23638.5 ME 9.87 23.52 49.77	7. 15 29. 666. 138. 252. 332. 843.	LH 10.0.6 13.2.2077 20.7	U 3 6.23 3 6.23 6 13.1 4 25.6 6 5 100.3 6 189.8 7 7 28 2 1250.1 U U U 5 22.0 1 38.6 1 38.6 1	9 7.65 6 13.26 7 21.76 6 36.04 9 96.39 9 152.83 8 895.22 ME 5 8.28 8 15.41 4 28.29		6.27 8.55 11.78 17.1 27.93 43.32 55.86 106.97	H 7.22 8.93 10.83 13.49 20.52 31.54 40.09 137.37 n = p + 4 = H	U 6.27 9.69 15.77 25.46 43.7 72.39 100.89 636.88 = 25 runs U 9	6.46 9.88 15.01 21.47 31.54 47.88 64.79 305.33 ME 9.75 17.75	SP SP	5.7 6.6 7.5 8.7 10.5 13.2 15 28.8	H 6.9 7.8 9.9 13.8 21.6 33.3 42.3 125.4 n = 2p = H 9.24 11.76	J 5.1 6.6 10.2 16.5 26.4 39.6 49.8 133.5 42 runs U 6.3 9.24	5.7 7.5 9 11.4 17.1 25.2 32.1 94.8 ME 6.72 8.82 13.02 19.32
min 5% 25% 50% 75% 90% 95% max 5 Factors mir 5% 25% 50%	8.55 88.05 441.6 995.5 1925.3 3381.7 4552.0 9812.3 SP 21.6 133.3 254.9 360.5	LH 8.1 8.1 9 12.75 9 143.5 6 67.2 9 97.35 6 608.4 9 14.28 5 27.72 14.28 6 4.47 7 135.45	U 8.25 14.7 25.8 41.55 69.6 132.45 215.85 1067.7 U 9.03 30.87 107.73	9.9 54.6 224.55 484.95 902.4 2265.15 3914.25 23638.5 ME 9.87 23.52 49.77 96.6	7. 15 29. 66. 138. 252. 332. 843.	LH 10.0 13.2 13.2 13.2 13.2 13.2 13.2 13.2 13.2	U 3 6.2:4 4 25.6 6 13.1 4 25.6 6 50.6 6 189.8:7 7 28:2 1250.1 2 = 23 runs U 9 11. 5 22.0 1 38.6 8 60.0	9 7.65 6 13.26 7 21.76 6 36.04 3 57.12 9 96.39 9 152.83 8 895.22 ME 5 8.28 8 15.41 4 28.29 3 52.9		6.27 8.55 11.78 17.1 27.93 43.32 55.86 06.97 L 10.5 15.25 18.75	H 7.22 8.93 10.83 13.49 20.52 31.54 40.09 137.37 n = p + 4 = H	U 6.27 9.69 15.77 25.46 43.7 72.39 100.89 636.88 = 25 runs U 9 17.75	6.46 9.88 15.01 21.47 31.54 47.88 64.79 305.33 ME 9.75 17.75 28	SP	5.7 6.6 7.5 8.7 10.5 13.2 15 28.8	H 6.9 7.8 9.9 13.8 21.6 33.3 42.3 125.4 n = 2p = H 9.24 11.76 14.7	J 5.1 6.6 10.2 16.5 26.4 39.6 49.8 133.5 42 runs U 6.3 9.24 16.8	5.7 7.5 9 11.4 17.1 25.2 32.1 94.8 ME 6.72 8.82 13.02
min 5% 25% 50% max 5 Factors mir 5% 25% 25% 75% 75% 75% 75% 75% 75% 75% 75% 75% 7	8.55 88.05 441.6 995.5 1925. 3381.7* 4552.0 9812.3 SP 21.6 333.3 254.9 360.5 482.5	LH 8.1 12.75 19.05	U 8.25 14.7 25.8 41.55 69.6 132.45 215.85 1067.7 21 runs U 9.03 30.87 107.73 300.09	9.9 54.6 224.55 484.95 902.4 2265.15 3914.25 23638.5 ME 9.87 23.52 49.77 96.6 199.92	7. 11 29. 66. 138. 252. 843.	LH 10.0 LH 10.	U 6.21 3 6.22 13.1 4 25.6 6 50.6 6 189.8 7 282 2 1250.1 2 = 23 runs U 9 11. 2 = 2.0 1 38.6 8 60.0 7 95.2	9 7.65 6 13.26 7 21.76 8 36.04 3 55.12 9 9 96.39 9 152.83 8 895.22 ME 5 8.28 8 15.41 4 28.29 3 52.9 3 52.9		6.27 8.55 11.78 17.1 27.93 43.32 55.86 106.97	H 7.22 8.93 10.83 13.49 20.52 31.54 40.09 137.37 n = p + 4 = H 12.5 17 21.75 28	U 6.27 9.69 15.77 25.46 43.7 72.39 100.89 636.88 = 25 runs U 9 17.75 32 56.5	6.46 9.88 15.01 21.47 31.54 47.88 64.79 305.33 ME 9.75 17.75 28 43.75	SP 11 11 11	5.7 6.6 7.5 8.7 10.5 13.2 15 28.8 L 7.98 9.66 0.92 2.18	H 6.9 7.8 9.9 13.8 21.6 33.3 42.3 125.4 n = 2p = H 9.24 11.76 14.7 19.74	J 5.1 6.6 10.2 16.5 26.4 39.6 49.8 133.5 42 runs U 6.3 9.24 16.8	5.7 7.5 9 11.4 17.1 25.2 32.1 94.8 ME 6.72 8.82 13.02 19.32
min 5% 25% 50% 75% 90% 95% max 5 Factors mir 5% 25% 50% 75% 90% 95% 90% 95% 90% 95% 90% 95% 90% 95% 90% 95% 90% 95% 90% 95% 95% 90% 95% 90%	8.58 88.01 441.6 995.51 1925. 3381.7 4552.01 9812.7 SP 21.6 133.3 360.5 482.5 607.9	B.1 12.75 19.05 19	U 8.25 14.7 25.8 41.55 69.6 132.45 215.85 1067.7 21 runs U 9.03 30.87 107.73 300.09 880.53 2058.84	9.9 54.6 224.55 484.95 902.4 2265.15 3914.25 23638.5 ME 9.87 23.52 49.77 96.6 199.92 383.04	7. 11 29. 66. 138. 252. 332. 843. SP 11 17. 23. 311. 45. 63.	LH 10.0.0 13.2 16.6 13.2 17.7 13 17.6 18 16.7 16.8 17.6 17.6 18 18 16.3 17.6 18 16.3 17.6 18 17.6 18 17.6 18 17.6 18 17.6 18 17.6 18 17.6 18 17.6 18 17.6 18 17.6 18 17.6 18 18 18 18 18 18 18 1	U 3 6.2:3 6.	9 7.65 6 13.26 6 36.04 3 57.12 9 96.39 9 152.83 8 895.22 ME 5 8.28 8 15.41 4 28.29 2 109.71 2 109.60		6.27 8.55 11.78 17.1 27.93 43.32 55.86 106.97	H 7.22 8.93 10.83 13.49 20.52 31.54 40.09 137.37 n = p + 4 = H 12.5 17 21.75 28 41	U 6.27 9.69 15.77 25.46 43.7 72.39 100.89 636.88 = 25 runs U 9 17.75 32 56.5	6.46 9.88 15.01 21.47 31.54 47.88 64.79 305.33 ME 9.75 17.75 28.4 43.75 82.5	SP	5.7 6.6 7.5 8.7 10.5 13.2 15 28.8 L 7.98 9.66 0.92 2.18 3.86	H 6.9 7.8 9.9 13.8 21.6 33.3 42.3 125.4 n = 2p = H 9.24 11.76 14.7 19.74 30.66	J 5,1 6,6 10,2 16,5 26,4 39,6 49,8 133,5 42 runs U 6,3 9,24 16,8 26,88 42,42	5.7 7.5 9 11.4 17.1 25.2 32.1 94.8 ME 6.72 8.82 13.02 19.32 28.98
min 5% 25% 50% 75% 90% 95% max 5 Factors mir 5% 25% 50%	8.55 88.05 441.6 995.5 1925.3 3381.7 4552.0 9812.3 SP 21.6 133.3 254.9 360.5	LH 8.1 8.1 9 12.75 9 143.5 6 67.2 9 97.35 6 608.4 9 14.28 5 27.72 14.28 6 4.47 7 135.45	U 8.25 14.7 25.8 41.55 69.6 132.45 215.85 1067.7 U 9.03 30.87 107.73	9.9 54.6 224.55 484.95 902.4 2265.15 3914.25 23638.5 ME 9.87 23.52 49.77 96.6	7. 15 29. 66. 138. 252. 332. 843.	LH 10.0 13.2 13.2 13.2 13.2 13.2 13.2 13.2 13.2	U 3 6.2:4 4 25.6 6 13.1 4 25.6 6 50.6 6 189.8:7 7 28:2 1250.1 2 = 23 runs U 9 11. 5 22.0 1 38.6 8 60.0	9 7.65 6 13.26 7 21.76 6 36.04 3 57.12 9 96.39 9 152.83 8 895.22 ME 5 8.28 8 15.41 4 28.29 3 52.9		6.27 8.55 11.78 17.1 27.93 43.32 55.86 106.97	H 7.22 8.93 10.83 13.49 20.52 31.54 40.09 137.37 n = p + 4 = H 12.5 17 21.75 28	U 6.27 9.69 15.77 25.46 43.7 72.39 100.89 636.88 = 25 runs U 9 17.75 32 56.5	6.46 9.88 15.01 21.47 31.54 47.88 64.79 305.33 ME 9.75 17.75 28 43.75	SP	5.7 6.6 7.5 8.7 10.5 13.2 15 28.8 L 7.98 9.66 0.92 2.18	H 6.9 7.8 9.9 13.8 21.6 33.3 42.3 125.4 n = 2p = H 9.24 11.76 14.7 19.74	J 5.1 6.6 10.2 16.5 26.4 39.6 49.8 133.5 42 runs U 6.3 9.24 16.8	5.7 7.5 9 11.4 17.1 25.2 32.1 94.8 ME 6.72 8.82 13.02 19.32
min 5% 25% 50% max 5 Factors mir 5% 25% 25% 75% 75% 75% 75% 75% 75% 75% 75% 75% 7	8.58 88.01 441.6 995.51 1925. 3381.7 4552.01 9812.7 SP 21.6 133.3 360.5 482.5 607.9	B.1 (12.75 (19.05) (19	U 8.25 14.7 25.8 41.55 69.6 132.45 215.85 1067.7 21 runs U 9.03 30.87 107.73 300.09	9.9 54.6 224.55 484.95 902.4 2265.15 3914.25 23638.5 ME 9.87 23.52 49.77 96.6 199.92	7. 11 29. 66. 138. 252. 843.	LH 10.0 448 10.0 475 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.	U 3 6.2: 3 6.2: 4 25.6 6 50.6: 5 100.0 5 100.2 7 28: 2 1250.1 2 = 23 runs U 11. 5 22.0 1 38.6 8 60.0 6 166.5 6 166.5 8 239.8	9 7.65 6 13.26 6 36.04 3 57.12 9 96.39 9 152.83 8 895.22 ME 5 8.28 8 15.41 4 28.29 3 52.9 2 109.71 2 200.08 9 314.87		6.27 8.55 11.78 17.1 27.93 43.32 55.86 06.97 L 10.5 15.25 18.75 22 26.75 33.5	H 7.22 8.93 10.83 13.49 20.52 31.54 40.09 137.37 n = p + 4 = H 12.5 17 21.75 28 41 64.75	U 6.27 9.69 15.77 25.46 43.7 72.39 100.89 636.88 = 25 runs U 9 17.75 32 56.5 103.5 176.75	6.46 9.88 15.01 21.47 31.54 47.88 64.79 305.33 ME 9.75 17.75 28 43.75 82.5 163.25	SP 11 11 11 11 11 11 11 11 11 11 11 11 11	5.7 6.6 7.5 8.7 10.5 13.2 15 28.8 L 7.98 9.66 0.92 2.18 3.86 6.38	H 6.9 7.8 9.9 13.8 21.6 33.3 42.3 125.4 n = 2p = H 9.24 11.76 14.7 19.74 30.66 45.36	J 5,1 6,6 10,2 11,5,5 26,4 39,6 49,8 133,5 42 runs U 6,3 9,24 16,8 26,88 42,42 63	5.7 7.5 9 11.4 17.1 25.2 32.1 94.8 ME 6.72 8.82 13.02 19.32 28.98 42

A small example demonstrates the idea. Consider Figure 3, which illustrates two designs, both containing two factors and 10 runs designs to fit a third-order polynomial (note these are saturated designs). The FDS plot for each of these designs is shown in Figure 4.

It is clear from this figure that the I-optimal design performs better because it has lower prediction variance over the entire curve. Can the performance of the LHD be improved by augmenting the design with I-optimal points? Figure 5 illustrates two designs each with two factors. The first design (Figure 5a) is an I-optimal design with 16 design points and the second (Figure 5b) is the LHD shown in Figure 3b augmented with 6 I-optimal points that were chosen to minimize the average prediction variance of the combined design given the preexisting 10 points. The FDS plot for these designs is shown in Figure 6.

The improved performance of the augmented LHD

is clear from examination of Figure 6. Design augmentation is a standard procedure in physical experimentation. Building up information sequentially through design augmentation is efficient and economical. Montgomery (2006) points out that it is almost always preferable to run a fractional design, analyze the results, and then decide on the best set of runs to perform next. We believe that design augmentation can also be used in computer-simulation modeling. We find that design augmentation is especially effective when the initial analysis of a space-filling design indicates that a polynomial is adequate. The results illustrated in Figure 4 and Figure 6 demonstrate that this procedure can be effective in improving the prediction variance across the design region. This is important because the goal of a surrogate model is to closely approximate the computer model. We introduce augmentation of space-filling designs and refer to them as space-filling-hybrid designs.

The next section demonstrates the augmentation

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TABLE 4. Prediction Variance Percentiles for Second-Order Models for Optimal Designs

_	n = p =			= 8 runs		= 10 runs		12 runs
	I Opt	D Opt	I Opt	D Opt	I Opt	D Opt	I Opt	D Opt
min	0.46	0.48	2.88	100000000000000000000000000000000000000	2.9	2.7	2.76	3.
5%	Later Control of the Control	0.67	3.12	3.12	2.9	3.3	3	3.4
25%	0.63	1.06	3,6	3.6	3.1	3.9	3.48	4
50%	0.9	1.62	4.16	4.16	3.4	4.3	3.84	4
75%	1.15	2.09	5.04	5.04	4	4.7	4.2	5.
90%	1.35	2.48	6	6	4.8	5.2	5.04	5.
95%	1.57	2.62	6.88	6.88	5.1	5.3	5.64	6.
max	5.45	2.79	9.84	9.92	7.9	7.7	9	9.
_		10 runs		= 12 runs		= 14 runs	n = 2p =	
3 Factors	I Opt	D Opt	I Opt	D Opt	I Opt	D Opt	I Opt	D Opt
min	27.6	28.8	3.72	4.32	4.34	4.34	3.8	
5%	30	40.2	4.32	5.64	4.62	4.62	4	
25% 50%	37.8 54	63.6	4.8	6.96	5.04	5.04	4.2	
75%	TOTAL STREET,	97.2	5.52	8.16	5.46	5.46	5	
90%	69	125.4	7.08	9.36	6.58	6.44	6.2	
	81	148.8	9.36	10.92	7.28	7.42	7.2	
000/	100000000000000000000000000000000000000				7.7	7.7	8.2	10
95%	94.2	157.2	12.12	200000000000000000000000000000000000000		40.00	10.0	Total Control of the Control
95% max	94.2 327	167.4	30.48	17.16	9.8	10.22	13.2	
max	327 n = p =	167.4 15 runs	30.48 n = p + 2	17.16 = 17 runs	9.8 n = p + 4	= 19 runs	n = 2p =	30 runs
max	n = p = I Opt	167.4 15 runs D Opt	30.48 n = p + 2 I Opt	17.16 = 17 runs D Opt	9.8 n = p + 4 I Opt	= 19 runs D Opt	n = 2p =	30 runs
Factors	327 n = p = I Opt 5.85	167.4 15 runs D Opt 6.6	30.48 n = p + 2 I Opt 4.25	17,16 = 17 runs D Opt 6.12	9.8 n = p + 4 I Opt 4.75	= 19 runs D Opt 6.46	n = 2p = I Opt 4.5	30 runs D Opt
Factors min 5%	n = p = I Opt 5.85 8.25	15 runs D Opt 6.6 8.56	30.48 n = p + 2 I Opt 4.25 5.44	17.16 = 17 runs D Opt 6.12 8.67	9.8 n = p + 4 l Opt 4.75 5.51	= 19 runs D Opt 6.46 8.36	n = 2p = I Opt 4.5 4.5	30 runs D Opt
Factors min 5% 25%	327 n = p = I Opt 5.85 8.25 10.05	167.4 15 runs D Opt 6.6 8.56 10.2	30.48 n = p + 2 I Opt 4.25 5.44 6.46	17.16 = 17 runs D Opt 6.12 8.67 10.71	9.8 n = p + 4 l Opt 4.75 5.51 6.27	= 19 runs D Opt 6.46 8.36 9.88	n = 2p = l Opt 4.5 4.5 5.4	30 runs D Opt
Factors min 5% 25% 50%	n = p = l Opt 5.85 8.25 10.05	167.4 15 runs D Opt 6.6 8.56 10.2 11.7	30.48 n = p + 2 I Opt 4.25 5.44 6.46 8.33	17.16 = 17 runs D Opt 6.12 8.67 10.71 12.58	9.8 n = p + 4 l Opt 4.75 5.51 6.27 7.79	= 19 runs D Opt 6.46 8.36 9.88 11.21	n = 2p = l Opt 4.5 4.5 5.4 6.9	30 runs D Opt
Factors min 5% 25% 50% 75%	n = p = 1 Opt 5.85 8.25 10.05 11.1 12.6	15 runs D Opt 6.6 8.56 10.2 11.7 13.35	30.48 n = p + 2 I Opt 4.25 5.44 6.46 8.33 10.54	17.16 = 17 runs D Opt 6.12 8.67 10.71 12.58 14,62	9.8 n = p + 4 l Opt 4.75 5.51 6.27 7.79 9.69	= 19 runs D Opt 6.46 8.36 9.88 11.21 12.92	n = 2p = l Opt 4.5 4.5 5.4 6.9 8.7	30 runs D Opt
Factors min. 5% 25% 50% 75% 90%	n = p = l Opt 5.85 8.25 10.05 11.1 12.6 14.55	167.4 15 runs D Opt 6.6 8.56 10.2 11.7 13.35 15.75	n = p + 2 I Opt 4.25 5.44 6.46 8.33 10.54 12.92	17,16 = 17 runs D Opt 6.12 8.67 10,71 12.58 14,62 16,32	9.8 n = p + 4 I Opt 4.75 5.51 6.27 7.79 9.69 11.97	= 19 runs D Opt 6.46 8.36 9.88 11.21 12.92 14.25	n = 2p = l Opt 4.5 4.5 5.4 6.9 8.7	30 runs D Opt 1 1 13
Factors min 5% 25% 50% 75%	n = p = 1 Opt 5.85 8.25 10.05 11.1 12.6	15 runs D Opt 6.6 8.56 10.2 11.7 13.35	30.48 n = p + 2 I Opt 4.25 5.44 6.46 8.33 10.54	17.16 = 17 runs D Opt 6.12 8.67 10.71 12.58 14,62	9.8 n = p + 4 l Opt 4.75 5.51 6.27 7.79 9.69	= 19 runs D Opt 6.46 8.36 9.88 11.21 12.92	n = 2p = l Opt 4.5 4.5 5.4 6.9 8.7	30 runs D Opt 12 13 18
max Factors min 5% 25% 50% 75% 90% 95% max	n = p = 1 Opt 5.85 8.25 10.05 11.1 12.6 14.55 16.65 40.5	167.4 15 runs D Opt 6.6 8.56 10.2 11.7 13.35 15.76 17.55 28.65	n = p + 2 l Opt 4.25 5.44 6.46 8.33 10.54 12.92 14.79 29.58	17.16 = 17 runs D Opt 6.12 8.67 10.71 12.58 14.62 16.32 17.34 23.97	9.8 n = p + 4 I Opt 4.75 5.51 6.27 7.79 9.69 11.97 13.49 27.93	= 19 runs D Opt 6.46 8.36 9.88 11.21 12.92 14.25 15.39 23.75	n = 2p = I Opt 4.5 4.5 5.4 6.9 8.7 10.8 12.3 24.6	30 runs D Opt 11 12 13 15 18 42 runs
Factors min 5% 25% 50% 75% 90% max Factors	n = p = 1 Opt 5.85 8.25 10.05 11.1 12.6 14.55 16.65 40.5	167.4 15 runs D Opt 6.6 8.55 10.2 11.7 13.35 15.75 17.55 28.65	30.48 n = p + 2 I Opt 4.25 5.44 6.46 8.33 10.54 12.92 14.79 29.58	17.16 = 17 runs D Opt 6.12 8.67 10.71 12.58 14.62 16.32 17.34 23.97 = 23 runs D Opt	9.8 n = p + 4 I Opt 4.75 5.51 6.27 7.79 9.69 11.97 13.49 27.93	= 19 runs D Opt 6.46 8.36 9.88 11.21 12.92 14.25 15.39 23.75	n = 2p = I Opt 4.5 4.5 5.4 6.9 8.7 10.8 12.3 24.6	30 runs D Opt 11 12 13 18 18 42 runs D Opt
Factors min 5% 25% 50% 75% 90% max Factors min	n = p = 1 Opt 5.85 8.25 10.05 11.1 12.6 14.55 16.65 40.5	167.4 15 runs D Opt 6.6 8.56 10.2 11.7 13.35 15.76 28.65 21 runs D Opt 6.93	30.48 n = p + 2 1 Opt 4.25 5.44 6.46 6.33 10.54 12.92 14.79 29.58 n = p + 2 1 Opt	17.16 = 17 runs D Opt 6.12 8.67 10.71 12.58 14.62 16.32 17.34 23.97 = 23 runs D Opt 8.05	9.8 n = p + 4 I Opt 4.75 5.51 6.27 7.79 9.69 9.11.97 13.49 27.93 n = p + 4 I Opt 6	= 19 runs D Opt 6.46 8.36 9.88 11.21 12.92 14.25 15.39 23.75 = 25 runs D Opt 9.25	n = 2p = I Opt 4.5 4.5 5.4 6.9 8.7 10.8 12.3 24.6	30 runs D Opt 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Factors min 5% Factors 90% 95% max Factors min 5%	n = p = 1 Opt 5.85 8.25 10.05 11.1 12.6 14.55 16.65 40.5 n = p = 1 Opt 7.77 10.5	167.4 15 runs D Opt 6.6 8.55 10.2 11.7 13.35 15.75 28.65 21 runs D Opt 6.93 13.44	30.48 n = p + 2 I Opt 4.25 5.44 6.46 6.33 10.54 12.92 14.79 29.58 n = p + 2 I Opt 6.44 7.59	17.16 = 17 runs D Opt 6.12 8.67 10.71 12.58 14.62 16.32 17.34 23.97 = 23 runs D Opt 8.05 13.11	9.8 n = p + 4 l Opt 4.75 5.51 6.27 7.79 9.69 11.97 13.49 27.93 n = p + 4 l Opt 6 7.25	= 19 runs D Opt 8.46 8.36 9.88 11.21 12.92 14.25 15.39 23.75 = 25 runs D Opt	n = 2p = 1 Opt 4.5 4.5 5.4 6.9 8.7 10.8 12.3 24.6 n = 2p = 1 Opt 5.04 5.46	30 runs D Opt 11 12 13 18 18 18 10 Opt 42 runs D Opt 10.
Factors min 5% 90% max Factors min 55% 90% 95% max	327 n = p = 1 1 Opt 5.85 8.25 10.05 11.1 12.6 14.55 16.65 40.5 n = p = 1 1 Opt 7.77 10.5 12.81	167.4 15 runs D Opt 6.6 8.56 10.2 11.7 13.35 15.75 28.65 21 runs D Opt 6.93 13.44 17.01	30.48 n = p + 2 I Opt 4.25 5.44 6.46 8.33 10.54 12.92 29.58 n = p + 2 I Opt 6.44 7.59 9.66	17.18 = 17 runs D Opt 6.12 8.67 10.71 12.58 14.62 16.32 17.34 23.97 = 23 runs D Opt 8.05 13.11 15.64	9.8 n = p + 4 l Opt 4.75 5.51 6.27 7.79 9.69 11.97 13.49 27.93 n = p + 4 l Opt 6 7.255	= 19 runs D Opt 6.49 8.36 9.88 11.21 12.92 14.25 15.39 23.75 = 25 runs D Opt 9.25 13 15.5	n = 2p = 1 Opt 4.5 4.5 4.5 5.4 6.9 8.7 10.8 12.3 24.6 n = 2p = 1 Opt 5.04 6.4 6.4 6.7 6.4 6.7	30 runs D Opt 1 1 12 16 18 18 18 D Opt 42 runs D Opt 10. 13. 15.
Factors min 5% 25% 50% 75% 90% 95% max Factors min 5% 50% 50%	n = p = 1 Opt 5.85 8.25 10.05 11.1 12.6 14.55 40.5 n = p = 1 Opt 7.77 10.5 12.81 15.12	167.4 15 runs D Opt 6.6 8.55 10.2 11.7 13.35 15.75 17.55 28.65 21 runs D Opt 6.93 13.44 17.01 19.53	30.48 n = p + 2 Opt	17.16 = 17 runs D Opt 6.12 8.67 10.71 12.58 14.62 17.34 23.97 = 23 runs D Opt 8.05 13.11 15.64 17.25	9.88 n = p + 4 l Opt 4.75 5.51 6.277 7.79 9.69 11.97 13.49 27.93 n = p + 4 l Opt 6 7.25 9 11.25	= 19 runs D Opt 6.46 8.36 9.88 11.21 12.92 14.25 15.39 23.75 = 25 runs D Opt 9.25 13 15.56 17.51	n = 2p = 1 Opt 4.5 4.5 5.4 6.9 8.7 10.8 12.3 24.6 n = 2p = 1 Opt 5.04 5.46	30 runs D Opt 1 1 12 16 18 18 18 D Opt 42 runs D Opt 10. 13. 15.
Factors min 5% 50% 95% max Factors min 5% 25% 75% 75% 75% 75% 75% 75%	327 n = p = 1 1 Opt 5.85 8.25 10.05 11.1 12.6 14.55 16.65 40.5 n = p = 1 1 Opt 7.77 10.5 12.81 15.12 18.27	167.4 15 runs D Opt 6.6 8.56 10.2 11.7 13.35 15.75 28.65 21 runs D Opt 6.93 13.44 17.01	30.48 n = p + 2 I Opt 4.25 5.44 6.46 8.33 10.54 12.92 29.58 n = p + 2 I Opt 6.44 7.47 9.68	17.18 = 17 runs D Opt 6.12 8.67 10.71 12.58 14.62 16.32 17.34 23.97 = 23 runs D Opt 8.05 13.11 15.64	9.8 n = p + 4 l Opt 4.75 5.51 6.27 7.79 9.69 11.97 13.49 27.93 n = p + 4 l Opt 6 7.255	= 19 runs D Opt 6.49 8.36 9.88 11.21 12.92 14.25 15.39 23.75 = 25 runs D Opt 9.25 13 15.5	n = 2p = 1 Opt 4.5 4.5 4.5 5.4 6.9 8.7 10.8 12.3 24.6 n = 2p = 1 Opt 5.04 6.4 6.4 6.7 6.4 6.7	30 runs D Opt 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Factors min 5% 50% 95% max Factors min 5% 95% 50% 95% 50% 95% 95% 95% 95% 95% 95% 95% 95% 95% 95	327 n = p = 1 1 Opt 5.85 8.25 11.1 12.6 14.55 16.65 40.5 n = p = 1 1 Opt 7.77 10.5 12.81 15.12 18.27 22.68	167.4 15 runs D Opt 6.6 8.55 10.2 11.7 13.35 15.75 17.55 28.65 21 runs D Opt 6.93 13.44 17.01 19.53	30.48 n = p + 2 Opt	17.16 = 17 runs D Opt 6.12 8.67 10.71 12.58 14.62 17.34 23.97 = 23 runs D Opt 8.05 13.11 15.64 17.25	9.88 n = p + 4 l Opt 4.75 5.51 6.277 7.79 9.69 11.97 13.49 27.93 n = p + 4 l Opt 6 7.25 9 11.25	= 19 runs D Opt 6.46 8.36 9.88 11.21 12.92 14.25 15.39 23.75 = 25 runs D Opt 9.25 13 15.56 17.51	n = 2p = 1 Opt 4.5 4.5 4.5 5.4 6.9 8.7 10.8 12.3 12.4 6 1 Opt 5.04 5.46 7.14 9.24	30 runs D Opt 11 12 15 18 18 42 runs D Opt 10. 13.
Factors min 5% 50% 95% max Factors min 5% 25% 75% 75% 75% 75% 75% 75%	327 n = p = 1 1 Opt 5.85 8.25 10.05 11.1 12.6 14.55 16.65 40.5 n = p = 1 1 Opt 7.77 10.5 12.81 15.12 18.27	167.4 15 runs D Opt 6.6 8.56 10.2 11.7 13.35 15.76 17.55 28.65 21 runs D Opt 6.93 13.44 17.01 19.53 22.68	n = p + 2 1 Opt 4.25 5.44 6.46 8.33 10.54 12.92 14.79 29.58 n = p + 2 1 Opt 6.44 7.59 9.66 11.96 14.95	17.16 = 17 runs D Opt 6.12 8.67 10.71 12.58 14.62 16.32 17.34 23.97 = 23 runs D Opt 8.05 13.11 15.64 17.25 19.09	9.8 n = p + 4 1 Opt 4.75 5.51 6.27 7.79 9.69 11.97 13.49 27.93 n = p + 4 1 Opt 6 7.25 9 11.25 13.5	= 19 runs D Opt 6.46 8.36 9.88 11.21 12.92 14.25 15.39 23.75 = 25 runs D Opt 9.25 13 15.5 17.55 19.5	n = 2p = 1 Opt 4.5 4.5 4.5 6.4 6.9 8.7 10.8 12.3 24.6 17.14 5.46 7.14 9.24 11.34	30 runs D Opt 11 12 13 15 18 42 runs

technique and investigates the robustness of the designs to the choice of surrogate model fitted. That is, we consider the performance of the designs with respect to not only the polynomial model, but also the Gaussian process (GASP model). Trade-offs between design and modeling choices are illustrated in the ex-

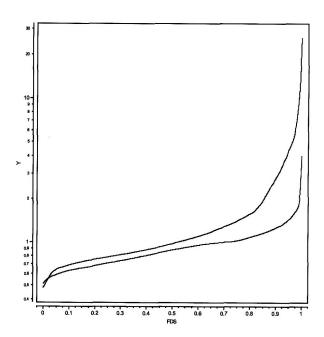
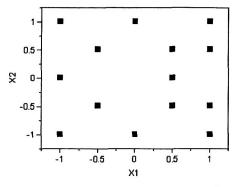


FIGURE 4. FDS Plots of the *I*-Optimal Design (Figure 3a) and LHD (Figure 3b). In this figure, the LHD is the design with the poorer prediction variance. Note: the log scale is used for the *y*-axis.

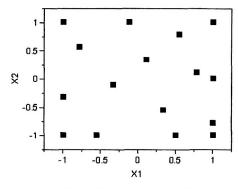
ample through a study of the theoretical integrated prediction variances and empirical mean-square error.

Case Study

In this section, we present a case study relating to a NASA-sponsored air-breathing propulsion experiment. Theoretical prediction variance of the pure de-



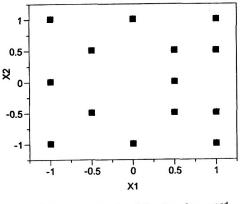
a)16 Run I-Optimal Design for a 3rd order polynomial Model



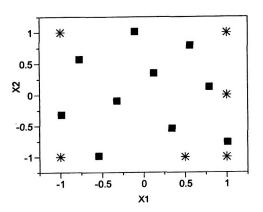
b) 16 Run Augmented Latin Hypercube Design for a 3rd order polynomial Model

FIGURE 3. Two Designs Each with 2 Factors and 10 Runs Designed for a Third-Order Polynomial. Figure 3a contains an *I*-optimal design and Figure 3b is an LHD.

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b) 16 Run Augmented Latin Hypercube Design for a 3rd order polynomial Model

FIGURE 5. Two 16-Run 2-Factor Designs for a Third-Order Polynomial Model.

sign and an augmented hybrid design are considered. Additionally, empirical mean square error of the designs is calculated by using the surrogate model to predict points not in the original design. The simulation results are based on a computational fluid dynamics (CDF) model built to mimic the flow-field parameters within an open jet flame. Because the CFD is not available for commercial use, we created a mathematical model that predicts the CFD accurately to four decimal places. The physical experiment on which the CFD is based is described in Johnson et al. (2009). In the example in this section, we are interested in modeling response, oxygen, as a function of two input factors: x- and y-axis location. See Figure 7, which displays a surface profile plot of the function.

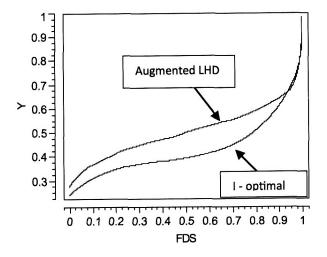


FIGURE 6. FDS Plots of Designs in Figure 5.

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While the output response is expected to be modeled by a third-order polynomial model, we also consider the GASP model. Note that we expect a third-order model to provide a good fit to the data, but because we are using a mathematical model in place of the CFD, we know that the true underlying function is neither polynomial nor a Gaussian process. We compared three designs: the maximin Latinhypercube design, the augmented maximin Latinhypercube design, and the *I*-optimal design. The Latin-hypercube design was chosen because is has good performance with respect to the kriging model and it is a staple in the computer-simulation literature.

Augmentation Technique

The hybrid design strategy that we propose is based on the design-augmentation technique described below:

Step 1: Assume that the total design size is $N = n_1 + n_2$.

Start with n_1 points using some space-filling design. Collect data at each of the n_1 points

design. Collect data at each of the n_1 points and find and fit an adequate polynomial model.

Step 2: Augment the space-filling design with n_2 points using a polynomial variance criterion.

The degree of the polynomial and important terms can be influenced by the fit in step 1.

Theoretical Integrated Variance

In this subsection, we evaluate the theoretical performance of the designs in the case study. We com-

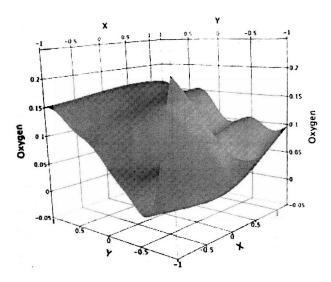


FIGURE 7. Oxygen as a Function of x- and y-Axis.

pare the designs with respect to the GASP integrated variance (IV) and the polynomial IV. The GASP prediction variance is given by the following equation:

$$\frac{\operatorname{Var}(\hat{y}(x))}{\sigma^2} = 1 - r'(x, \hat{\boldsymbol{\theta}}) R^{-1}(\mathbf{X}, \hat{\boldsymbol{\theta}}) r(x, \hat{\boldsymbol{\theta}}) + \frac{(1 - 1'R^{-1}(\mathbf{X}, \hat{\boldsymbol{\theta}}) r(x, \hat{\boldsymbol{\theta}}))^2}{1'R^{-1}(\mathbf{X}, \hat{\boldsymbol{\theta}})_1}.$$
(5)

The polynomial prediction variance equation was presented in Equation (1). Note that both the GASP IV and the polynomial IV can be computed by integrating the prediction variance equation over the design region, which is the [-1,1] hypercube. Three 18-run designs are compared. The first design is a maximin LHD, the next is an augmented maximin LHD generated with $n_1 = 12$ and $n_2 = 6$, and the third is an *I*-optimal design (optimal with respect to the third-order model in two variables). Table 5 presents the theoretical results. Note that the theoretical IV cannot directly be compared between the GASP model and the cubic polynomial model. The LHDs have the lowest expected IV with respect to

TABLE 5. Theoretical Integrated Prediction Variance for Each of Three Designs for the Gaussian Process (GASP) Model and the Cubic Polynomial

	LHD	Hybrid	I-optimal
GASP	0.009	0.0214	0.0407
Cubic	0.576	0.3999	0.365

TABLE 6. Empirical Root-Mean–Square Error for Each of Three Designs Fit Using Either the GASP Model or the Cubic Model

	LHD	Hybrid	I-optimal
GASP Cubic	0.01776 0.01983	0.01514 0.01794	0.02996 0.02488

the GASP model and the I-optimal design has the lowest IV with respect to the cubic model. The hybrid design demonstrates a compromise between the pure LHD and the pure I-optimal design. By augmenting the LHD, we see an improved performance with respect to the cubic polynomial and a degradation in performance with respect to the GASP model.

Empirical Mean-Square Error

In addition to the theoretical performance of the designs, the empirical performance is also considered. Table 6 presents the results for empirical root mean-square error (ERMSE) of the design with respect to the model used to fit the design points. In this case study, the hybrid design outperformed the other design/surrogate model combinations. While all of the values are relatively small, the results demonstrate that the hybrid LHD has the lowest ERMSE for when the design is fit to both the GASP model and the cubic polynomial model.

Conclusions

The results presented in this paper give insight into how space-filling designs perform with respect to prediction variance properties for polynomial models. The designs are compared with optimal designs, which are designed with respect to criteria pertaining to the polynomial models. Of the space-filling designs, the sphere-packing design was generally the best choice of design for minimizing the SPV for a polynomial model, followed by the Latin-hypercube design. We also introduce a new class of hybrid designs. These designs consist of a space-filling design augmented with *I*-optimal points. These designs are shown to have much improved prediction variance with respect to polynomial models.

One of the benefits of deterministic computersimulation models is the ability to build up a design sequentially, without concern for blocking or randomization. In such cases, the space-filling-hybrid design is an excellent choice. After running a preliminary set

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of runs, the experimenter has a better idea of what modeling strategy to use. At this point, the design can be augmented with a criterion that is optimal for that strategy.

While some might question the use of the spacefilling design for polynomials at all, it is important to remember that, in advance of any experimentation, it is impossible to know whether a polynomial model of any order will prove to be adequate. Using a spacefilling design for initial exploration makes sense.

The implications to the researcher are summarized in the following points: (1) space-filling designs do not perform as well as optimal designs with respect to a polynomial model, (2) of the space-filling designs, sphere-packing designs generally have the lowest prediction variance with respect to polynomials,

and (3) augment space-filling designs with *I*-optimal points whenever initial modeling indicates that the computer-simulation model can be adequately approximated by a polynomial.

Acknowledgments

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Appendix A Prediction Variance for Third-Order Models

TABLE 7 Prediction Variance Percentiles for Third-Order Models for Space-Filling Designs

- 1		n = p =	10 rune			n = p + 2 =	12 runs			n = p + 4 =	14 runs				n = 2p = 2	20 runs	
Factors	SP			ME	SP	H 1		ME	SP	LH I		ME	SP	L	H L		ME
min	5.1	4.6	4.5	5.6	4.2	4.2	4.8	4.2	4.34	4.34	4.06	5.6		3.8	4.2	4	
5%	7.6	6.5	8.1	30.2	5.76	5.64	7.2	6.24	5.6	5.6	5.6	6.02		4.8	5.2	5.2	
25%	10.1	9.1	19.8	495.9	7.44	6.96	10.44	9.12	7.14	6.86	7.56	7.14		6.4	6.4	6.6	
50%	15	12.5	39.9	2616	8.4	8.04	15.48	23.64	7.98	7.42	9.94	8.54		7	7.2	7.8	
75%	28.5	20.2	83.2	8341	9.96	9.6	24.96	76.8	9.1	10.22	17.08	11.48		7.6	10	12.4	1
90%	43.6	33.7	203.3	18879.6	11.76	15.84	63.24	179.52	10.08	19.46	37.24	45.78		9.8	16.8	24.2	3
95%	50.1	50.3	394.8	47626.9	13.08	24.72	128.4	330.12	11.34	28.98	56.42	125.02	000000000000000000000000000000000000000	11.4	23.6	37.2	
max	65.9	340.8	5308.2	177126	51.24	115.92	713.16	2940.6	38.08	89.04	392.84	1065.12		35.4	103.4	141	
		n = p = 2	20 runs			n = p + 2 =				n = p + 4 =					n = 2p = 4		
Factors	SP	LH	U	ME	-	LH I		ME	SP		U	ME	SP		H L		ME
min	9	9.4	11.2	8	7.26	8.36	9.46	8.36	7.44	8.64	7.68	6.48		5.6	6	6.4	
5%	24.6	18.2	42.8	14.2	13.42	14.74	16.28	15.84	14.88	14.4	15.12	10.8		9.2	10.4	14.8	
25%	46.6	29.6	172.8	25.8	18.26	19.58	26.62	45.98	21.12	17.28	37.92 93.6	14.16		13.2	14.8	20.8	
50%	89.4	51.8	470.8	52	23.1	26.84	46.2	185.9	26.88	21.36		21.84		15.2	24.8	41.6	
75%	190.8	100	1277.6	139.8	30.8	47.08	101.42	794.2	34.32 42	32.16 66.72	231.12 514.56	30.24		18	46	80	
90%	350.8	189	3722	355.2	41.14	120.34	275	2914.12	46.8	109.92	960.96	37.92		20.4	66.4	124.8	
95% max	447 1196.6	446.4 6293.6	6407.4 62956.4	650 3099.2	47.74 83.16	219.12 1521.52	469.7 3682.58	7767.76 121052	67.92	762.24	7399.92	116.16	0.0000000000000000000000000000000000000	56.4	314.8	593.6	
	-	n = p =	35 rups			n = p + 2 =	: 37 runs			n = p + 4	= 39 runs				n = 2p = 1	70 runs	
actors	SP			ME	SP			ME	SP	LH	U	ME	SP	I			ME
min	12.25	21	16.1	22.4	15.91	14.43	16.65	17.02	12.87	12.87	9.75			9.1	9.8	7.7	
5%	42.7	39.9	58.1	138.6	33.67	27.75	79.18	37	27.3	24.18	33.93	33.54		17.5	18.9	16.1	
25%	98	65.45	165.9	958.65	51.8	39.59	333.74	71.04	37.44	34.32	128.7	56.55	No contract and	21.7	22.4	24.5	
50%	205.8	107.45	383.6	3703.35	80.29	61.42	1001.22	129.5	48.75	53.43	349.83	92.04	12000000000000	23.8	29.4	43.4	
75%	444.85	211.75	980.7	10938.6	133.94	122.84	2942.24	265.66	65.13	101.79	886.86	175.11	P159933443433	26.6	52.5	82.6	
90%	905.45	568.4	2238.6	26606	210.9	253.45	7209.82	529.1	85.41	211.38	2023.71	376.35		30.8	95.2	150.5	
95%	1519.7	984.9	3641.75	47555.2	294.89	393.68	11912.5	789.21	99.84	336.57	3060.72	590.07		34.3	137.2	212.8	
													7055E00E003	92.4	910	1242.5	6
max	13384.7	18964.8	19146.4	230053	4460.35	2945.2	89726.9	6631.88	202.8	2906.67	14390.6	3320.85	2000000000	JZ			
		n = p = 5	56 runs			n = p + 2 =	= 58 runs		202.8	n = p + 4 :	= 60 runs				n = 2p = 1		ME
actors	SP	n = p = 5	56 runs U	ME	SP	n = p + 2 = LH	= 58 runs U	ME	202.8 SP	n = p + 4 :	= 60 runs U	ME	SP		_H \ \	J	ME
actors min	SP 43.12	n = p = 5 LH 47.04	56 runs U 44.24	ME 36.96	SP 26.68	n = p + 2 : LH 43.5	= 58 runs U 24.36	ME 34.8	202.8 SP 28.2	n = p + 4 : LH 35.4	= 60 runs U 26.4	ME 34.2	SP	11.2	_H (J 12.32	1
actors min 5%	SP 43.12 179.76	n = p = 5 LH 47.04 141.12	56 runs U 44.24 304.08	ME 36.96 110.88	SP 26.68 81.78	n = p + 2 = LH 43.5 112.52	= 58 runs U 24.36 111.94	ME 34.8 107.3	202.8 SP 28.2 60	n = p + 4 = LH 35.4 71.4	= 60 runs U 26.4 108	ME 34.2 69.6	SP 2	11.2	16.8 30.24	12.32 25.76	2
actors min 5% 25%	SP 43.12 179.76 469.28	n = p = 5 LH 47.04 141.12 441.28	56 runs U 44.24 304.08 1090.32	ME 36.96 110.88 265.44	SP 26.68 81.78 154.28	n = p + 2 = LH 43.5 112.52 348.58	= 58 runs U 24.36 111.94 322.48	ME 34.8 107.3 280.14	202.8 SP 28.2 60 88.8	n = p + 4 = LH 35.4 71.4 135	= 60 runs U 26.4 108 301.8	ME 34.2 69.6 145.2	SP	11.2 3.52 0.24	16.8 30.24 36.96	12.32 25.76 40.32	2
Factors min 5% 25% 50%	SP 43.12 179.76 469.28 913.36	n = p = 5 LH 47.04 141.12 441.28 1202.88	56 runs U 44.24 304.08 1090.32 2638.16	ME 36.96 110.88 265.44 557.2	SP 26.68 81.78 154.28 278.4	n = p + 2 = LH 43.5 112.52 348.58 984.84	= 58 runs U 24.36 111.94 322.48 752.26	ME 34.8 107.3 280.14 585.8	202.8 SP 28.2 60 88.8 123	n = p + 4 = LH 35.4 71.4 135 247.8	= 60 runs U 26.4 108 301.8 741.6	ME 34.2 69.6 145.2 284.4	SP 2 3 3 3	11.2 3.52 0.24 4.72	16.8 30.24 36.96 51.52	12.32 25.76 40.32 67.2	3
Factors min 5% 25% 50% 75%	SP 43.12 179.76 469.28 913.36 1692.88	n = p = 5 LH 47.04 141.12 441.28 1202.88 3108	56 runs U 44.24 304.08 1090.32 2638.16 6375.6	ME 36.96 110.88 265.44 557.2 1298.64	SP 26.68 81.78 154.28 278.4 531.86	n = p + 2 = LH 43.5 112.52 348.58 984.84 2669.74	= 58 runs U 24.36 111.94 322.48 752.26 1803.8	ME 34.8 107.3 280.14 585.8 1380.4	202.8 SP 28.2 60 88.8 123 175.2	n = p + 4 = LH 35.4 71.4 135 247.8 580.8	= 60 runs U 26.4 108 301.8 741.6	ME 34.2 69.6 145.2 284.4 621	SP 2 3 3 4	11.2 3.52 0.24 4.72 0.32	16.8 30.24 36.96 51.52 91.84	12.32 25.76 40.32 67.2 125.44	3
Factors min 5% 25% 50%	SP 43.12 179.76 469.28 913.36 1692.88	n = p = 5 LH 47.04 141.12 441.28 1202.88 3108 7762.16	56 runs U 44.24 304.08 1090.32 2638.16	ME 36.96 110.88 265.44 557.2 1298.64	SP 26.68 81.78 154.28 278.4	n = p + 2 = LH 43.5 112.52 348.58 984.84	= 58 runs U 24.36 111.94 322.48 752.26	ME 34.8 107.3 280.14 585.8	202.8 SP 28.2 60 88.8 123	n = p + 4 = LH 35.4 71.4 135 247.8	= 60 runs U 26.4 108 301.8 741.6	ME 34.2 69.6 145.2 284.4 621 1275	SP 2 3 3 4 4 4	11.2 3.52 0.24 4.72	16.8 30.24 36.96 51.52	12.32 25.76 40.32 67.2	ME 1 2 3 3 1 6 2 3

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TABLE 8. Prediction Variance Percentiles for Third-Order Models for Optimal Designs

		10	<u> </u>	10				-
2 Factors	I Opt	10 runs D Opt	I Opt	= 12 runs D Opt	n = p + 4	= 14 runs D Opt	n = 2p =	= 20 runs D Opt
min	5.1	5 Spt	4.56		4.48	4.62	3.8	5.2
5%	5.9	6.1	5.4		5.04	5.88	4.4	6.8
25%	7.1	8.7	6.6		6.02		5.4	8
50%	8.8	10.7	7.44		7.42	7.28	6.2	9
75%	10.3	13	8.04		8.12	7.7	7.6	10
90%	12.8	14.7	8.76		9.24	8.68	9.8	10.4
95%	14.3	15.4	9.6		10.22	9.52	11.2	10.4
max	40.1	18.7	11.28		13.16	12.46	17.2	10.8
					10.10	12.10	17.2	17
	n = p =	20 runs	n=n+2	= 22 runs	n = n + 4	= 24 runs	n = 2n =	: 40 runs
3 Factors	I Opt	D Opt	I Opt	D Opt	I Opt	D Opt	I Opt	D Opt
min	8	9	8.14	10.34	6.48	8.64	5.2	10
5%	12.4	14.4	10.34	13.42	9.6	13.44	7.6	13.2
25%	14.8	17.8	12.32	17.82	12	16.32	9.2	15.2
50%	17	20.8	14.08	22.88	13.2	18.24	10.8	16.8
75%	21.2	26.2	16.94	31.68	15.36	20.64	14	18.4
90%	26	34	20.24	41.8	18.48	23.28	16.8	20
95%	29.2	39.6	23.1	47.96	20.4	24.96	18.8	21.2
max	66.6	57.2	65.12	61.16	51.6	30.24	42	26.4
	n = p =		n = p + 2			= 39 runs	n = 2p =	70 runs
4 Factors	The second second	D Opt	I Opt	D Opt	I Opt	D Opt	I Opt	D Opt
min	12.25	18.55	13.32	14.8	10.14	13.65	6.3	16.8
5%	19.6	27.65	19.24	25.16	16.38	23.01	10.5	24.5
25%	23.8	34.65	23.68	31.45	20.28	29.25	14.7	28
50% 75%	28 34.65	41.3	27.75	36.63	23.79	33.93	18.2	30.1
90%	44.1	50.75	32.93	42.55	28.47	40.95	23.1	32.9
95%	52.15	62.65 70.7	40.7	49.95 55.13	34.32	49.53	28	35
max	131.95	105.7	193.51	82.88	39	54.6	30.8	36.4
IIIax	101.90	103.7	193.51	02.00	97.89	93.6	57.4	43.4
ı	/	-0		50				
5 Factors	n = p = 5	D Opt	n = p + 2	= 58 runs D Opt	n = p + 4	= 60 runs D Opt	n = 2p =	
min	21.28	35.28	14.5	34.8	13.8	28.2	7.84	D Opt 26.88
5%	33.6	56.56	28.42	50.46	25.2	45	15.68	40.32
25%	42	70	36.54	63.8	33.6	55.2	21.28	45.92
50%	49.84	82.88	44.08	77.14	40.8	64.8	25.76	49.28
75%	62.16	100.24	54.52	92.8	51	74.4	32.48	52.64
90%	78.4	117.6	69.02	106.72	63.6	84.6	40.32	54.88
95%	90.72	127.12	80.04	114.84	73.8	92.4	44.8	57.12
max	276.08	198.24	262.16	176.32	205.2	145.2	96.32	68.32
	0		202.10	170.02	200.2	140.2	30.32	00.32

$\begin{array}{c} \textbf{Appendix B} \\ \textbf{Prediction Variance for Fourth-Order Models} \end{array}$

TABLE 9. Prediction Variance Percentiles for Fourth-Order Models for Space-Filling Designs

		IAE	3LE 9.	Predic
		n = p =	15 runs	
2 Factors	SP	LH	U	ME
min	9.15	8.25	7.5	8.55
5%	13.5	9.9	19.5	10.95
25%	25.05	13.5	93	15.9
50%	43.5	18	381	24
75%	81.9	30.45	1459.2	49.8
90%	125.55	80.1	4535.1	101.25
95%	148.65	142.8	6958.5	133.8
max	723.9	1526.55	100142.3	246.9
3 Factors	SP	n = p =	35 runs	ME
min	19.6		20.3	20.3
5%	43.75	ECONOMISSION CONTRACTOR	46.2	42.35
25%	91.35	78.4	117.25	84.7
50%	184.45	CONTRACTOR OF STREET	271.95	182.35
75%	345.45		760.9	386.05
	527.1	1537.2	2603.3	763.7
2006				
90% 95%	663,95		5116.3	1199.45

	n = p = 70 runs								
4 Factors	SP	LH	U	ME					
min	63.7	41.3	51.8	46.9					
5%	283.5	98.7	219.8	249.2					
25%	1005.9	293.3	788.9	864.5					
50%	2943.5	833.7	2517.2	2114					
75%	7675.5	2854.6	8088.5	5134.5					
90%	15145.2	9442.3	23260.3	13273.4					
95%	20278.3	18734.1	42473.2	29230.6					
max	137232.9	246286.6	470064	820859					

		n = p = 1	126 runs	
5 Factors	SP	LH	U	ME
min	104.58	118.44	149.94	134.82
5%	1208.34	395.64	1116.36	496.44
25%	11066.58	1253.7	4315.5	1549.8
50%	45051.3	3763.62	12233.34	3693.06
75%	132699.4	12389.58	35964.18	9477.72
90%	272734.6	36169.56	92985.48	23291.1
95%	385675.9	69117.3	159935.6	39027.2
max	2476063	1066477	2256729	873213

n = p + 2 = 17 runs								
SP	LH	U	ME					
7.31	6.97	6.46	7.31					
8.16	9.35	9.52	8.67					
11.05	11.9	15.98	11.05					
14.45	15.47	23.12	13.6					
17.68	20.91	53.38	18.53					
23.29	40.46	162.69	24.14					
30.77	100.13	284.58	29.92					
88.74	1301.18	2613.41	92.14					

	n = p + 2	= 37 runs	
SP	LH	U	ME
16.28	19.98	19.98	15.54
25.9	50.69	172.79	25.53
37.37	301.55	1515.15	34.04
54.76	1152.92	7647.9	42.18
92.5	3953.45	39744.29	57.35
172.42	14236.12	162511.4	85.1
238.28	37415.14	428477.02	103.6
530.21	529365.66	11992464	430.68

SP	LH	U	ME
46.8	46.8	38.88	41.76
113.76	97.92	207.36	123.12
285.84	171.36	794.88	285.84
748.8	287.28	2354.4	527.76
1990.8	632.16	7527.6	1047.6
4134.96	2129.04	20486.16	2332.08
6264	4611.6	38268	4203.36
35667.4	136063.44	674393.04	53618.4

	n = p + 2	= 128 runs	
SP	LH	U	ME
97.28	101.12	120.32	81.92
272.64	245.76	1713.92	486.4
608	519.68	10278.4	1569.28
1162.24	1107.2	36746.24	3988.48
2241.28	3120.64	130310.4	11581.4
3747.84	8840.96	435159.04	32389.1
5053.44	16505.6	859343.36	55932.2
18741.8	371531.52	16379917	925300

	$n = p + \epsilon$	4 = 19 runs	
SP	LH	U	ME
7.6	8.17	6.27	7.41
8.93	9.12	9.5	7.98
11.02	11.4	13.11	9.69
13.68	14.06	16.72	12.35
18.24	18.24	23.37	14.82
23.75	32.3	66.31	18.05
27.74	57.19	131.67	19.57
81.89	702.62	1134.49	108.3

	n = p + 4	$4 \approx 39 \text{ runs}$	
SP	LH	U	ME
16.38	19.89	12.87	17.55
23.4	24.96	36.27	22.62
33.15	33.54	97.11	31.2
43.29	49.14	231.66	41.73
61.23	100.62	703.56	57.33
85.41	284.7	1904.76	75.27
107.25	531.57	3355.56	88.92
376.74	13378.6	43967.8	301.47

SP	LH	U	ME
40.7	44.4	31.82	38.48
71.78	84.36	111	71.78
111.74	161.32	380.36	139.12
158.36	312.28	1046.36	247.16
232.36	689.68	2959.26	503.94
330.04	2093.46	7069.96	1033.78
433.64	4849.96	12917.4	1725.68
1669.4	159974	211978	41193.6

SP	LH	U	ME
93.6	83.2	83.2	63.7
219.7	184.6	370.5	263.9
384.8	319.8	1235	711.1
568.1	552.5	3146	1604.2
841.1	1353.3	8676.2	4035.2
1192.1	3742.7	21361.6	9921.6
1467.7	6696.3	34790.6	16422.9
11617	86529.3	542974	221402

n = 2p = 30 runs						
SP	LH	U	ME			
6.9	6.6	6.6	6.9			
7.5	7.5	7.5	7.5			
9.3	9	11.4	9			
11.4	11.4	15	10.5			
13.8	15.3	23.7	13.2			
15.6	27.9	63.3	17.4			
17.4	44.1	112.5	19.5			
81.6	410.4	1499.4	82.5			

	n = 2p	= 70 runs	
SP	LH	U	ME
14	13.3	11.9	13.3
16.1	15.4	16.8	15.4
21	22.4	25.2	19.6
25.9	28.7	39.2	23.8
30.8	46.2	75.6	29.4
35	93.8	151.9	35
39.2	162.4	235.9	40.6
111.3	2429	3818.5	93.8

	n = 2p :	= 140 runs	
SP	LH	U	ME
23.8	23.8	21	23.8
30.8	30.8	33.6	29.4
39.2	44.8	49	39.2
47.6	60.2	81.2	50.4
57.4	117.6	166.6	70
70	250.6	354.2	103.6
79.8	390.6	560	142.8
236.6	2839.2	7445.2	995.4

	n = 2p	= 252 runs	
SP	LH	U	ME
42.84	45.36	32.76	37.8
52.92	63	50.4	52.92
70.56	85.68	90.72	78.12
85.68	115.92	158.76	123.48
103.3	229.32	320.04	231.84
123.5	501.48	612.36	466.2
136.1	778.68	904.68	715.68
473.8	7020.72	4394.88	6688.08

TABLE 10. Prediction Variance Percentiles for Fourth-Order Models for Optimal Designs

0.5	n = p =			= 17 runs		= 19 runs		= 30 runs
	I Opt	D Opt	I Opt	D Opt	I Opt	D Opt	I Opt	D Opt
min	8.25	7.95	8.16	8.5	8.36	6.84	6.9	alifolishing the sales of the sales
5%	10.35	10.95	9.18	10.88	9.12	11.21	7.2	11.1
25%	11.85	13.5	10.03	12.24	10.07	12.54	8.1	12.3
50%	12.9	15.3	11.39	13.43	11.4	13.3	9.9	13.2
75%	14.1	17.7	13.6	15.13	12.92	15.01	11.1	14.7
90%	15	20.85	15.98	18.87	14.25	17.1	14.4	15.9
95%	15.75	23.1	17.17	22.27	15.58	18.43	16.8	16.2
max	50.4	29.1	45.9	26.35	22.42	19.95	25.5	19.2
	n=p=			= 37 runs	n = p + 4			70 runs
3 Factors		D Opt	l Opt	D Opt	l Opt	D Opt	l Opt	D Opt
min	18.9	17.15	17.02	17.02	16.77	18.72	13.3	18.9
5% 25%	23.8	25.2	19.98	24.79	18.33	23.4	14	27.3
50%	26.25	34.3	24.42	29.97	22.62	28.47	16.8	30.1
	28.35	46.55	27.75	37	25.74	31.98	20.3	31.5
75% 90%	31.5	66.15	31.08	48.47	29.64	37.05	25.2	33.6
90%	36.05	78.4	34.78	58.83	35.88	44.07	30.8	35.7
	40.6	82.95	38.11	65.49	40.95	47.97	33.6	36.4
max	146.3	92.05	167.98	78.44	84.63	60.45	63.7	40.6
[n = p = 1			= 72 runs	n = p + 4			140 runs
4 Factors		D Opt	l Opt	D Opt	l Opt	D Opt	-	D Opt
min 5%	35	37.8	32.4	35.28	29.6	44.4	19.6	39.2
25%	44.1 50.4	65.1	38.16	58.32	35.52	56.98	22.4	54.6
50%	50.4	81.9	44.64	69.84	44.4	67.34	29.4	58.8
75%	65.8	97.3	51.84	79.92	51.06	77.7	36.4	61.6
90%	81.9	116.2 140	61.2 74.16	94.32	60.68 72.52	92.5	46.2	65.8
95%	94.5	157.5	85.68	12.32	82.14	120.62	56	70
max	323.4	277.2	328.32	240.48	217.56	201.28	64.4 123.2	72.8
max	020.4	211.2	320.32	240.48	217.50	201.28	123.2	85.4
5 Factors	n = p = 1			= 128 runs		= 130 runs	n = 2p =	
5 Factors min	I Opt 60.48	D Opt 79.38	1 Opt 55.04	D Opt		D Opt	I Opt	D Opt
5%	75.6	128.52	67.84	92.16 130.56	48.1	85.8	27.72	78.12
25%	86.94	158.76			63.7	136.5	32.76	103.32
50%	100.8	191.52	81.92	158.72	79.3	171.6	47.88	110.88
75%	126	238.14	97.28	183.04	93.6	206.7	60.48	115.92
90%	158.76	293.58	119.04	212.48	115.7	247	75.6	123.48
90%	156.76	293.58	149.76	245.76	145.6	288.6	95.76	128.52
050/	106 40	207.6	17F 00	007.50	4740	040.6	400 00	
95% max	186.48 478.8	327.6 539.28	175.36 390.4	267.52 448	171.6 438.1	313.3 471.9	108.36 178.92	133.56 156.24

$\begin{array}{c} \textbf{Appendix} \ \textbf{C} \\ \textbf{Prediction Variance for Fifth-Order Models} \end{array}$

TABLE 11. Prediction Variance Percentiles for Fifth-Order Models for Space-Filling Designs

	n = p = 21 runs				n = p + 2 = 23 runs				n = p + 4 = 25 runs			n = 2p = 42 runs				
2 Factors	SP		LJ TURS	ME	SP	LH		ME	SP	LH	U	ME	SP	LH		ME
min	13.23	17.64	11.55	10.92	8.28	10.81	9.2	8.74		8.75	9	9.25	9.24	9.24	8.4	7.50
5%	149.52	879.69	23.1	18.69	16.1	13.34	18.86	11.96	13.5	12	13.5	12.5	11.34	10.92	10.5	11.34
25%	2946.3	19463.85	49.77	40.53	36.34	17.94	45.54	15.64	15.75	15.75	25.75	16.25	13.02	12.18	13.86	16.38
50%	15259.44	71401.26	129.36	90.3	101.43	28.75	111.32	23.23	20.25	25.25	39.5	22.25	15.12	16.38	18.9	23.1
75%	44937.9	187185.6	483,21	249.69	342.7	55.66	314.87	39.33	28.25	46.75	97.75	32.25	20.16	23.52	28.56	33.18
90%	118104.8	616205.52	4902.45	1752.87	857.67	194.12	1282.48	66.93	38.25	102.25	356	45.75	25.62	48.72	65.94	90.72
95%	179711.1	4170833.31	20081.67	4100.88	1116.19	420.21	4440.84	119.14	51.25	214	779.5	61.75	28.56	87.78	120.96	242.76
max	506326.2	248090098	593927.25	204561.21	7233.04	2288.96	141624.11	608.12	4466.75	1876.75	8435	165.5	147.42	1257.48	2284.38	4552.38
								-				-				
	n = p = 56 runs			n = p + 2 = 58 runs					n = p + 4	= 60 runs		n = 2p = 112 runs				
3 Factors	SP	LH	U	ME	SP	LH	U	ME	SP	LH	U	ME	SP	LH	U	ME
min	33.6	29.68	34.72	33.04	31.32	26.68	33.06	29.58	31.8	28.2	28.8	24.6	19.04	17.92	20.16	RESIDENCE PROPERTY OF
5%	124.32	82.32	200.48	94.64	51.62	62.06	157.18	51.04	46.2	44.4	62.4	45.6	25.76	24.64	28	
25%	346.08	226.8	806.4	368.48	98.02	301.6	1064.88	89.32	70.8	78	Bright Charles and Control	100000000000000000000000000000000000000	31.36	CONTRACTOR DESCRIPTION OF THE PERSON OF THE	SECURIOR PLANTS	BEST SERVICE CONTROL
50%	778.96	708.4	3236.8	1178.8	215.76	1610.08	4636.52	175.16	115.8	151.2	777	94.2	38.08	48.16	53.76	40.32
75%	1819.44	2647.12	16870	3411.52	583.48	7699.5	19263.54	408.32	193.2		2739.6	F 25 CONTRACTOR STATE OF THE PARTY OF THE PA	52.64	78.4	112	
90%	3690.96	11039.28	68297.6	7162.4	1366.48	27347	78008.26	780.68	312		8037.6	Contraction of the Contraction o	67.2		290.08	69.44
95%	5230.4	26107.2	143396.96	9900.8	2249.82	53730.04		1050.96	423		15192.6	316.2	75.04	319.2	545.44	80.64
max	25872.56	758089.36	2139024.7	107511.04	16493.5	3843412.3	13602403	4464.26	5176.8	67502.4	252365.4	2082.6	225.12	4992.96	13533	313.6
	n = p = 126 runs			n = p + 2 = 128 runs			n = p + 4 = 130 runs			n = 2p = 252 runs SP						
4 Factors	SP	LH	U	ME	SP	LH	U	ME	SP	LH	U	ME	0,		00.04	
min	85.68	88.2	177.66	100000000000000000000000000000000000000	75.52	99.84	81.92	69.12	70.2		91 353.6	72.8 166.4	35.28 52.92	55,44	30.24 52.92	
5%	315	355.32	2707.74	100000000000000000000000000000000000000	207.36	403.2	450 E. C.		169		1471.6	100000000000000000000000000000000000000	68.04	80.64	85.68	
25%	892.08	1179.36	21297.78	SECURIOR SEC	444.16	1771.52	2795.52	1409.28	323.7	370.5	4904.9		88.2		STORES STORES	
50%	1906.38	3262.14	110243.7	2268	783.36	6224.64	9758.72		538.2 946.4	813.8 2364.7	16775.2		113.4		HARMAN STREET, SANS STREET, SAN	
75%	4204.62	10032.12	542542.14	6311.34	1413.12	20897.28 87644.16		9402.88	1567.8	9426.3	49907	3250	141.12		HONOR STANSANCE	191.52
90%	8133.3	30134.16	2009925.5		2288.64	223239.68		39828.48	2063.1	23072.4	94069.3	5586.1	158.76		1333.08	
95%	11463.48 45130.68	63653.94 8455909.14	4049973.9 81253087	328589.1	17006.1	12150177			10179		STATE OF THE PARTY		771.12		15276.2	
max	45130.00	8455909.14	61203007	320309.1	17000.1	12100111	4230402.0	303720.72	10110	1000010	TOTEGTO	000.00			BEAUTIME TO SERVICE	
											056			n - 2n -	504 rups	
r r	n = p = 252 runs Prs SP LH U ME			n = p + 2 = 254 runs SP				n = p + 4 = 256 runs SP			n = 2p = 504 runs SP LH U ME					
5 Factors	380.52		420.84		200.66		-		240.64		296.96		55,44	65.52	45.36	55.44
min 5%	2797.2	1990.8	7101.36		1805.94	1442.72			1090.56		Delication of the second	Contract Con	100.8	SECTION AND DESCRIPTION AND DE		
25%		6894.72	42139.44		5471.16	4831.08	d United States States States		3038.72	2001202-0000000000000000000000000000000	Name and Administration of the Parket of the		131.04		A SERVICE SERV	The state of the s
50%		Barrier Section Section	MERCHANIST CONTRACTOR		14879.3	13883.64	A DESCRIPTION OF THE PERSON NAMED IN		6195.2		RESIDENCE STREET		171.36		327.6	
75%			Belleville and the second second		38150.8	43058.08	Comments of the Comments of th		12815.4	200000000000000000000000000000000000000	6 postponenservania		221.76		705.E	504
90%	147034.4	CONTRACTOR DE LA CONTRA	1822716		82245.2	138739.88	ENTERNISMON AND SERVICE		24673.3		185216		282.24		1547.28	1038.24
90%	147034.4				200000000000000000000000000000000000000				_ 10,000						THE REAL PROPERTY AND PERSONS ASSESSMENT	
OF N	221947 6	207771 02	3565100 7	1200320 6	127836	288709 1	1322669 4	762142.24	36167 7	98309 12	312650.2	126855.7	322.56	2283.12	2484.72	
95% max	231847.6 1445273		3565192.7 75758337	1299329.6 31106676	127836 592958	288709.1 8632370.3	1322669.4		36167.7 220088	98309.12	Biological States of the State		1249.92		STREET, STREET	

TABLE 12. Prediction Variance Percentiles for Fifth-Order Models for Optimal Designs

		21 runs		= 23 runs	n = p + 4 =		n = 2p = 42 runs		
2 Factors	l Opt	D Opt	l Opt	D Opt		D Opt	I Opt	D Opt	
min	12.81	12.18	12.19	12.65	11.75	13.25	9.66	11.76	
5%	15.12	16.59	13.57	15.18	12.75	15.75	11.34	16.8	
25%	17.22	21	15.64	17.71	14.5	17.75	12.18	18.06	
50%	18.48	24.78	17.25	20.24	16	19.5	13.44	18.9	
75%	20.37	32.76	19.32	23.92	19	21.25	16.8	19.74	
90%	21.84	40.11	22.31	28.06	22.5	23.25	21	21	
95%	23.52	44.31	24.15	30.82	24.75	24.5	24.78	21.84	
max	98.7	49.98	38.87	36.8	69.5	31.25	38.22	26.04	
		56 runs	n = p + 2	= 58 runs	n = p + 4 =	60 runs	n = 2p = 112 runs		
3 Factors	l Opt	D Opt	l Opt	D Opt	·	O Opt	l Opt	D Opt	
min	28	31.92	30.16	31.9	28.8	28.8	16.8	32.48	
5%	40.88	48.72	37.12	42.92	36	45	23.52	43.68	
25%	46.48	59.36	43.5	52.78	40.8	52.2	26.88	48.16	
50%	50.4	71.12	48.14	59.16	45	58.2	33.6	50.4	
75%	55.44	87.92	54.52	67.86	49.8	64.2	42.56	53.76	
90%	64.96	112	63.22	77.14	57	71.4	51.52	56	
95%	75.04	131.04	71.34	83.52	63.6	75.6	58.24	57.12	
max	421.68	254.24	234.32	121.8	264	107.4	99.68	64.96	
	n = p = 1			= 128 runs	n = p + 4 =		n = 2p =	252runs	
4 Factors	I Opt	D Opt	I Opt	D Opt		O Opt	I Opt	D Opt	
min	64.26	86.94	60.16	84.48	59.8	81.9	27.72	70.56	
5%	90.72	132.3	84.48	125.44	81.9	120.9	42.84	103.32	
25%	105.84	165.06	98.56	154.88	94.9	152.1	52.92	113.4	
50%	117.18	196.56	111.36	184.32	106.6	183.3	65.52	118.44	
75%	137.34	241.92	133.12	220.16	123.5	224.9	85.68	126	
90%	167.58	296.1	165.12	258.56	150.8	275.6	105.84	131.04	
95%	194.04	332.64	189.44	281.6	171.6	308.1	120.96	133.56	
max	921.06	643.86	742.4	483.84	553.8	553.8	219.24	148.68	
[n = p = 252 runs			n = p + 2 = 254 runs		256 runs	n = 2p = 504 runs		
5 Factors	l Opt	D Opt	l Opt	D Opt		Opt		D Opt	
mìn	128.52	231.84	119.38	228.6	122.88	202.24	45.36	146.16	
min 5%	128.52 186.48	345.24	175.26	347.98	171.52	202.24 317.44	45.36 70.56	146.16 211.68	
min 5% 25%	128.52 186.48 216.72	345.24 443.52			BERTHROLD STREET, STREET, SEE	44 - 12 - 12 - 12 - 12 - 12 - 12 - 12 -			
min 5% 25% 50%	128.52 186.48 216.72 254.52	345.24 443.52 529.2	175.26 203.2 241.3	347.98 447.04 528.32	171.52 199.68 230.4	317.44	70.56	211.68	
min 5% 25% 50% 75%	128.52 186.48 216.72 254.52 317.52	345.24 443.52 529.2 637.56	175.26 203.2	347.98 447.04	171.52 199.68	317.44 399.36	70.56 95.76	211.68 226.8	
min 5% 25% 50% 75% 90%	128.52 186.48 216.72 254.52 317.52 410.76	345.24 443.52 529.2 637.56 750.96	175.26 203.2 241.3	347.98 447.04 528.32	171.52 199.68 230.4	317.44 399.36 465.92	70.56 95.76 120.96	211.68 226.8 236.88	
min 5% 25% 50% 75%	128.52 186.48 216.72 254.52 317.52	345.24 443.52 529.2 637.56	175.26 203.2 241.3 302.26	347.98 447.04 528.32 622.3	171.52 199.68 230.4 279.04	317.44 399.36 465.92 552.96	70.56 95.76 120.96 156.24	211.68 226.8 236.88 252	

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