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# NAVAL POSTGRADUATE SCHOOL Monterey, California



## THESIS

**PRELIMINARY DESIGN CODE FOR AN AXIAL STAGE  
COMPRESSOR**

by

Rizwan R. Ramakdawala

September 2001

Thesis Advisor:  
Second Reader:

Raymond P. Shreeve  
Garth V. Hobson

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**PRELIMINARY DESIGN CODE FOR AN AXIAL STAGE COMPRESSOR**

Rizwan R. Ramakdawala  
B.S., University of Maryland, College Park, 1994

Submitted in partial fulfillment of the  
requirements for the degree of

**MASTER OF SCIENCE IN AERONAUTICAL ENGINEERING**

from the

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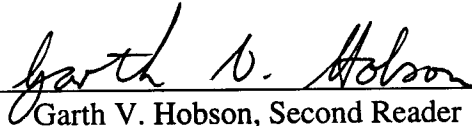


Rizwan R. Ramakdawala

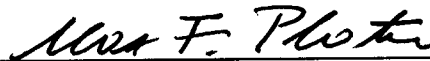
Approved by:



Raymond P. Shreeve, Thesis Advisor



Garth V. Hobson, Second Reader



Max F. Platzer, Chairman  
Department of Aeronautics and Astronautics

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## **ABSTRACT**

Current two-dimensional preliminary design codes use structured programming, which is rigid and does not allow the user to vary parameters easily. This study uses object-oriented programming to allow the user to vary all selectable parameters in a familiar Windows operating environment. The programmed design is based on the assumptions of axial and free-vortex flow between blade rows, simple radial equilibrium, and a thermally and calorically perfect gas. The program allows a fan or core stage design and uses an open architecture to facilitate upgrades and extensions.

Using the Naval Postgraduate School's (NPS) transonic compressor design as input, the preliminary design code output was compared to the detailed throughflow design of the transonic compressor. The results agreed reasonably well with detailed throughflow design. With some minor improvements this code can easily be used to develop a preliminary design that can be optimized to the user's requirements.

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## LIST OF SYMBOLS

### Symbols

$\alpha$	Absolute flow angle
$\beta$	Relative flow angle
$\delta$	Tip gap
$\delta^*$	Deviation angle
$\Phi$	Flow parameter
$\phi$	Axial velocity ratio
$\phi^*$	Camber angle
$\gamma$	Ratio of specific heats
$\eta$	Efficiency
$\iota^*$	Incidence angle
$\dot{m}$	Mass flow
$\Pi$	Total pressure ratio
$\sigma$	Solidity
$\tau$	Total temperature ratio
$\omega$	Rotor angular velocity
$\tilde{w}$	Loss coefficient
A	Area
AR	Aspect ratio
C	Chord
D	Diffusion factor
$f_\sigma$	Solidity fraction
$g^*$	Gravitational constant in units conversion
J	Mechanical equivalent of heat
H	Blade height
M	Mach number
P	Pressure
R	Gas constant or mean-line ratio
r	Radius
$r_{st}$	Degree of reaction
S	Blade spacing
T	Temperature
t/c	Thickness to chord ratio
V	Velocity in stator frame of reference
W	Velocity in rotating frame of reference
X	Velocity as a fraction of inlet limiting velocity
Y	Velocity as a fraction of the local limiting velocity
Z	Number of blades

## Subscripts

$\theta$	Tangential component
1	Inlet
2	Rotor
3	Stator
21	Ratio of rotor exit to rotor inlet
32	Ratio of stator exit to stator inlet
31	Ratio of stator exit to rotor inlet
E	Equivalent (ideal rotor outlet [Ref. 8])
H	Hub
ht	Hub-to-tip ratio
m or mn	Mean
p	Profile
R	Relative
rev	Revised
s	Shock
sftc	Secondary flow and tip clearance
T	Total
t	Tip or stagnation
U	Wheel speed component
W	Relative component
Z	Axial component



## I. INTRODUCTION

The design of a new axial compressor involves a sequence of steps, progressing through a sequence of computational programs of increasing complexity and sophistication. The first, or ‘preliminary design’ step, can be a one-dimensional ‘mean-line calculation’, or a two-dimensional calculation of a preliminary flow path and selection of the blading. The latter is the minimum required if the overall task is the preliminary design of an aircraft gas turbine engine. It is also what is required to provide the input for detailed throughflow design codes [Ref. 1], which, in turn, generate inputs to codes, which compose the blade geometry [Ref. 2] for manufacturing.

The current preliminary compressor design code used in aircraft engine design courses [Ref. 3], was developed progressively using different versions of Hewlett-Packard (HP) BASIC [Ref. 4]. This highly structured programming language is rigid and does not allow the user to vary one, or several, parameters easily in order to change or optimize a design. Use of the programs requires the installation of HP BASIC for Windows.

The purpose of the present study was to develop a preliminary compressor design code that would satisfy the following conditions:

- Be simple to use.
- Allow all selectable parameters to be changed.
- Require only the Windows operating system.
- Use an open architecture to allow upgrades (e.g., different loss models) or additions (e.g., turbine design)

To meet these conditions, Microsoft’s Visual Basic 6.0 [Ref. 5] was selected and used to develop the source code.

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## II. PROGRAM OVERVIEW

### A. ASSUMPTIONS

The following assumptions were made in the development of the programmed equations and design of the code:

- Design is for an *axial flow* compressor (with radial movement of the mean line).
- *Simple* radial equilibrium is assumed from hub to tip.
- Free vortex flow is assumed between blade rows.
- A conceptual engine design study [using Ref. 6 for example] will generate the inputs for the code.

### B. INPUTS AND OUTPUTS

The stage is shown schematically in Fig. 1, and the inputs required by the code, are shown in Table 1.

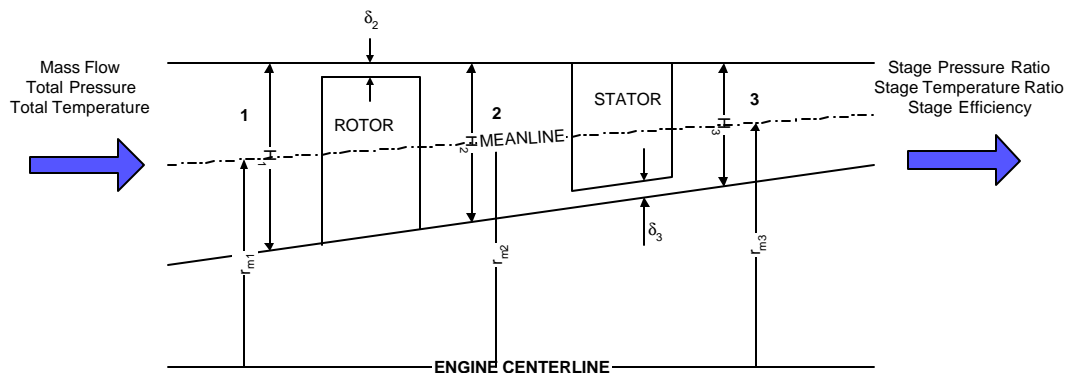


Figure 1. Throughflow Schematic

Inlet (1)	Rotor (2)	Stator (3)
$\dot{m}$	$D_{2m}$	$A_{31}$
$P_t$	$\sigma_{2m}$	$\sigma_{3m}$
$T_t$	$R_{21}$	$R_{32}$
$R$	$\phi_{21}$	$\phi_{32}$
$\gamma$	$\delta_2$	$\delta_3$
$\omega$	$AR_2$	$AR_3$
$M_{Z1t}$	$t/c_{2h}$	$t/c_{3h}$
$M_{W1t}$	$t/c_{2m}$	$t/c_{3m}$
$\alpha_{1t}$	$t/c_{2t}$	$t/c_{3t}$
	$f_{\sigma 2}$	$f_{\sigma 3}$
	$Z_2$	$Z_3$

Table 1. User-Provided Inputs

At the inlet station, it is required to specify the gas (through the gas constant and ratio of specific heats; a thermally and calorically perfect gas is assumed), the mass flow rate, and the stagnation conditions. Then, in order to accommodate the usual fan or core design constraints, four parameters must be specified for the rotor; namely, rotational speed, axial Mach number, relative Mach number, and flow angle at the tip. Only three of these four are independent. Off-line calculation is required to determine the other one.

The design selections for the rotor and stator are listed in columns two and three of Table 1. Note that the blade loading throughout the stage is determined by the selection of the diffusion factor at only one location for one blade. Blade aspect ratio and thickness variations are choices, which are determined by structural considerations. Structural constraints are not included in the program.

The parameters, which are calculated and output by the code, are shown in Table 2.

Comp.	Inlet (1)			Rotor (2)			Stator (3)		
	Hub (h)	Mean (m)	Tip (t)	Hub (h)	Mean (m)	Tip (t)	Hub (h)	Mean (m)	Tip (t)
<b>X</b>	X <sub>1h</sub>	X <sub>1m</sub>	X <sub>1t</sub>	X <sub>2h</sub>	X <sub>2m</sub>	X <sub>2t</sub>	X <sub>3h</sub>	X <sub>3m</sub>	X <sub>3t</sub>
<b>X<sub>Z</sub></b>	X <sub>Z1h</sub>	X <sub>Z1m</sub>	X <sub>Z1t</sub>	X <sub>Z2h</sub>	X <sub>Z2m</sub>	X <sub>Z2t</sub>	X <sub>Z3h</sub>	X <sub>Z3m</sub>	X <sub>Z3t</sub>
<b>X<sub>U</sub></b>	X <sub>U1h</sub>	X <sub>U1m</sub>	X <sub>U1t</sub>	X <sub>U2h</sub>	X <sub>U2m</sub>	X <sub>U2t</sub>	X <sub>U3h</sub>	X <sub>U3m</sub>	X <sub>U3t</sub>
<b>X<sub>W</sub></b>	X <sub>W1h</sub>	X <sub>W1m</sub>	X <sub>W1t</sub>	X <sub>W2h</sub>	X <sub>W2m</sub>	X <sub>W2t</sub>	X <sub>W3h</sub>	X <sub>W3m</sub>	X <sub>W3t</sub>
<b>X<sub>q</sub></b>	X <sub>θ1h</sub>	X <sub>θ1m</sub>	X <sub>θ1t</sub>	X <sub>θ2h</sub>	X <sub>θ2μ</sub>	X <sub>θ2t</sub>	X <sub>θ3h</sub>	X <sub>θ3m</sub>	X <sub>θ3t</sub>
<b>r</b>	r <sub>1h</sub>	r <sub>1m</sub>	r <sub>1t</sub>	r <sub>2h</sub>	r <sub>2m</sub>	r <sub>2t</sub>	r <sub>3h</sub>	r <sub>3m</sub>	r <sub>3t</sub>
<b>M</b>	M <sub>1h</sub>	M <sub>1m</sub>	M <sub>1t</sub>	M <sub>2h</sub>	M <sub>2m</sub>	M <sub>2t</sub>	M <sub>3h</sub>	M <sub>3m</sub>	M <sub>3t</sub>
<b>M<sub>Z</sub></b>	M <sub>Z1h</sub>	M <sub>Z1m</sub>	M <sub>Z1t</sub>	M <sub>Z2h</sub>	M <sub>Z2m</sub>	M <sub>Z2t</sub>	M <sub>Z3h</sub>	M <sub>Z3m</sub>	M <sub>Z3t</sub>
<b>M<sub>W</sub></b>	M <sub>W1h</sub>	M <sub>W1m</sub>	M <sub>W1t</sub>	M <sub>W2h</sub>	M <sub>W2m</sub>	M <sub>W2t</sub>	M <sub>W3h</sub>	M <sub>W3m</sub>	M <sub>W3t</sub>
<b>b</b>	β <sub>1h</sub>	β <sub>1m</sub>	β <sub>1t</sub>	β <sub>2h</sub>	β <sub>2m</sub>	β <sub>2t</sub>	β <sub>3h</sub>	β <sub>3m</sub>	β <sub>3t</sub>
<b>a</b>	α <sub>1h</sub>	α <sub>1m</sub>	Input	α <sub>2h</sub>	α <sub>2m</sub>	α <sub>2t</sub>	α <sub>3h</sub>	α <sub>3m</sub>	α <sub>3t</sub>
<b>Y</b>				Y <sub>2h</sub>	Y <sub>2m</sub>	Y <sub>2t</sub>	Y <sub>3h</sub>	Y <sub>3m</sub>	Y <sub>3t</sub>
<b>Y<sub>W</sub></b>				Y <sub>W2h</sub>	Y <sub>W2m</sub>	Y <sub>W2t</sub>	Y <sub>W3h</sub>	Y <sub>W3m</sub>	Y <sub>W3t</sub>
<b>D</b>				D <sub>2h</sub>	Input	D <sub>2t</sub>	D <sub>3h</sub>	D <sub>3m</sub>	D <sub>3t</sub>
<b>s</b>				σ <sub>2h</sub>	Input	σ <sub>2t</sub>	σ <sub>3h</sub>	Input	σ <sub>3t</sub>
<b>r<sub>st</sub></b>				r <sub>st2h</sub>	r <sub>st2m</sub>	r <sub>st2t</sub>	r <sub>st3h</sub>	r <sub>st3m</sub>	r <sub>st3t</sub>
<b>i*</b>				ι* <sub>2h</sub>	ι* <sub>2m</sub>	ι* <sub>2t</sub>	ι* <sub>3h</sub>	ι* <sub>3m</sub>	ι* <sub>3t</sub>
<b>f*</b>				φ* <sub>2h</sub>	φ* <sub>2m</sub>	φ* <sub>2t</sub>	φ* <sub>3h</sub>	φ* <sub>3m</sub>	φ* <sub>3t</sub>
<b>d*</b>				δ* <sub>2h</sub>	δ* <sub>2m</sub>	δ* <sub>2t</sub>	δ* <sub>3h</sub>	δ* <sub>3m</sub>	δ* <sub>3t</sub>
<b>r<sub>ht</sub></b>		r <sub>ht1</sub>			r <sub>ht2</sub>			r <sub>ht3</sub>	
<b>A</b>		A <sub>1</sub>			A <sub>2</sub>			A <sub>3</sub>	
<b>T/T<sub>t1</sub></b>		T <sub>1</sub> /T <sub>t1</sub>			T <sub>2</sub> /T <sub>t1</sub>			T <sub>3</sub> /T <sub>t1</sub>	
<b>P/P<sub>t1</sub></b>		P <sub>1</sub> /P <sub>t1</sub>			P <sub>2</sub> /P <sub>t2</sub>			P <sub>3</sub> /P <sub>t3</sub>	
<b>T<sub>t</sub>/T<sub>t1</sub></b>					T <sub>t2</sub> /T <sub>t1</sub>			T <sub>t3</sub> /T <sub>t1</sub>	
<b>P<sub>t</sub>/P<sub>t1</sub></b>					(τ) P <sub>2</sub> /P <sub>t1</sub>			P <sub>t3</sub> /P <sub>t1</sub>	
<b>A/A<sub>1</sub></b>					A <sub>2</sub> /A <sub>1</sub>			A <sub>3</sub> /A <sub>1</sub>	
<b>W<sub>p</sub></b>					ω <sub>p2</sub>			ω <sub>p3</sub>	
<b>W<sub>sftc</sub></b>					ω <sub>sftc2</sub>			ω <sub>sftc3</sub>	
<b>W<sub>s</sub></b>					ω <sub>s2</sub>			ω <sub>s3</sub>	
<b>W<sub>T</sub></b>					ω <sub>T2</sub>			ω <sub>T3</sub>	
<b>F</b>					Φ <sub>2m</sub>			Φ <sub>3m</sub>	
<b>H</b>					H <sub>2</sub>			H <sub>3</sub>	
<b>C</b>					C <sub>2</sub>			C <sub>3</sub>	
<b>S</b>					S <sub>2</sub>			S <sub>3</sub>	
<b>Z<sub>rev</sub></b>					Z <sub>rev2</sub>			Z <sub>rev3</sub>	
<b>AR<sub>rev</sub></b>					AR <sub>rev2</sub>			AR <sub>rev3</sub>	
<b>C<sub>rev</sub></b>					C <sub>rev2</sub>			C <sub>rev3</sub>	

Table 2. Outputs

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### III. ALGORITHMS

#### A. PROGRAM SEQUENCE

The overall program sequence is shown in Fig. 2. After the program is started a “splash” screen is first shown. A splash screen is an introductory screen (similar to an “about” screen) which states the name, owner(s), and version of the program. Next, an interactive screen appears, giving the user a choice of either going through a compressor design or a turbine design. The scope of this paper covers only a compressor design; therefore the turbine option has been disabled. When the *Compressor Design* button is pressed the input screen will appear. The design sequence is shown in Fig. 3. The required inputs are shown in Table 1. Once the inputs are typed in the user presses the *OK* button and the main screen appears. The main screen is laid out in a tab format with five tabs. The tabs are as follows:

- Inlet Conditions (1)
- Rotor Calculations (2)
- Stator Calculations (3)
- Stage Performance
- Blade Geometry

This allows the variables and code to be grouped so the user can better understand what is being displayed. It also allows the programmer to develop the code with an open architecture for easy updates. At this point the user can still modify the inputs before executing the design calculations.

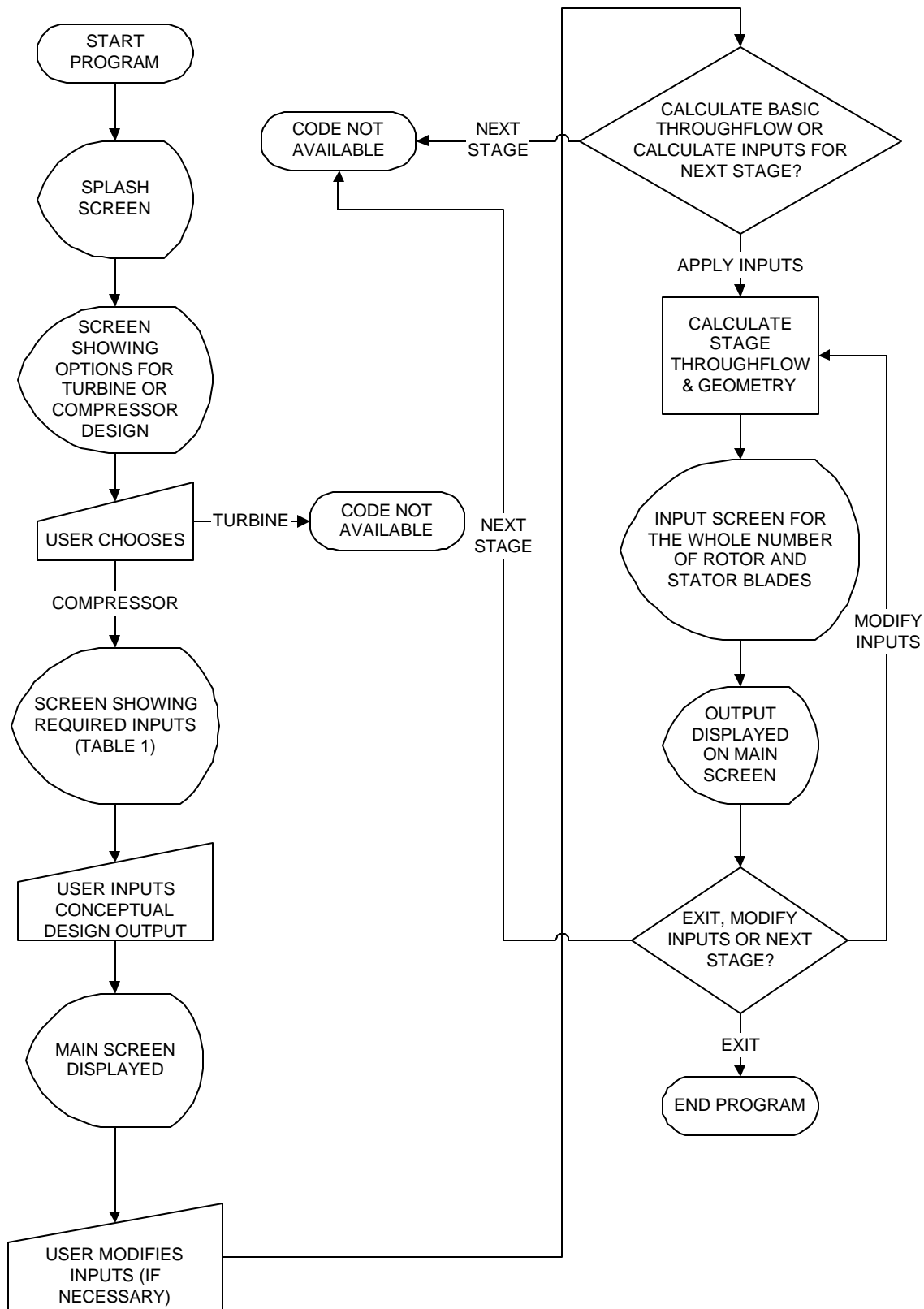


Figure 2. Main Program Flowchart



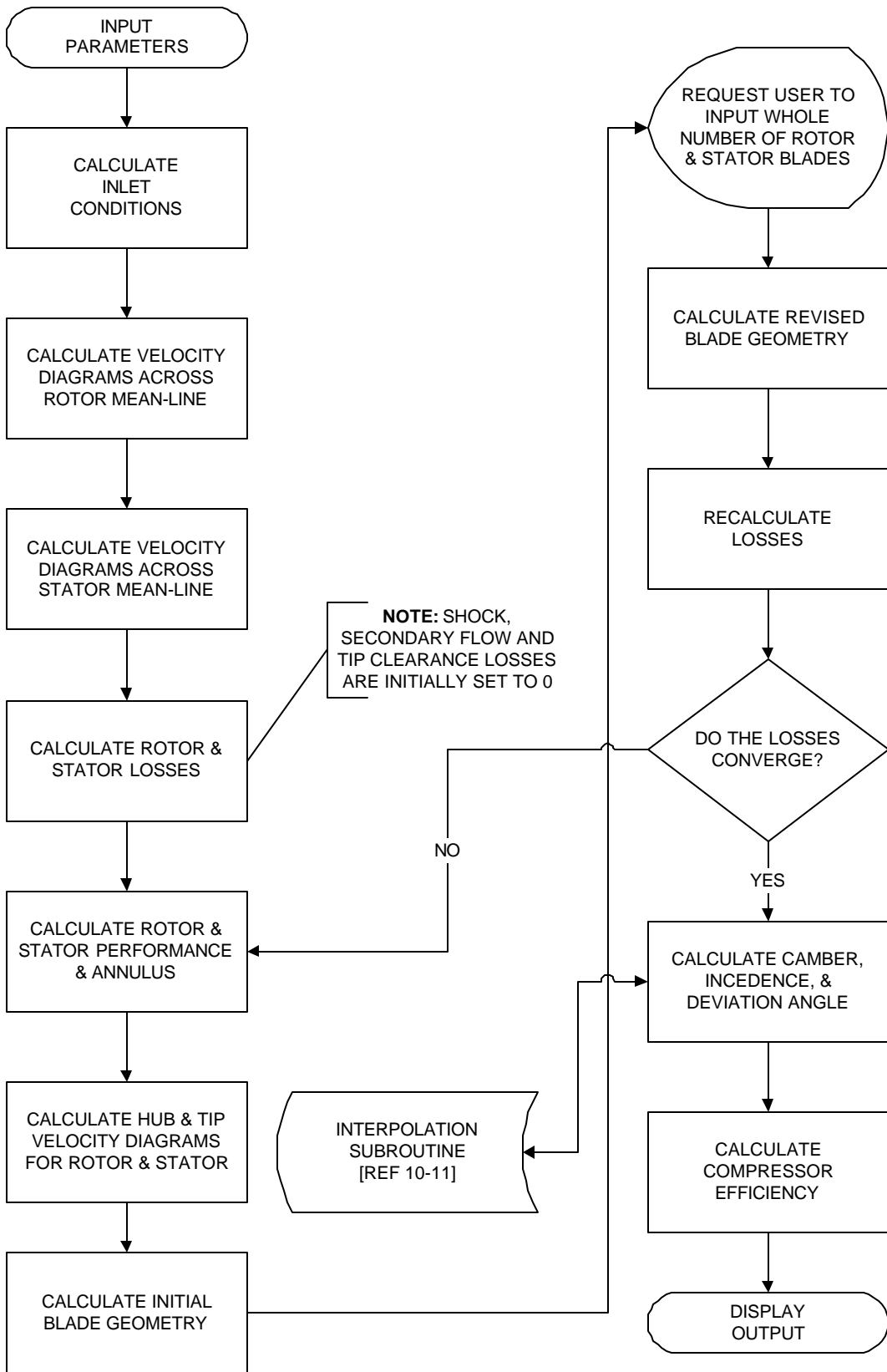


Figure 3. Design Flowchart

The user has the option to either apply the inputs to the design calculations or calculate the next stage. A multistage approach is also outside the scope of this paper so this option has been disabled. After the user presses the *Apply* button the program calculates the basic throughflow velocity diagrams, losses, performance and geometry. During the throughflow calculations an input screen is displayed for the user to input the whole number of blades needed ( $Z$ ) for the rotor and stator. The main screen is displayed again with the outputs filled in the text boxes. The outputs are shown in Table 2. With the initial throughflow calculations complete the user may end the program or modify the inputs until the desired results are achieved.

## **B. DESIGN EQUATIONS**

The equations programmed in the source code are listed in Appendix A. The equations are grouped the same as the tabs on the main screen. The equations for the velocity diagrams, profile loss, secondary flow loss, tip clearance loss, and stage performance are from Shreeve [Ref. 7 and 8]. The shock loss equation is from Koch and Smith [Ref. 9].

The incidence, deviation and camber angles (which relate the flow angles to the blade geometry, as shown in Fig. 4) were derived from NASA SP-36 [Ref. 10]. Sixth degree polynomial curvefits were used to approximate the data in Figs. 137, 138, 142, 161, 162, 168, 172, 178, 179, and 180 of Ref. 10. An interpolation routine [Ref. 11], was programmed to solve for unknowns within the curve-fits.

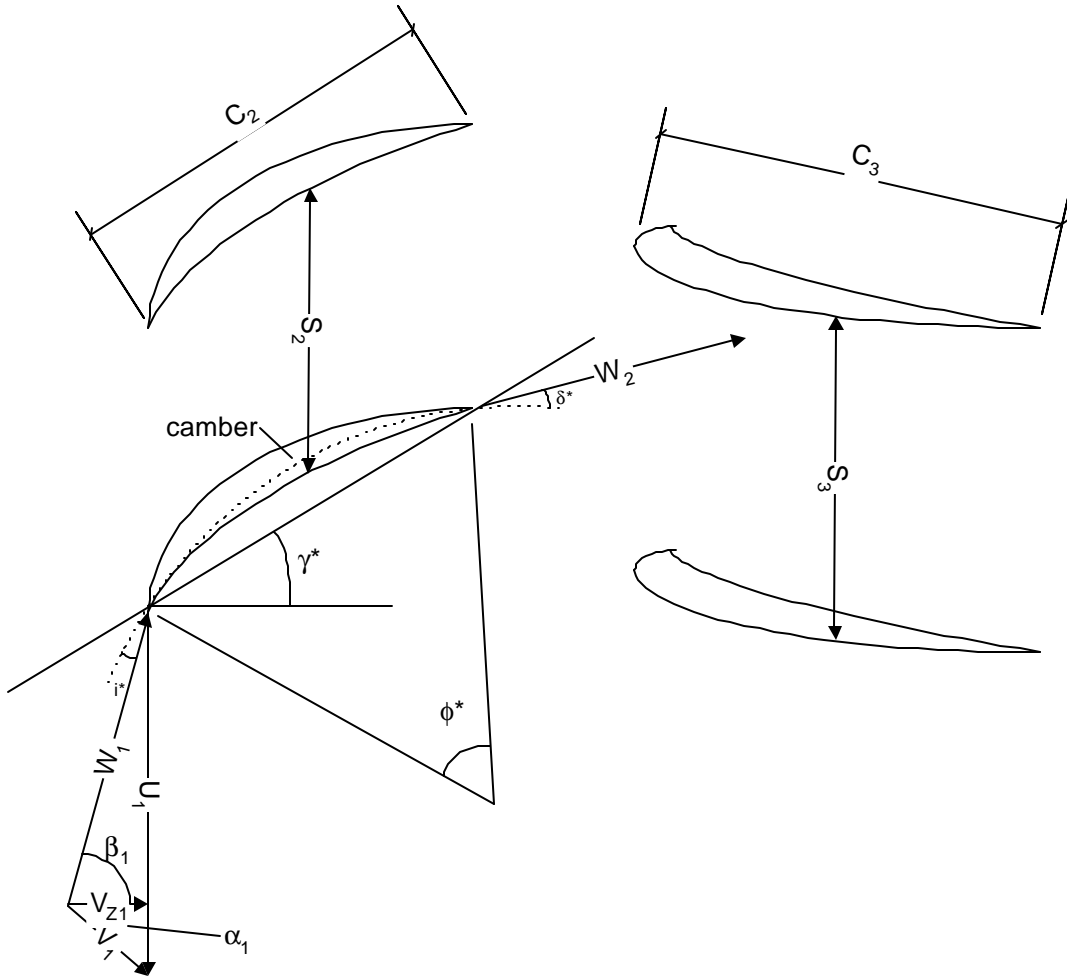


Figure 4. Blade Geometry Schematic

The performance of the stage is calculated following the thermodynamic process shown in Fig. 5. The conditions on the mean line are taken as being representative of the stage; however, the loss coefficients include contributions due to secondary flow and tip-clearance.

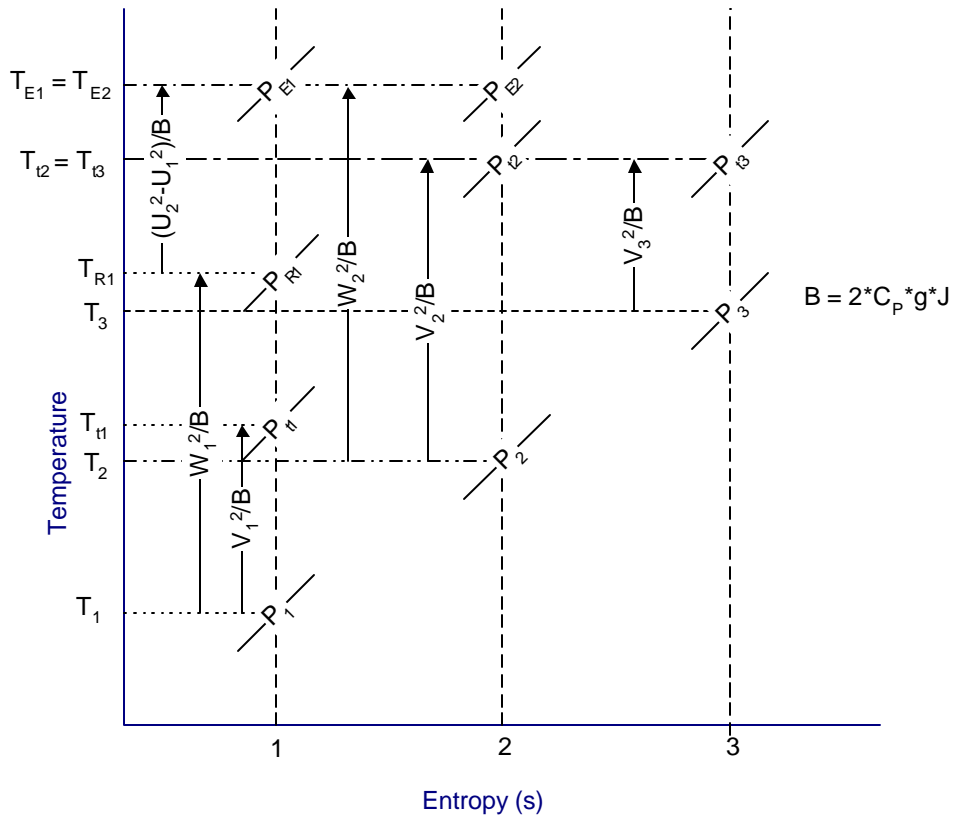


Figure 5. T-s Diagram for a Compressor Stage

## IV. PROGRAM STRUCTURE

### A. OBJECTS

Forms (a.k.a. screens) are used to interact with the user. Forms are ‘objects’ in Visual Basic and Visual C++ programming. Other common objects include text boxes, option boxes and tabs. Objects have properties (this is how the object looks to the user) which can be affected during design or run time (program execution). The objects allow the user to modify the inputs throughout the program and either executes the desired modification or keeps the original inputs. The objects (or “screen captures”) are shown in Appendix B.1.

### B. VARIABLES

Variables are used in programming as placeholders of data where they are used throughout the code to execute statements. Two-dimensional arrays are used extensively throughout the code since they allow a parameter that changes both throughflow and spanwise to be stored in one variable. For example,  $X_w$  (relative velocity) varies from inlet (1) to stator (3) and from hub (1) to tip (3). If we store this variable separately we would need to track nine variables. Instead, we simply track one variable  $X_w(3,3)$  where the first number is the throughflow number and the second number is the spanwise number. Appendix B.2 shows all the variables used in the program. This includes all the input and output parameters as well as others that are not seen by the user.

### C. MODULES

Code is used to state what needs to be executed. The code syntax is based on BASIC, which translates “pseudo” language to machine language. Code is written for objects to tell the object what to do when acted upon by the user. For this program there is very little code for objects. Most of the code is a sequence of design equations which do not cause changes in any objects and require minimal interaction with the user during execution. Modules are used in this situation. Modules take subroutines or functions that do not affect an object and keep them in a separate file for easier reading during

programming or debugging. The code, under the form 'frmCompressor', is the design code sequence shown in Figure 2. Appendix B.3 shows all the source code for the program.

## V. RESULTS AND DISCUSSION

Sanger's transonic compressor design [Ref. 13] was used to test the ability of the code to approximate a known axial stage design. A set of hand calculations was also carried out independently of the code in order to both validate the coding, and to document the test case. The design input flow conditions, and parameters derived from the final geometry of the Sanger design, were used as inputs to both the preliminary design code and hand calculations. Appendix C.1 and Appendix C.2 document, in detail, the results of the hand calculations and the preliminary design code, respectively.

The results from hand calculations and from the code were compared to the output of the streamline curvature code applied to the Sanger design, which is given in Appendix E of Sanger [Ref. 13]. The comparisons are shown in Appendix D. It can be seen from the comparison charts in Appendix D that the hand calculations agreed fully with the preliminary design code calculations. Also, for most parameters, the hand and preliminary design code calculations agreed with the streamline curvature code outputs. In Figure D1, the calculated annulus geometry agrees well at the inlet and then begins to deviate somewhat through the stage. This is because the streamline curvature code takes into account blockage, whereas the preliminary design code and hand calculations, do not. This is easy to correct. The stage performance however, shown in Fig. D2, is predicted very successfully by the code. In Fig. D3 and D4, the differences in solidity and blade height are also, indirectly, the result of omitting blockage from the calculation of annulus area. Velocity diagram details are compared in Figs. D5 to D8. It is clear that the preliminary design code reproduces the final design values to very acceptable accuracy.

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## VI. CONCLUSIONS AND RECOMMENDATIONS

From the comparisons given in Appendix D, it can be seen that the preliminary design code does very well in developing the velocity diagrams and the initial blading geometry necessary for a detailed throughflow design and final geometry calculation [Ref. 3 and 4].

Improvements can be made in order to have the design more detailed as well as improve the code's usability. They are as follows:

- Add the ability to do a multi-stage design (use the output of the previous stage as an input to the new stage).
- Add different input screens for specific design cases (e.g., fan or core).
- Add stress limits (hoop and centrifugal) for fan design.
- Add blockage and bleed to the throughflow calculations.
- Draw scale velocity diagrams.
- Draw blades based on code output (i.e., built in geometry package).
- Add parametric analysis for a range of values (e.g., inlet flow angle).
- Add turbine stage design (in parallel).
- Add the ability to open and save data.
- Add the ability to print the user's results.
- Compile the code into a stand-alone executable.

Incorporation of these improvements will make the code a preliminary turbomachine design software package that can be used as inputs to detailed design packages, as well as providing a needed teaching tool for aircraft engine design.

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## APPENDIX A. DESIGN EQUATIONS

A.1 shows the throughflow equations and A.2 shows the interpolation equations for the incidence, camber and deviation angles.

### A.1. THROUGHFLOW EQUATIONS

#### 1. Inlet Conditions

Given:  $\dot{m}$ ,  $P_t$ ,  $T_t$ ,  $M_{w1t}$ ,  $\omega$ ,  $R$ ,  $\gamma$

Vary:  $M_{z1t}$  ( $\equiv \beta_{1t}$ ),  $\alpha_{1t}$  ( $0 \leq \alpha_{1t} < \beta_{1t}$ )

$$\text{Where: } \beta_{1t} = \cos^{-1} \left( \frac{M_{z1t}}{M_{w1t}} \right)$$

$$M_{1t} = \frac{M_{z1t}}{M_{w1t}}$$

$$X_{1t} = \sqrt{\frac{\frac{\gamma-1}{2} M_{1t}^2}{1 + \frac{\gamma-1}{2} M_{1t}^2}}$$

$$X_{z1t} = X_{1t} \cdot \cos \alpha_{1t}$$

$$X_{\theta 1t} = X_{z1t} \cdot \tan \alpha_{1t}$$

$$X_{u1t} = X_{\theta 1t} + X_{z1t} \cdot \tan \beta_{1t}$$

$$\rho_{t1} = \frac{P_t}{R \cdot T_t}$$

$$V_{t1} = \sqrt{2 \cdot C_p \cdot g \cdot T_t}, \text{ where } C_p = \left( \frac{\gamma}{\gamma-1} \right) \cdot R$$

$$A_{1t} = \left( \frac{\dot{m}}{\rho_{t1} \cdot V_{t1}} \right) \cdot \frac{1}{\Phi_{1t} \cdot \cos \alpha_{1t}}, \text{ where } \Phi_{1t} = X_{1t} (1 - X_{1t}^2)^{\frac{1}{\gamma-1}}$$

$$r_{1t} = \frac{X_{u1t} \cdot V_{t1}}{\omega}$$

$$r_{1h} = \sqrt{r_{1t}^2 - \frac{A_{1t}}{\pi}}$$

$$r_{ht1} = \frac{r_{1h}}{r_{1t}}$$

$$r_{1m} = \frac{r_{1t} + r_{1h}}{2}$$

$$\text{Due to Radial Equilibrium} \begin{cases} X_{\theta 1m} = \frac{r_{1t}}{r_{1m}} \cdot X_{\theta 1t} \\ X_{Z1m} = X_{Z1t} \end{cases}$$

$$\therefore \alpha_{1m} = \tan^{-1} \left( \frac{X_{\theta 1m}}{X_{Z1m}} \right) = \tan^{-1} \left[ \frac{r_{1t}}{r_{1m}} \cdot \tan \alpha_{1t} \right]$$

$$X_{U1m} = \frac{r_{1m}}{r_{1t}} \cdot X_{U1t} \text{ for constant } \omega$$

$$\therefore \beta_{1m} = \tan^{-1} \left( \frac{X_{U1m} - X_{\theta 1m}}{X_{Z1m}} \right)$$

$$X_{1m} = \frac{X_{Z1m}}{\cos \alpha_{1m}}, M_{1m} = \sqrt{\frac{\frac{2}{\gamma-1} \cdot X_{1m}^2}{1 - X_{1m}^2}}$$

$$X_{W1m} = \frac{X_{Z1m}}{\cos \beta_{1m}}, M_{W1m} = \sqrt{\frac{\frac{2}{\gamma-1} \cdot X_{1m}^2}{1 - X_{1m}^2}}$$

## 2. Rotor Across the Mean Line

Assume:  $D_{2m}$ ,  $\sigma_{2m}$ ,  $R_{21} \equiv \frac{r_{2m}}{r_{1m}}$  (pitch of mean line),  $\phi_{21} \equiv \frac{V_{Z2}}{V_{Z1}}$  (change in axial velocity)

$$\text{Where: } D_{2m} = 1 - \phi_{21} \cdot \frac{\cos \beta_{1m}}{\cos \beta_{2m}} + \frac{(\tan \beta_{1m} - R_{21} \cdot \phi_{21} \cdot \tan \beta_{2m}) \cdot \cos \beta_{1m}}{(1 + R_{21}) \cdot \sigma_{2m}}$$

Solve for  $\beta_{2m}$

$$X_{U2m} = R_{21} \cdot X_{U1m}$$

$$\phi_{2m} = \phi_{21} \cdot \phi_{1m} \cdot \left( \frac{1}{R_{21}} \right), \text{ where } \phi_{1m} = \frac{X_{Z1m}}{X_{U1m}}$$

$$X_{Z2m} = \phi_{2m} \cdot X_{U2m}$$

$$X_{\theta 2m} = X_{U2m} - X_{Z2m} \cdot \tan \beta_{2m}$$

$$\alpha_{2m} = \tan^{-1} \left( \frac{X_{\theta 2m}}{X_{Z2m}} \right)$$

$$r_{sm} = \left[ 1 - \frac{1}{2} \left( \frac{X_{\theta 1m}}{X_{U1m}} + \frac{X_{\theta 2m}}{X_{U2m}} \right) \right]$$

$$\tau = 1 + 2 [X_{U2m} \cdot X_{\theta 2m} - X_{U1m} \cdot X_{\theta 1m}]$$

$$X_{2m} = \frac{X_{Z2m}}{\cos \alpha_{2m}}$$

$$X_{W2m} = \frac{X_{Z2m}}{\cos \beta_{2m}}$$

$$Y_{2m} = \frac{X_{2m}}{\sqrt{\tau}}$$

$$Y_{W2m} = \frac{X_{W2m}}{\sqrt{\tau}}$$

$$M_{2m} = \sqrt{\frac{\frac{2}{\gamma-1} \cdot Y_{2m}^2}{1-Y_{2m}^2}}$$

$$M_{W2m} = \sqrt{\frac{\frac{2}{\gamma-1} \cdot Y_{W2m}^2}{1-Y_{W2m}^2}}$$

### 3. Stator Across the Mean Line

$$\text{Assume: } \sigma_{3m}, R_{32} = \frac{R_{3m}}{R_{2m}}, \phi_{32} = \frac{V_{Z3}}{V_{Z2}}$$

Set  $\alpha_{3m} = A_{31} \cdot \alpha_{1m}$  (this allows for non-repeating stage calculations)

$$\text{Then: } D_{3m} = 1 - \phi_{32} \cdot \frac{\cos \alpha_{2m}}{\cos \alpha_{3m}} + \frac{(\tan \alpha_{2m} - R_{32} \cdot \phi_{32} \cdot \tan \alpha_{3m}) \cdot \cos \alpha_{2m}}{(1 + R_{32}) \cdot \sigma_{3m}}$$

$$X_{Z3m} = \phi_{32} \cdot X_{Z2m}$$

$$X_{\theta 3m} = X_{Z3m} \cdot \tan \alpha_{3m}$$

$$X_{U3m} = X_{U2m} \cdot R_{32}$$

$$\beta_{3m} = \tan^{-1} \left( \frac{X_{U3m} - X_{\theta 3m}}{X_{Z3m}} \right)$$

$$X_{3m} = \frac{X_{Z3m}}{\cos \alpha_{3m}}$$

$$X_{W3m} = \frac{X_{Z3m}}{\cos \beta_{3m}}$$

$$Y_{3m} = \frac{X_{3m}}{\sqrt{\tau}}$$

$$Y_{W3m} = \frac{X_{W3m}}{\sqrt{\tau}}$$

$$M_{3m} = \sqrt{\frac{\frac{2}{\gamma-1} \cdot Y_{3m}^2}{1-Y_{3m}^2}}$$

$$M_{W3m} = \sqrt{\frac{\frac{2}{\gamma-1} \cdot Y_{W3m}^2}{1 - Y_{W3m}^2}}$$

#### 4. Rotor Performance

Initially set  $\tilde{\omega}_{SFTC_2}, \tilde{\omega}_{S_2} = 0$

On subsequent iterations  $\tilde{\omega}_{SFTC_2}$  and  $\tilde{\omega}_{S_2}$  are

$$\beta_{\infty} = \tan^{-1} \left[ \left( \frac{\tan \beta_{1m} + \tan \beta_{2m}}{2} \right) \right]$$

$$C_L = \frac{2}{\sigma_{2m}} \cdot (\tan \beta_{1m} - \tan \beta_{2m}) \cdot \cos \beta_{\infty}$$

$$C_{Dx} = \frac{1}{4} \cdot C_L^2 \cdot \sigma_{2m} \cdot \left( \frac{\delta_2}{H_2} \right) \cdot \frac{1}{\cos \beta_{\infty}} + 0.04 \cdot C_L^2 \cdot \sigma_{2m} \cdot \left( \frac{S_2}{H_2} \right)$$

$$\tilde{\omega}_{SFTC_2} = C_{Di} \cdot \frac{\cos^2 \beta_{1m}}{\cos^3 \beta_{\infty}} \cdot \sigma_{2m}$$

$$y^* = \frac{1}{4 \cdot \gamma \cdot M_{W1m}^2} \left[ (\gamma+1) \cdot M_{W1m}^2 - (3-\gamma) + \sqrt{(\gamma+1) \cdot \{(\gamma+1) \cdot M_{W1m}^2 - 2 \cdot (3-\gamma) \cdot M_{W1m}^2 + \gamma + 9\}} \right]$$

$$\frac{P_{te}}{P_{ti}} = \left[ \frac{\gamma+1}{2 \cdot \gamma \cdot M_{W1m}^2 \cdot y^* - (\gamma-1)} \right]^{\frac{1}{\gamma-1}} \cdot \left[ \frac{(\gamma+1) \cdot M_{W1m}^2 \cdot y^*}{2 + (\gamma-1) \cdot M_{W1m}^2 \cdot y^*} \right]^{\frac{\gamma}{\gamma-1}}$$

$$\tilde{\omega}_{S_2} = \frac{P_{Ri} - P_{Re}}{P_{Ri} - P_{ti}} = \frac{1 - P_{Re}/P_{Ri}}{1 - P_{ti}/P_{Ri}} = \frac{1 - P_{te}/P_{ti}}{1 - \left[ 1 + \frac{\gamma-1}{2} \cdot M_{W1m}^2 \right]^{\frac{\gamma}{\gamma-1}}}$$

$$\tilde{\omega}_{P_2} = 2 \cdot \sigma_{2m} \cdot \frac{\cos^2 \beta_{1m}}{\cos^3 \beta_{2m}} \cdot [0.005 + 0.16 \cdot D_{2m}^4]$$

$$\tilde{\omega}_{T_2} = \tilde{\omega}_{P_2} + \tilde{\omega}_{SFTC_2} + \tilde{\omega}_{S_2}$$

$$\frac{T_1}{T_{t1}} = 1 - X_{1m}^2$$

$$\frac{P_1}{P_{t1}} = \left( \frac{T_1}{T_{t1}} \right)^{\frac{\gamma}{\gamma-1}}$$

$$\frac{T_{R1}}{T_{t1}} = \left( \frac{T_1}{T_{t1}} \right) + X_{W1m}^2$$

$$\frac{P_{R1}}{P_{t1}} = \left( \frac{T_{R1}}{T_{t1}} \right)^{\frac{\gamma}{\gamma-1}}$$

$$\frac{T_{E1}}{T_{t1}} = \left( \frac{T_{R1}}{T_{t1}} \right) + X_{U2m}^2 - X_{U1m}^2$$

$$\frac{P_{E1}}{P_{t1}} = \left( \frac{T_{E1}}{T_{t1}} \right)^{\frac{\gamma}{\gamma-1}}$$

$$\frac{P_{E2}}{P_{t1}} = \frac{P_{E1}}{P_{t1}} - \tilde{\omega}_{T_1} \cdot \left[ \frac{P_{R1}}{P_{t1}} - \frac{P_1}{P_{t1}} \right]$$

$$\frac{T_{t2}}{T_{t1}} = \tau$$

$$\frac{P_{t2}}{P_{t1}} = \frac{P_{E1}}{P_{t1}} \cdot \left( \frac{T_{t2}}{T_{E2}} \right)^{\frac{\gamma}{\gamma-1}} = \frac{P_{E2}}{P_{t1}} \cdot \left[ \frac{\tau}{T_{E2}/T_{t1}} \right]^{\frac{\gamma}{\gamma-1}}, \text{ where } \frac{T_{E2}}{T_{t1}} = \frac{T_{E1}}{T_{t1}}$$

$$\frac{T_2}{T_{t1}} = \tau - X_{2m}^2$$

$$\frac{P_2}{P_{t1}} = \frac{P_{t2}}{P_{t1}} \cdot \left( \frac{T_2}{T_{t1}} \right)^{\frac{\gamma}{\gamma-1}} = \frac{P_{t2}}{P_{t1}} \cdot \left( \frac{T_2/T_{t1}}{\tau} \right)^{\frac{\gamma}{\gamma-1}}$$

**a. Rotor Annulus**

$$\Phi_{2m} = Y_{2m} \cdot (1 - Y_{2m}^2)^{\frac{1}{\gamma-1}}$$

$$\frac{A_2}{A_1} = \frac{\Phi_{1t} \cdot \cos \alpha_{1t}}{\Phi_{2m} \cdot \cos \alpha_{2m}} \cdot \frac{\sqrt{\tau}}{\left( \frac{P_{t2}}{P_{t1}} \right)}$$

$$A_2 = \frac{A_2}{A_1} \cdot A_1$$

$$r_{2m} = r_{1m} \cdot R_{21}$$

$$H_2 = \frac{A_2}{2 \cdot \pi \cdot r_{2m}}$$

$$r_{ht2} = \frac{1 - H_2/2 \cdot r_{2m}}{1 + H_2/2 \cdot r_{2m}}$$

$$r_{t2} = \left( \frac{2}{1 + r_{ht2}} \right) \cdot r_{2m}$$

$$r_{h2} = r_{ht2} \cdot r_{t2}$$

## 5. Stator Performance

Initially set  $\tilde{\omega}_{\text{SFTC}_3}, \tilde{\omega}_s = 0$

On subsequent iterations  $\tilde{\omega}_{\text{SFTC}_3}$  and  $\tilde{\omega}_s$  are

$$\beta_\infty = \tan^{-1} \left[ \left( \frac{\tan \alpha_{2m} + \tan \alpha_{3m}}{2} \right) \right]$$

$$C_L = \frac{2}{\sigma_{3m}} \cdot (\tan \alpha_{2m} - \tan \alpha_{3m}) \cdot \cos \beta_\infty$$

$$C_{D3} = \frac{1}{4} \cdot C_L^2 \cdot \sigma_{3m} \cdot \left( \frac{\delta_3}{H_3} \right) \cdot \frac{1}{\cos \beta_\infty} + 0.04 \cdot C_L^2 \cdot \sigma_{3m} \cdot \left( \frac{S_3}{H_3} \right)$$

$$\tilde{\omega}_{\text{SFTC}_3} = C_{Di} \cdot \frac{\cos^2 \alpha_{2m}}{\cos^3 \beta_\infty} \cdot \sigma_{3m}$$

$$y^* = \frac{1}{4 \cdot \gamma \cdot M_{2m}^2} \left[ (\gamma+1) \cdot M_{2m}^2 - (3-\gamma) + \sqrt{(\gamma+1) \cdot \{(\gamma+1) \cdot M_{2m}^2 - 2 \cdot (3-\gamma) \cdot M_{2m}^2 + \gamma+9\}} \right]$$

$$\frac{P_{te}}{P_{ti}} = \left[ \frac{\gamma+1}{2 \cdot \gamma \cdot M_{2m}^2 \cdot y^* - (\gamma-1)} \right]^{\frac{1}{\gamma-1}} \cdot \left[ \frac{(\gamma+1) \cdot M_{2m}^2 \cdot y^*}{2 + (\gamma-1) \cdot M_{2m}^2 \cdot y^*} \right]^{\frac{\gamma}{\gamma-1}}$$

$$\tilde{\omega}_s = \frac{P_{ti} - P_{te}}{P_{ti} - P_i} = \frac{1 - P_{te}/P_i}{1 - P_i/P_i} = \frac{1 - P_{te}/P_i}{1 - \left[ 1 + \frac{\gamma-1}{2} \cdot M_{2m}^2 \right]^{\frac{\gamma}{\gamma-1}}}$$

$$\tilde{\omega}_p = 2 \cdot \sigma_{3m} \cdot \frac{\cos^2 \alpha_{2m}}{\cos^3 \alpha_{3m}} \cdot [0.005 + 0.16 \cdot D_{3m}^4]$$

$$\tilde{\omega}_{T_3} = \tilde{\omega}_p + \tilde{\omega}_{\text{SFTC}_3} + \tilde{\omega}_s$$

$$\frac{P_{i3}}{P_{i1}} = \frac{P_{i2}}{P_{i1}} - \tilde{\omega}_{T_3} \cdot \left( \frac{P_{i2}}{P_{i1}} - \frac{P_2}{P_{i1}} \right)$$

$$\frac{T_{i3}}{T_{i1}} = \tau$$

$$\frac{T_3}{T_{i1}} = \tau - X_{3m}^2$$

$$\frac{P_3}{P_{i1}} = \left( \frac{P_3}{P_{i3}} \right) \cdot \left( \frac{P_{i3}}{P_{i1}} \right) = \left( \frac{T_3}{T_{i1}} \right)^{\frac{\gamma}{\gamma-1}} \cdot \left( \frac{P_{i3}}{P_{i1}} \right) = \left[ \left( \frac{T_3}{T_{i1}} \right) \cdot \left( \frac{T_{i1}}{T_{i3}} \right) \right]^{\frac{\gamma}{\gamma-1}} \cdot \frac{P_{i3}}{P_{i1}} = \left[ \frac{T_3/T_{i1}}{\tau} \right]^{\frac{\gamma}{\gamma-1}} \cdot \frac{P_{i3}}{P_{i1}}$$

### a. Stator Annulus

$$\Phi_{3m} = Y_{3m} \cdot (1 - Y_{3m}^2)^{\frac{1}{\gamma-1}}$$



$$\frac{A_3}{A_1} = \frac{\Phi_{1t} \cdot \cos \alpha_{1t}}{\Phi_{3m} \cdot \cos \alpha_{3m}} \cdot \frac{\sqrt{\tau}}{\left( \frac{P_{t3}}{P_{t1}} \right)}$$

$$A_3 = \frac{A_3}{A_1} \cdot A_1$$

$$H_3 = \frac{A_3}{2 \cdot \pi \cdot r_{3m}}$$

$$r_{3m} = r_{2m} \cdot R_{32}$$

$$r_{ht3} = \frac{1 - H_3 / 2 \cdot r_{3m}}{1 + H_3 / 2 \cdot r_{3m}}$$

$$r_{3t} = \left( \frac{2}{1 + r_{ht3}} \right)$$

$$r_{3h} = r_{3m} \cdot r_{3t}$$

## 6. Rotor & Stator at the Hub and Tip

The below equations are generic forms of the specific equation. The brackets [] replace the rotor (2) and stator (3) subscripts. Also, the parentheses () replace the hub (1) and tip (3) subscripts.

$$X_{\theta[10]} = X_{\theta[1m]} \cdot \frac{r_{[1]m}}{r_{[1]0}}$$

$$X_{U[10]} = X_{U[1m]} \cdot \frac{r_{[1]0}}{r_{[1]m}}$$

$$\alpha_{[10]} = \tan^{-1} \frac{X_{\theta[10]}}{X_{Z[1m]}}$$

$$\beta_{[10]} = \tan^{-1} \frac{X_{U[10]} - X_{\theta[10]}}{X_{Z[1m]}}$$

$$X_{[10]} = \frac{X_{Z[1m]}}{\cos \alpha_{[10]}}$$

$$X_{w[10]} = \frac{X_{Z[1m]}}{\cos \beta_{[10]}}$$

$$Y_{[10]} = \frac{X_{[10]}}{\sqrt{\tau}}$$

$$Y_{w[10]} = \frac{X_{w[10]}}{\sqrt{\tau}}$$

$$M_{l|0} = \sqrt{\frac{\frac{2}{\gamma-1} \cdot Y_{l|0}^2}{1 - Y_{l|0}^2}}$$

$$M_{w|0} = \sqrt{\frac{\frac{2}{\gamma-1} \cdot Y_{w|0}^2}{1 - Y_{w|0}^2}}$$

## 7. Blade Geometry

The below equations are generic forms of the specific equation. The brackets [] replace the rotor (2) and stator (3) subscripts.

$$H_{[]} = r_{|t} - r_{|h}$$

$$C_{|} = \frac{H_{|}}{AR}$$

$$Z_{|} = \frac{2 \cdot \pi \cdot r_{|m} \cdot \sigma_{|m}}{C_{|}}$$

$Z_{|}$  is chosen by the user at this point.

$$AR_{Rev} = \frac{H_{|}}{\left( \frac{2 \cdot \pi \cdot r_{|m} \cdot \sigma_{|m}}{Z_{|}} \right)}$$

$$C_{Rev|} = \frac{H_{|}}{AR_{Rev}}$$

$$S_{|} = \frac{C_{Rev|}}{\sigma_{|m}}$$

## 8. Efficiency

$$\Pi_c = \frac{P_{t3}}{P_{t1}}$$

$$\tau_c = \frac{T_{t2}}{T_{t1}}$$

$$\eta_c = \frac{\Pi_c^{\frac{\gamma}{\gamma-1}} - 1}{\tau_c - 1}$$

### A.2. INTERPOLATION EQUATIONS

Starting with a general quadratic equation

$$D^i(R) = A_i \cdot R^2 + B_i \cdot R + C_i$$

solve for  $A_i$ ,  $B_i$ , and  $C_i$  using known points  $i-1$ ,  $i$ , and  $i+1$ .

$$A_i = \left( \frac{1}{R_{i+1} - R_{i-1}} \right) \cdot \left[ \left( \frac{D_{i+1} - D_i}{R_{i+1} - R_i} \right) - \left( \frac{D_i - D_{i-1}}{R_i - R_{i-1}} \right) \right]$$

$$B_i = \left( \frac{D_i - D_{i-1}}{R_i - R_{i-1}} \right) - A_i \cdot (R_i + R_{i-1})$$

$$C_i = D_i - A_i \cdot R_i^2 - B_i \cdot R_i$$

Over the first and last intervals, only one quadratic can be defined, so that

$$D_{\text{int}}(1) = \frac{A_1}{3} \cdot (R_2^3 - R_1^3) + \frac{B_1}{2} \cdot (R_2^2 - R_1^2) + C_1 \cdot (R_2 - R_1)$$

$$D_{\text{int}}(N) = \frac{A_N}{3} \cdot (R_{N+1}^3 - R_N^3) + \frac{B_N}{2} \cdot (R_{N+1}^2 - R_N^2) + C_N \cdot (R_{N+1} - R_N)$$

The complete integral is given by

$$\int_{R_1}^{R_{N+1}} \bar{D}(R) dr = D_{\text{int}}(1) + \sum_{i=2}^{N-1} D_{\text{int}}(i) + D_{\text{int}}(N)$$

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# APPENDIX B. PROGRAM SOURCE DATA

## B.1. SCREEN SNAPSHOTS

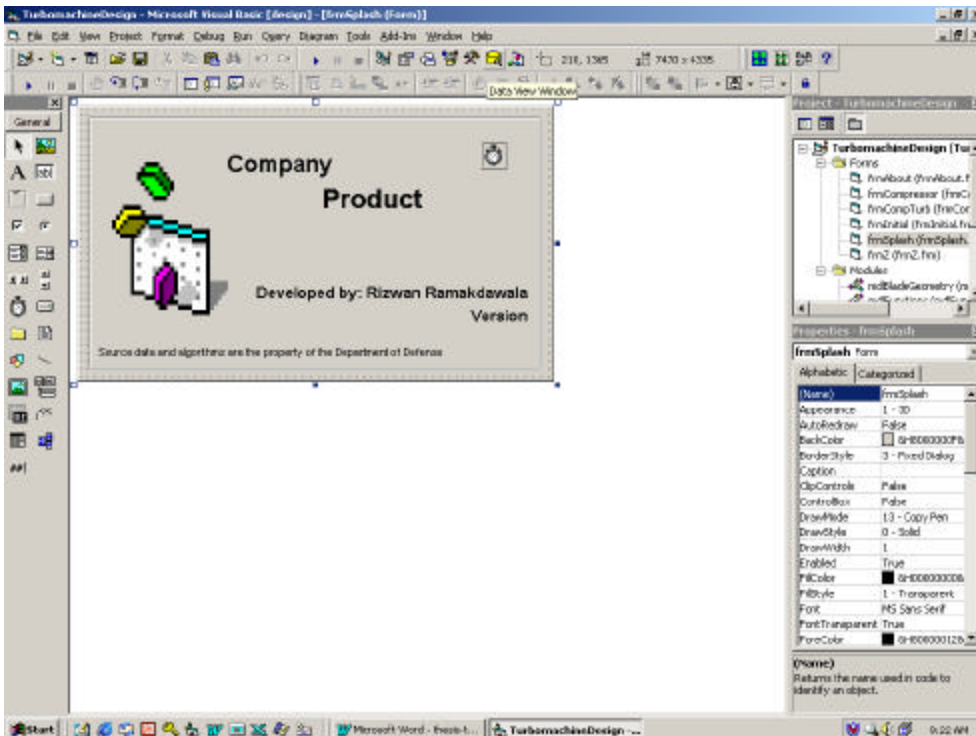


Figure B1. Splash Screen

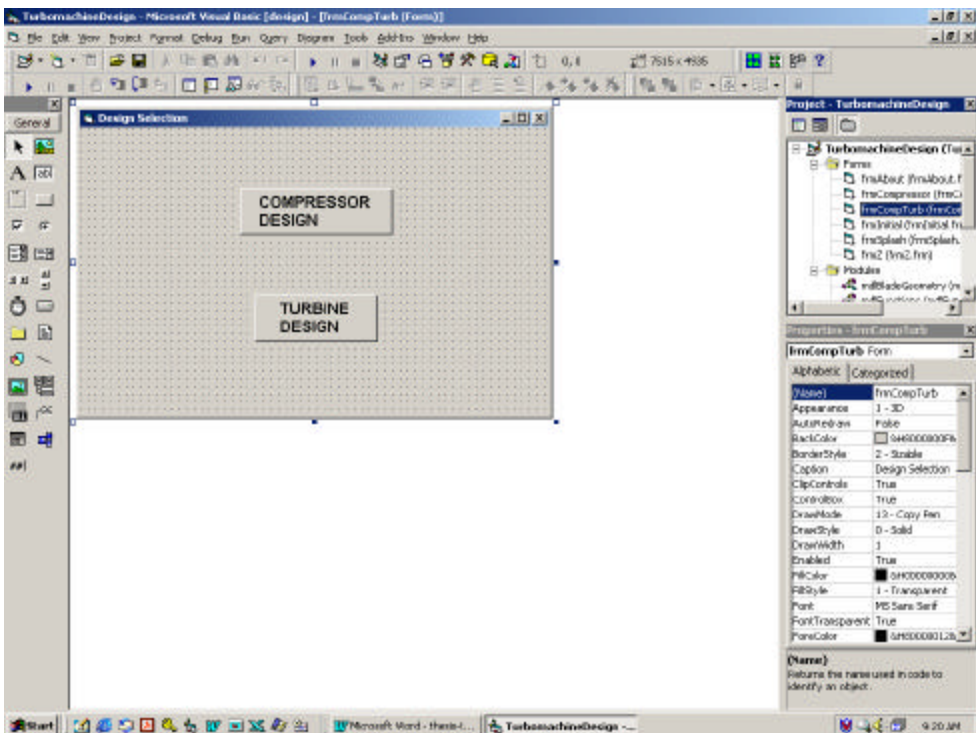


Figure B2. Compressor/Turbine Selection Screen

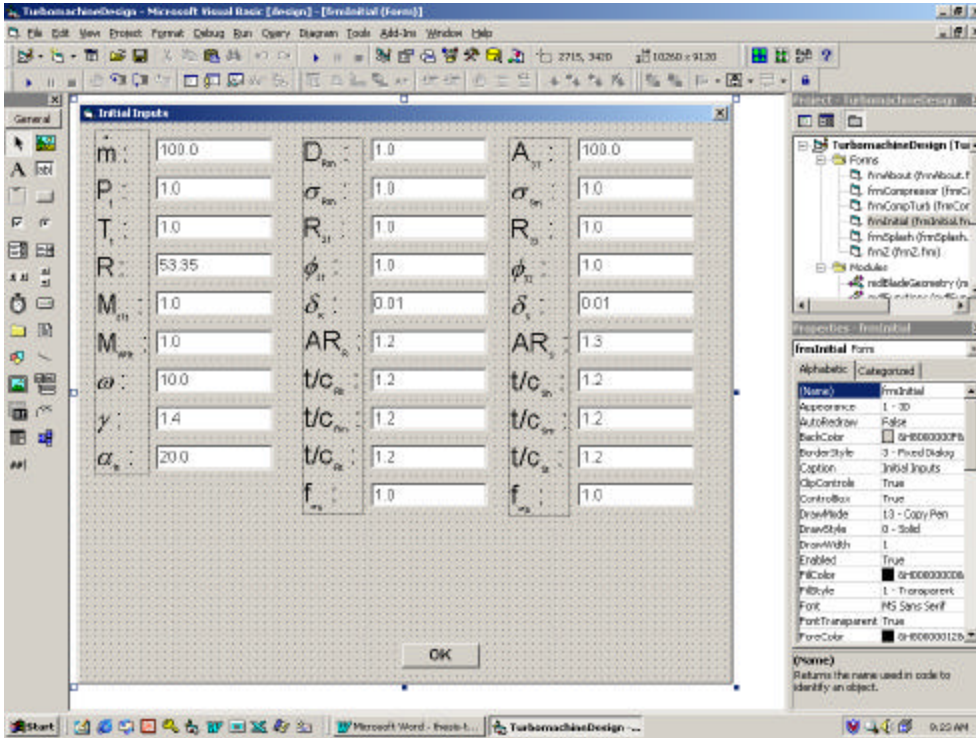


Figure B3. Initial Inputs Screen

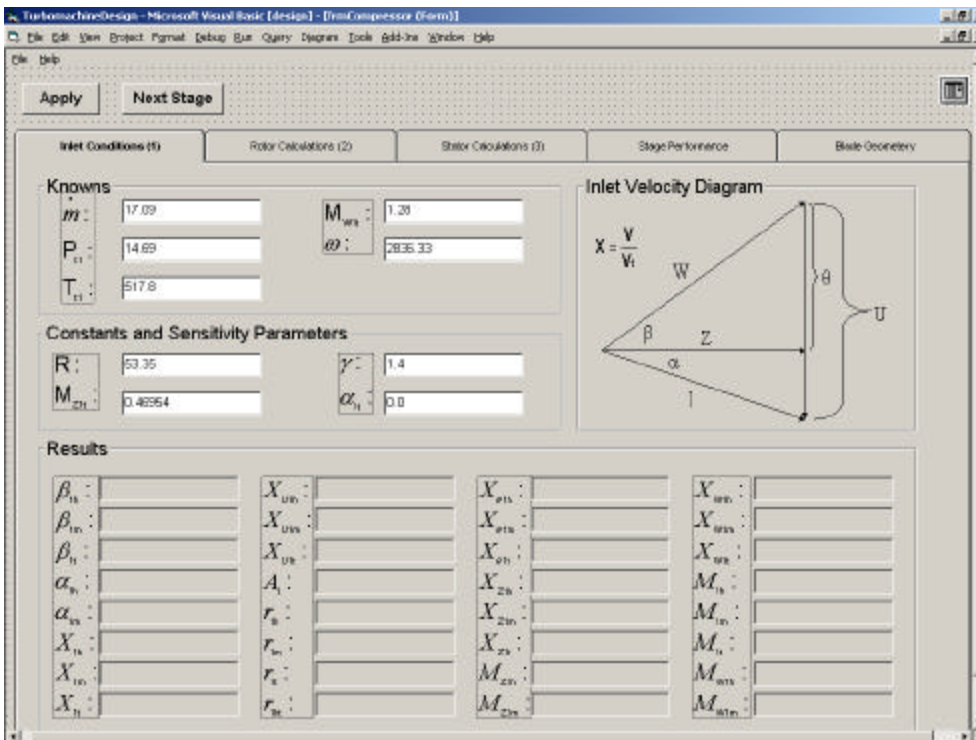


Figure B4. Compressor Design Screen: Inlet Conditions (1)

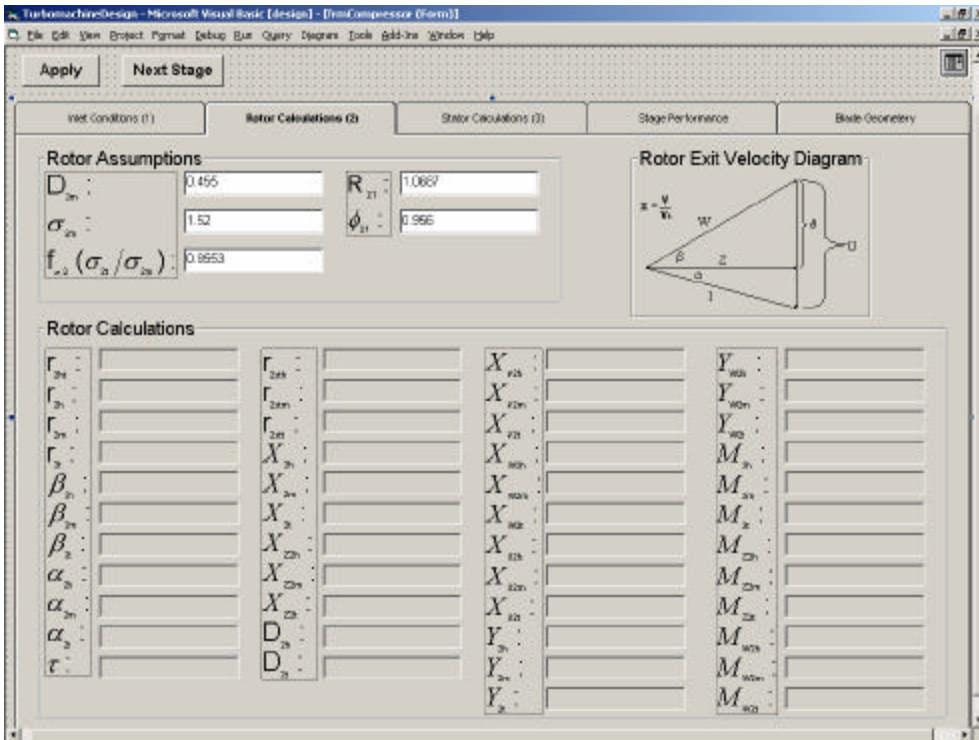


Figure B5. Compressor Design Screen: Rotor Calculations (2)

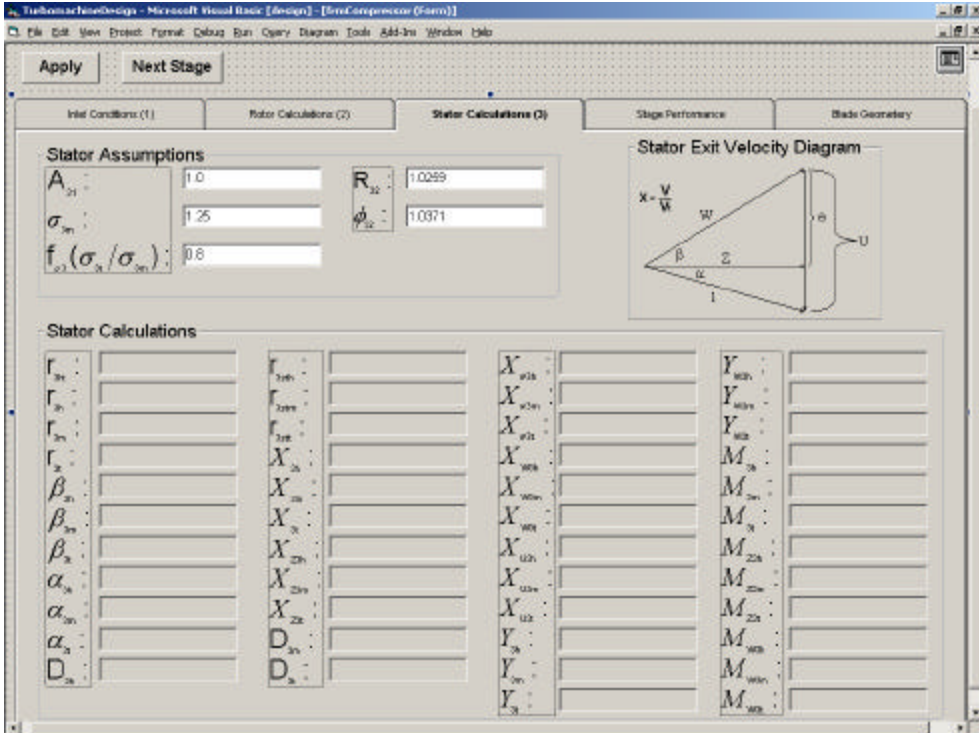


Figure B6. Compressor Design Screen: Stator Calculations (3)

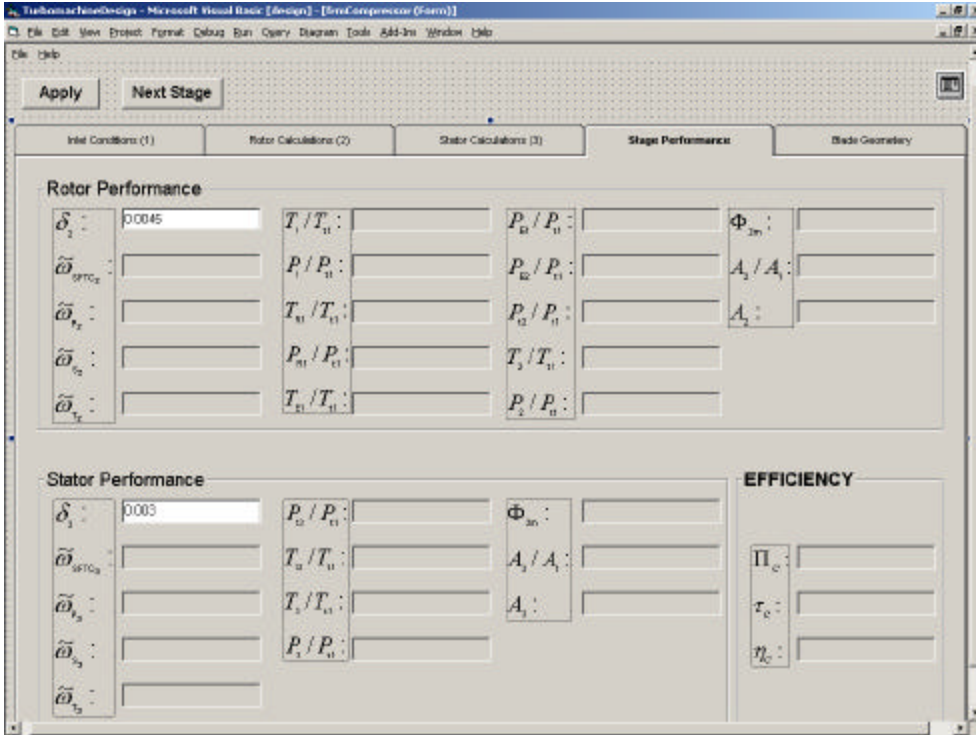


Figure B7. Compressor Design Screen: Stage Performance

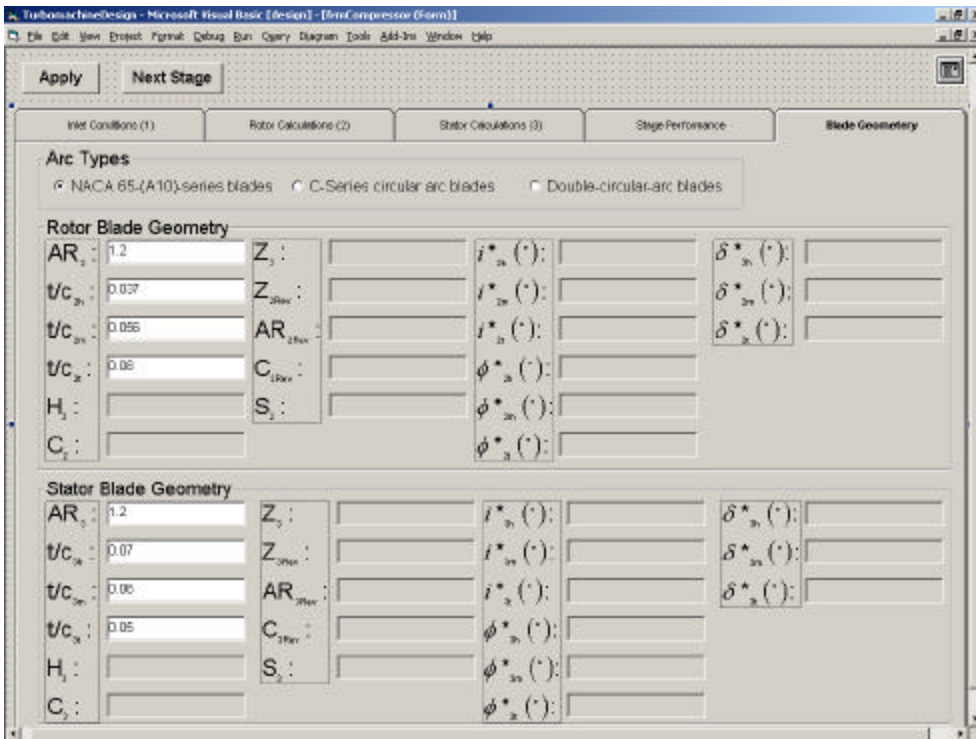


Figure B8. Compressor Design Screen: Blade Geometry



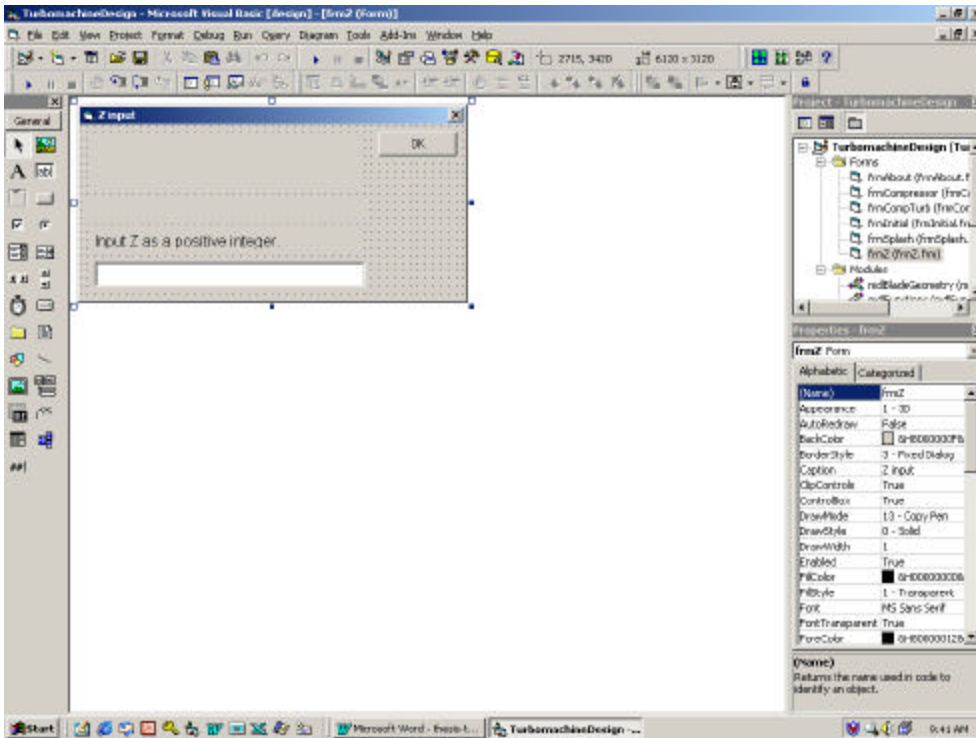


Figure B9. Blade Number Input Screen

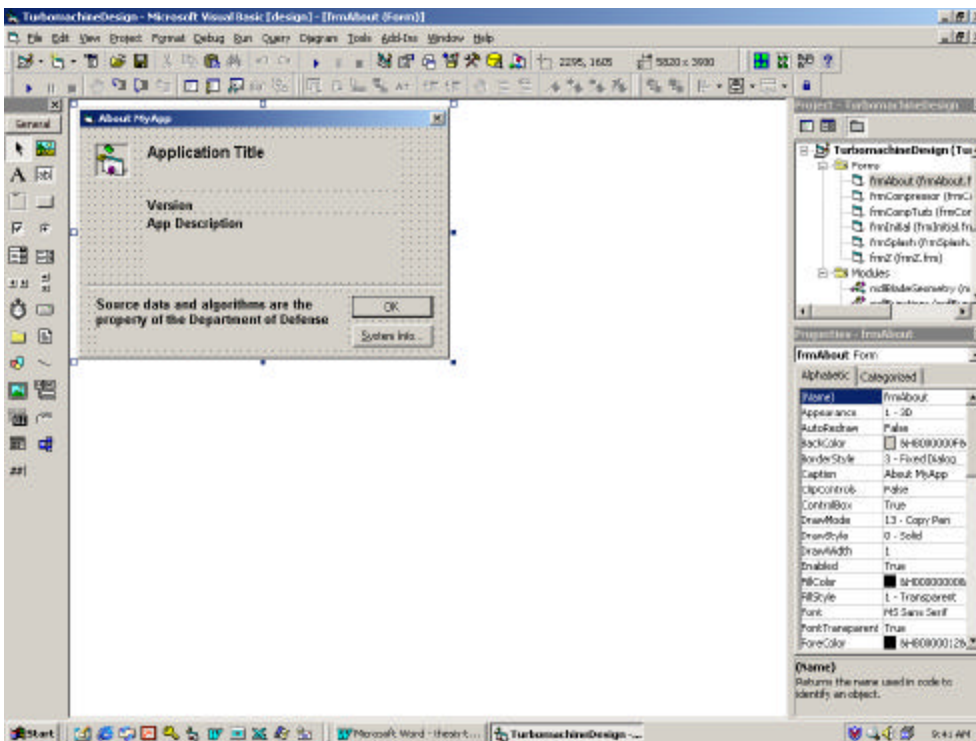


Figure B10. About Screen

## B.2. KEY VARIABLES

Table B1. [Error! Not a valid link.](#)  
Velocity Diagram Variables

Table B2. [Error! Not a valid link.](#)  
Stage Performance Variables

Table B3. [Error! Not a valid link.](#)  
Blade Geometry Variables

## B.3. SOURCE CODE

Lines with an apostrophe (') in the front is a comment line in the code and is not an executed statement.

### 1. Splash Screen Code

```
Option Explicit
Private Sub Form_Load()
    lblVersion.Caption = "Version " & App.Major & "." & App.Minor & "." & App.Revision
    lblProductName.Caption = App.Title
    lblCompany.Caption = App.CompanyName
End Sub
Private Sub tmrSplash_Timer()
    Unload Me
    frmCompTurb.Show
End Sub
```

### 2. Compressor/Turbine Selection Screen Code

```
Private Sub cmdComp_Click()
    Unload Me
    frmInitial.Show
End Sub
```

### 3. Initial Input Screen Code

```
Option Explicit
Option Base 1
Private Sub OKButton_Click()
    frmInitial.Hide
```

```

frmCompressor.Show
' Transfer initial values to the main form.
End Sub

4. Compressor Design Screen Code

Option Explicit
Option Base 1
Public i As Integer
' Integer to use as an array counter from inlet (i = 1) to rotor (i=2) to stator (i=3)
' It should be noted that although some arrays have no inlet values (e.g. diffusion and deg. of
  reation)
' we still set the array value to 3 versus 2. This is to keep consistent with the numbering.
' arrays that don't have the i=1 value assigned are null and irrelevant since they are not used
' in any calculations.
Public j As Integer
' integer to use as an array counter from hub (j = 1) to mean (j = 2) to tip (j = 3)
' It should be noted that although hub, mn and tip have been set up a constants
' j will be used to calculate the minimum loss incidence angle and the camber angle

Public ksh As Single
' correction factor for shape
Public slopegraph As Boolean
' checks which graph should be used to calculate the slope factor
Const testvar As Single = 0.0001
' exit criteria for main loop
Public loopcount As Integer
' loop counter to track the number of iterations
Dim tempvar(3) As Double
' holder for previous loss value for comparison
Public CompEff As Double
' compressor efficiency
Private Sub cmdApply_Click()
    Sequence
    UpdateVelDiag
    UpdatePerf
    UpdateGeo
End Sub

```

Private Sub Form\_Initialize()

```
frmCompressor.txtmdot.Text = frmInitial.txtmdot.Text
frmCompressor.txtPt1.Text = frmInitial.txtPt1.Text
frmCompressor.txtTt1.Text = frmInitial.txtTt1.Text
frmCompressor.txtR.Text = frmInitial.txtR.Text
frmCompressor.txtMzt(1).Text = frmInitial.txtMz1t.Text
frmCompressor.txtMwt(1).Text = frmInitial.txtMw1t.Text
frmCompressor.txtspeed.Text = frmInitial.txtomega.Text
frmCompressor.txtgamma.Text = frmInitial.txtgamma.Text
frmCompressor.txtalphan(1).Text = frmInitial.txtAlpha1t.Text
frmCompressor.txtDm(2).Text = frmInitial.txtDRm.Text
frmCompressor.txtsigmam(2).Text = frmInitial.txtsigmaRm.Text
frmCompressor.txtsigmam(3).Text = frmInitial.txtsigmaSm.Text
frmCompressor.txtR21.Text = frmInitial.txtR21.Text
frmCompressor.txtR32.Text = frmInitial.txtR32.Text
frmCompressor.txtphi21.Text = frmInitial.txtphi21.Text
frmCompressor.txtphi32.Text = frmInitial.txtphi32.Text
frmCompressor.txtA31.Text = frmInitial.txtA31.Text
frmCompressor.txtDelta(2).Text = frmInitial.txtDeltar.Text
frmCompressor.txtDelta(3).Text = frmInitial.txtDeltas.Text
frmCompressor.txtAR(2).Text = frmInitial.txtARr.Text
frmCompressor.txtAR(3).Text = frmInitial.txtARs.Text
frmCompressor.txttch(2).Text = frmInitial.txttcrh.Text
frmCompressor.txttch(3).Text = frmInitial.txttcsH.Text
frmCompressor.txttcm(2).Text = frmInitial.txttcrm.Text
frmCompressor.txttcm(3).Text = frmInitial.txttcs m.Text
frmCompressor.txttct(2).Text = frmInitial.txttctr.Text
frmCompressor.txttct(3).Text = frmInitial.txttctst.Text
frmCompressor.txtfsigma(2).Text = frmInitial.txtfsigmar.Text
frmCompressor.txtfsigma(3).Text = frmInitial.txtfsigmas.Text
' Initialize Inlet Condition Variables.
alpha(1, 3) = frmCompressor.txtalphan(1).Text
gamma = frmCompressor.txtgamma.Text
Mz(1, 3) = frmCompressor.txtMzt(1).Text
mdot = frmCompressor.txtmdot.Text
Mw(1, 3) = frmCompressor.txtMwt(1).Text
omega = frmCompressor.txtspeed.Text
```

```

Pt(1) = frmCompressor.txtPt1.Text
Rbar = frmCompressor.txtR.Text
Tt(1) = frmCompressor.txtTt1.Text
' Initialize Rotor Assumption Variables
D(2, 2) = frmCompressor.txtDm(2).Text
sigma(2, 2) = frmCompressor.txtsigmam(2).Text
pitch(2) = frmCompressor.txtR21.Text
phi21 = frmCompressor.txtphi21.Text
fsigma(2) = frmCompressor.txtfsigma(2).Text
' Initialize Stator Assumption Variables
A31 = frmCompressor.txtA31.Text
sigma(3, 2) = frmCompressor.txtsigmam(3).Text
pitch(3) = frmCompressor.txtR32.Text
phi32 = frmCompressor.txtphi32.Text
fsigma(3) = frmCompressor.txtfsigma(3).Text
' Initialize Stage Performance variables
delta(2) = frmCompressor.txtDelta(2).Text
delta(3) = frmCompressor.txtDelta(3).Text
' initialize blade geometry variables
For i = 2 To 3
    For j = 1 To 3
        AR(i) = frmCompressor.txtAR(i).Text
        If j = 1 Then
            tc(i, j) = frmCompressor.txttch(i).Text
        ElseIf j = 2 Then
            tc(i, j) = frmCompressor.txttcm(i).Text
        ElseIf j = 3 Then
            tc(i, j) = frmCompressor.txttct(i).Text
        End If
    Next j
Next i
End Sub
Private Sub UpdateVelDiag()
    For i = 1 To 3
        For j = 1 To 3
            If j = 1 Then
                txtBetah(i).Text = beta(i, j)
            End If
        Next j
    Next i
End Sub

```

```

txtAlphah(i).Text = alpha(i, j)
txtXh(i).Text = x(i, j)
txtXUh(i).Text = Xu(i, j)
txtXzh(i).Text = Xz(i, j)
txtXtheta(i).Text = Xtheta(i, j)
txtXwh(i).Text = Xw(i, j)
txtrh(i).Text = R(i, j)
txtMh(i).Text = M(i, j)
txtMwh(i).Text = Mw(i, j)
txtMzh(i).Text = Mz(i, j)
If i = 2 Then
    txtrsth(i).Text = rst(i, j)
    txtDh(i).Text = D(i, j)
    txtYh(i).Text = Y(i, j)
    txtYwh(i).Text = Yw(i, j)
ElseIf i = 3 Then
    txtrsth(i).Text = rst(i, j)
    txtDh(i).Text = D(i, j)
    txtYh(i).Text = Y(i, j)
    txtYwh(i).Text = Yw(i, j)
End If

```

End If

If j = 2 Then

```

txtbetam(i).Text = beta(i, j)
txtalpham(i).Text = alpha(i, j)
txtXm(i).Text = x(i, j)
txtXUm(i).Text = Xu(i, j)
txtXzm(i).Text = Xz(i, j)
txtXthetam(i).Text = Xtheta(i, j)
txtXwm(i).Text = Xw(i, j)
txtrm(i).Text = R(i, j)
txtMm(i).Text = M(i, j)
txtMwm(i).Text = Mw(i, j)
txtMzm(i).Text = Mz(i, j)
If i = 2 Then

```

```

    txtrstm(i).Text = rst(i, j)
    txtYm(i).Text = Y(i, j)

```

```

        txtYwm(i).Text = Yw(i, j)
    ElseIf i = 3 Then
        txt rstm(i).Text = rst(i, j)
        txtYm(i).Text = Y(i, j)
        txtYwm(i).Text = Yw(i, j)
        txtDm(i) = D(i, j)
    End If
End If
If j = 3 Then
    txtbetat(i).Text = beta(i, j)
    txtXt(i).Text = x(i, j)
    txtXUt(i).Text = Xu(i, j)
    txtXzt(i).Text = Xz(i, j)
    txtXthetat(i).Text = Xtheta(i, j)
    txtXwt(i).Text = Xw(i, j)
    txtrt(i).Text = R(i, j)
    txtMt(i).Text = M(i, j)
    If i = 2 Then
        txtalpat(i).Text = alpha(i, j)
        txtMwt(i).Text = Mw(i, j)
        txtMzt(i).Text = Mz(i, j)
        txtrstt(i).Text = rst(i, j)
        txtDt(i).Text = D(i, j)
        txtYt(i).Text = Y(i, j)
        txtYwt(i).Text = Yw(i, j)
    ElseIf i = 3 Then
        txtalpat(i).Text = alpha(i, j)
        txtMwt(i).Text = Mw(i, j)
        txtMzt(i).Text = Mz(i, j)
        txtrstt(i).Text = rst(i, j)
        txtDt(i).Text = D(i, j)
        txtYt(i).Text = Y(i, j)
        txtYwt(i).Text = Yw(i, j)
    End If
End If
txtA(i).Text = A(i)
txtrht(i).Text = rht(i)

```

```

        Next j
    Next i
    txttau.Text = tau
End Sub
Private Sub UpdatePerf()
    For i = 1 To 3
        txtTTt1(i).Text = TTt1(i)
        txtPPt1(i).Text = PPt1(i)
    Next i
    For i = 1 To 2
        txtPEPt1(i).Text = PEPt1(i)
    Next i
    For i = 2 To 3
        txtDelta(i).Text = delta(i)
        txtomegasftc(i).Text = omegasftc(i)
        txtomegap(i).Text = omegap(i)
        txtomegasl(i).Text = omegas(i)
        txtomega(i).Text = omegat(i)
        txtAA1(i).Text = AA1(i)
        txtPhim(i).Text = Capphi(i, mn)
        txtPtPt1(i).Text = PtPt1(i)
    Next i
    txtTETt1(1).Text = TETt1(1)
    txtTR1Tt1.Text = Tr1Tt1
    txtPR1Pt1.Text = Pr1Pt1
    txtTt3Tt1.Text = TtTt1(3)
    txtPl.Text = PtPt1(3)
    txtBTau.Text = tau
    txteff.Text = CompEff
End Sub
Private Sub UpdateGeo()
    For i = 2 To 3
        txtH(i).Text = h(i)
        txtC(i).Text = C(i)
        txtZ(i).Text = Z(i)
        txtZrev(i).Text = intZ(i)
        txtARrev(i).Text = ARrev(i)
    
```



```

        txtCrev(i).Text = Crev(i)
        txtS(i).Text = S(i)
        txtcamberh(i) = camber(i, 1)
        txtcamberm(i) = camber(i, 2)
        txtcambert(i) = camber(i, 3)
        txtincidenceh(i) = icor(i, 1)
        txtincidencem(i) = icor(i, 2)
        txtincidencec(i) = icor(i, 3)
        txtdevh(i) = dref(i, 1)
        txtdevm(i) = dref(i, 2)
        txtdevt(i) = dref(i, 3)
    Next i
End Sub
Private Sub Form_Load()
    ' Initialize Inlet Condition Variables.
    alpha(1, 3) = frmCompressor.txtalphat(1).Text
    gamma = frmCompressor.txtgamma.Text
    Mz(1, 3) = frmCompressor.txtMzt(1).Text
    mdot = frmCompressor.txtmdot.Text
    Mw(1, 3) = frmCompressor.txtMwt(1).Text
    omega = frmCompressor.txtspeed.Text
    Pt(1) = frmCompressor.txtPt1.Text
    Rbar = frmCompressor.txtR.Text
    Tt(1) = frmCompressor.txtTt1.Text
    ' Initialize Rotor Assumption Variables
    D(2, 2) = frmCompressor.txtDm(2).Text
    sigma(2, 2) = frmCompressor.txtsigmam(2).Text
    pitch(2) = frmCompressor.txtR21.Text
    phi21 = frmCompressor.txtphi21.Text
    fsigma(2) = frmCompressor.txtfsigma(2).Text
    ' Initialize Stator Assumption Variables
    A31 = frmCompressor.txtA31.Text
    sigma(3, 2) = frmCompressor.txtsigmam(3).Text
    pitch(3) = frmCompressor.txtR32.Text
    phi32 = frmCompressor.txtphi32.Text
    fsigma(3) = frmCompressor.txtfsigma(3).Text
    ' Initialize Stage Performance variables

```

```

delta(2) = frmCompressor.txtDelta(2).Text
delta(3) = frmCompressor.txtDelta(3).Text
' initialize blade geometry variables
For i = 2 To 3
    For j = 1 To 3
        AR(i) = frmCompressor.txtAR(i).Text
        If j = 1 Then
            tc(i, j) = frmCompressor.txttch(i).Text
        ElseIf j = 2 Then
            tc(i, j) = frmCompressor.txttcm(i).Text
        ElseIf j = 3 Then
            tc(i, j) = frmCompressor.txttct(i).Text
        End If
    Next j
Next i
End Sub
Private Sub mnuAbout_Click()
    frmAbout.Show
End Sub
Private Sub mnuContents_Click()
    MsgBox "This function is not available yet.", vbInformation, "Not Implemented"
End Sub
Private Sub mnuExit_Click()
    End
End Sub
Private Sub mnuOpen_Click()
    dlgFile.ShowOpen
End Sub
Private Sub mnuPrint_Click()
    dlgFile.ShowPrinter
    Printer.Copies = dlgFile.Copies
    Printer.Orientation = dlgFile.Orientation
    Printer.Print A(i)
    Printer.EndDoc
End Sub
Private Sub mnuSave_Click()
    dlgFile.ShowSave

```

```

End Sub
Private Sub mnuSearch_Click()
    MsgBox "This function is not available yet.", vbInformation, "Not Implemented"
End Sub
Public Sub Sequence()
    i = 1
    InletCond
    HubCalc i
    If optNACA = True Then
        ksh = 1
        slopegraph = True
    End If
    If optC = True Then
        ksh = 1.1
        slopegraph = False
    End If
    If optDCA = True Then
        ksh = 0.7
        slopegraph = False
    End If
    For i = 2 To 3
        MeanCalc i
    Next i
    loopcount = 1
    Do
        For i = 2 To 3
            If loopcount = 1 Then
                omegat(i) = 0
                omegasftc(i) = 0
                omegas(i) = 0
            End If
            tempvar(i) = omegat(i)
            If i = 2 Then
                RotorPerf i, loopcount
            ElseIf i = 3 Then
                StatorPerf i, loopcount
            End If
        Next i
        loopcount = loopcount + 1
    Loop
End Sub

```

```

        HubTipCalc i
        BladeGeo i, loopcount
    Next i
    loopcount = loopcount + 1
Loop Until Abs(omegat(2) - tempvar(2)) < testvar And Abs(omegat(3) - tempvar(3)) <
    testvar
For i = 2 To 3
    For j = 1 To 3
        Incidence i, j, slopegraph, ksh
    Next j
Next i
CompEff = ((PtPt1(3) ^ g1g(gamma)) - 1) / (tau - 1)
End Sub
Private Sub txtA31_KeyPress(KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtA31.Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
    End Select
End Sub
Private Sub txtalphanat_KeyPress(Index As Integer, KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtalphanat(1).Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
    End Select
End Sub

```

```

        End If
    Case Else
        KeyAscii = 0
        Beep
    End Select
End Sub
Private Sub txtAR_KeyPress(Index As Integer, KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtAR(2).Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            ElseIf Len(txtAR(3).Text) <> 0 Then
                KeyAscii = 0
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
        End Select
    End Sub
Private Sub txtDelta_KeyPress(Index As Integer, KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtDelta(2).Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            ElseIf Len(txtDelta(3).Text) <> 0 Then
                KeyAscii = 0
                Beep
            End If
    End If

```

```

        Case Else
            KeyAscii = 0
            Beep
    End Select
End Sub
Private Sub txtDm_KeyPress(Index As Integer, KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtDm(2).Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
    End Select
End Sub
Private Sub txtgamma_KeyPress(KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtgamma.Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
    End Select
End Sub
Private Sub txtmdot_KeyPress(KeyAscii As Integer)
    Select Case KeyAscii

```

```

        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtmdot.Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
        End Select
    End Sub

Private Sub txtMwt_KeyPress(Index As Integer, KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtMwt(1).Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
        End Select
    End Sub

Private Sub txtMzt_KeyPress(Index As Integer, KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtMzt(1).Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
        End Select
    End Sub

```

```

        End If
    Case Else
        KeyAscii = 0
        Beep
    End Select
End Sub
Private Sub txtphi21_KeyPress(KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtphi21.Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
        End Select
    End Sub
Private Sub txtphi32_KeyPress(KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtphi32.Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
        End Select
    End Sub
Private Sub txtPt1_KeyPress(KeyAscii As Integer)

```



```

Select Case KeyAscii
    Case vbKey0 To vbKey9
    Case vbDecimal, 46
    Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
    Case 45
        If Len(txtPt1.Text) <> 0 Then
            KeyAscii = 0 ' ignore keystroke
            Beep
        End If
    Case Else
        KeyAscii = 0
        Beep
    End Select
End Sub

Private Sub txtR_KeyPress(KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtR.Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
        End Select
    End Sub

Private Sub txtR21_KeyPress(KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtR21.Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke

```

```

        Beep
    End If
Case Else
    KeyAscii = 0
    Beep
End Select
End Sub
Private Sub txtR32_KeyPress(KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtR32.Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
    End Select
End Sub
Private Sub txtsigmam_KeyPress(Index As Integer, KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtsigmam(2).Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            ElseIf Len(txtsigmam(3).Text) <> 0 Then
                KeyAscii = 0
                Beep
            End If
        Case Else
            KeyAscii = 0

```

```

        Beep
    End Select
End Sub
Private Sub txtspeed_KeyPress(KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtspeed.Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
    End Select
End Sub
Private Sub txttch_KeyPress(Index As Integer, KeyAscii As Integer)
    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txttch(2).Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            ElseIf Len(txttch(3).Text) <> 0 Then
                KeyAscii = 0
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
    End Select
End Sub
Private Sub txttcm_KeyPress(Index As Integer, KeyAscii As Integer)

```

```

Select Case KeyAscii
    Case vbKey0 To vbKey9
    Case vbDecimal, 46
    Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
    Case 45
        If Len(txttcm(2).Text) <> 0 Then
            KeyAscii = 0 ' ignore keystroke
            Beep
        ElseIf Len(txttcm(3).Text) <> 0 Then
            KeyAscii = 0
            Beep
        End If
    Case Else
        KeyAscii = 0
        Beep
End Select
End Sub

```

```

Private Sub txttct_KeyPress(Index As Integer, KeyAscii As Integer)

```

```

    Select Case KeyAscii
        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txttct(2).Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            ElseIf Len(txttct(3).Text) <> 0 Then
                KeyAscii = 0
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
    End Select
End Sub

```

```

Private Sub txtTt1_KeyPress(KeyAscii As Integer)

```

```

    Select Case KeyAscii

```

```

        Case vbKey0 To vbKey9
        Case vbDecimal, 46
        Case vbKeyBack, vbKeyClear, vbKeyTab, vbKeyUp, vbKeyDown
        Case 45
            If Len(txtTt1.Text) <> 0 Then
                KeyAscii = 0 ' ignore keystroke
                Beep
            End If
        Case Else
            KeyAscii = 0
            Beep
        End Select
    End Sub

```

## 5. Blade Number Input Screen Code

```

Option Explicit
Option Base 1
Private x As Variant
Private Sub OKButton_Click()
    x = txtZ.Text
    If IsNumeric(x) = False Then
        MsgBox "Input is not a number!", vbExclamation, "Numeric Validation"
    Else
        frmZ.Hide
    End If
End Sub

```

## 6. About Screen Code

```

Option Explicit
' Reg Key Security Options...
Const READ_CONTROL = &H20000
Const KEY_QUERY_VALUE = &H1
Const KEY_SET_VALUE = &H2
Const KEY_CREATE_SUB_KEY = &H4
Const KEY_ENUMERATE_SUB_KEYS = &H8
Const KEY_NOTIFY = &H10
Const KEY_CREATE_LINK = &H20

```

```

Const KEY_ALL_ACCESS = KEY_QUERY_VALUE + KEY_SET_VALUE +
    _ KEY_CREATE_SUB_KEY + KEY_ENUMERATE_SUB_KEYS +
    _ KEY_NOTIFY + KEY_CREATE_LINK + READ_CONTROL
' Reg Key ROOT Types...
Const HKEY_LOCAL_MACHINE = &H80000002
Const ERROR_SUCCESS = 0
Const REG_SZ = 1                ' Unicode nul terminated string
Const REG_DWORD = 4            ' 32-bit number
Const gREGKEYSYSINFOLOC = "SOFTWARE\Microsoft\Shared Tools Location"
Const gREGVALSYSINFOLOC = "MSINFO"
Const gREGKEYSYSINFO = "SOFTWARE\Microsoft\Shared Tools\MSINFO"
Const gREGVALSYSINFO = "PATH"

Private Declare Function RegOpenKeyEx Lib "advapi32" Alias "RegOpenKeyExA" (ByVal hKey
    As Long, ByVal lpSubKey As String, ByVal ulOptions As Long, ByVal samDesired As
    Long, ByRef phkResult As Long) As Long

Private Declare Function RegQueryValueEx Lib "advapi32" Alias "RegQueryValueExA" (ByVal
    hKey As Long, ByVal lpValueName As String, ByVal lpReserved As Long, ByRef
    lpType As Long, ByVal lpData As String, ByRef lpcbData As Long) As Long

Private Declare Function RegCloseKey Lib "advapi32" (ByVal hKey As Long) As Long

Private Sub cmdSysInfo_Click()
    Call StartSysInfo
End Sub

Private Sub cmdOK_Click()
    Unload Me
End Sub

Private Sub Form_Load()
    Me.Caption = "About " & App.Title
    lblVersion.Caption = "Version " & App.Major & "." & App.Minor & "." & App.Revision
    lblTitle.Caption = App.Title
    lblDescription.Caption = App.FileDescription
End Sub

Public Sub StartSysInfo()
    On Error GoTo SysInfoErr
    Dim rc As Long
    Dim SysInfoPath As String
    ' Try To Get System Info Program Path\Name From Registry...

```

```

If          GetKeyValue(HKEY_LOCAL_MACHINE,          gREGKEYSYSINFO,
gREGVALSYSINFO, SysInfoPath) Then
    ' Try To Get System Info Program Path Only From Registry...
ElseIf     GetKeyValue(HKEY_LOCAL_MACHINE,          gREGKEYSYSINFOLOC,
gREGVALSYSINFOLOC, SysInfoPath) Then
' Validate Existence Of Known 32 Bit File Version
    If (Dir(SysInfoPath & "\\MSINFO32.EXE") <> "") Then
        SysInfoPath = SysInfoPath & "\\MSINFO32.EXE"
        ' Error - File Can Not Be Found...
    Else
        GoTo SysInfoErr
    End If
    ' Error - Registry Entry Can Not Be Found...
Else
    GoTo SysInfoErr
End If
Call Shell(SysInfoPath, vbNormalFocus)
Exit Sub

SysInfoErr:
    MsgBox "System Information Is Unavailable At This Time", vbOKOnly
End Sub

Public Function GetKeyValue(KeyRoot As Long, KeyName As String, SubKeyRef As String,
ByRef KeyVal As String) As Boolean
    Dim i As Long          ' Loop Counter
    Dim rc As Long         ' Return Code
    Dim hKey As Long       ' Handle To An Open Registry Key
    Dim hDepth As Long    '
    Dim KeyValType As Long ' Data Type Of A Registry Key
    Dim tmpVal As String   ' Temporary Storage For A Registry Key Value
    Dim KeyValSize As Long ' Size Of Registry Key Variable
    '-----
    ' Open RegKey Under KeyRoot {HKEY_LOCAL_MACHINE...}
    '-----
    rc = RegOpenKeyEx(KeyRoot, KeyName, 0, KEY_ALL_ACCESS, hKey)
        ' Open Registry Key
    If (rc <> ERROR_SUCCESS) Then GoTo GetKeyError    ' Handle Error...
    tmpVal = String$(1024, 0)                        ' Allocate Variable Space
    KeyValSize = 1024                               ' Mark Variable Size

```

```

'-----
' Retrieve Registry Key Value...
'-----

rc = RegQueryValueEx(hKey, SubKeyRef, 0, _
    KeyValType, tmpVal, KeyValSize)      ' Get/Create Key Value
If (rc <> ERROR_SUCCESS) Then GoTo GetKeyError      ' Handle Errors
If (Asc(Mid(tmpVal, KeyValSize, 1)) = 0) Then      ' Win95 Adds Null
    Terminated String...
    tmpVal = Left(tmpVal, KeyValSize - 1)      ' Null Found, Extract
    From String
Else      ' WinNT Does NOT Null Terminate String...
    tmpVal = Left(tmpVal, KeyValSize)      ' Null Not Found,
    Extract String Only
End If
'-----
' Determine Key Value Type For Conversion...
'-----

Select Case KeyValType      ' Search Data Types...
Case REG_SZ      ' String Registry Key Data Type
    KeyVal = tmpVal      ' Copy String Value
Case REG_DWORD      ' Double Word Registry Key Data Type
    For i = Len(tmpVal) To 1 Step -1      ' Convert Each Bit
        KeyVal = KeyVal + Hex(Asc(Mid(tmpVal, i, 1)))      ' Build Value Char.
        By Char.
    Next
    KeyVal = Format$("&h" + KeyVal)      ' Convert Double Word To String
End Select
GetKeyValue = True      ' Return Success
rc = RegCloseKey(hKey)      ' Close Registry Key
Exit Function      ' Exit

GetKeyError:      ' Cleanup After An Error Has Occured...
    KeyVal = ""      ' Set Return Val To Empty String
    GetKeyValue = False      ' Return Failure
    rc = RegCloseKey(hKey)      ' Close Registry Key

End Function

```

## 7. Module mdInletCond Code

Option Explicit



Option Base 1  
 Public gamma As Double  
 ' Specific Heat Ratio (Cp/Cv)  
 Public mdot As Double  
 ' Mass Flow  
 Public Rbar As Double  
 ' Specific Gas Constant  
 Public omega As Double  
 ' wheel speed  
 Public Cp As Double  
 ' at constant pressure  
 Const g As Long = 32.2  
 ' gravitational constant  
 Public Caphi(3, 3) As Double  
 ' Flow Function  
 Public Tt(3) As Double  
 ' Total Temperature  
 Public Pt(3) As Double  
 ' Total Pressure  
 Public M(3, 3) As Double  
 ' Mach Number  
 Public Mw(3, 3) As Double  
 ' Mach Relative to the Blade  
 Public Mz(3, 3) As Double  
 ' Mach of the Axial Component  
 Public alpha(3, 3) As Double  
 ' Inlet Flow angle  
 Public beta(3, 3) As Double  
 ' Inlet Flow angle  
 Public x(3, 3) As Double  
 ' Dimensionless Velocity  
 Public Xz(3, 3) As Double  
 ' Dimensionless Velocity of the Axial Component  
 Public Xtheta(3, 3) As Double  
 ' Dimensionless Velocity along Theta  
 Public Xu(3, 3) As Double  
 ' Dimensionless Velocity of the Wheel Speed Component

```

Public Xw(3, 3) As Double
' Dimensionless Velocity Relative to the Blade
Public rot(3) As Double
' Density
Public Vt(3) As Double
' Total Velocity
Public A(3) As Double
' Annulus Area
Public R(3, 3) As Double
' Radius
Public rht(3) As Double
' Hub to Tip Ratio
Public pitch(3) As Double
' Mean Line Pitch (Rm2/Rm1)
Public rst(3, 3) As Double
' Degree of Reaction
Public i As Integer
Public Const hub As Integer = 1
' Integer used when making hub calculations (hub = 1)
Public Const mn As Integer = 2
' Integer used when making mean line calculations (mn = 2)
Public Const tip As Integer = 3
' Integer used when making tip calculations (tip = 3)
Public Sub InletCond()
    ' Calculation of Inlet Conditions at the tip
    i = 1
    beta(i, tip) = Arccos(Mz(i, tip) / Mw(i, tip))
    M(i, tip) = Mz(i, tip) / Cos(DegToRad(alpha(i, tip)))
    x(i, tip) = Sqr((((gamma - 1) / 2) * M(i, tip) ^ 2) / (1 + (((gamma - 1) / 2) * M(i, tip) ^ 2)))
    Xz(i, tip) = x(i, tip) * Cos(DegToRad(alpha(i, tip)))
    Xtheta(i, tip) = Xz(i, tip) * Tan(DegToRad(alpha(i, tip)))
    Xu(i, tip) = Xtheta(i, tip) + Xz(i, tip) * Tan(DegToRad(beta(i, tip)))
    Xw(i, tip) = Xwfunc(Xz(i, tip), beta(i, tip))
    rot(i) = Pt(i) / (12 * Rbar * Tt(i))
    Cp = gg1(gamma) * Rbar
    Vt(i) = Sqr(2 * Cp * g * Tt(i)) * 12
    Caphi(i, tip) = x(i, tip) * (1 - x(i, tip) ^ 2) ^ (1 / (gamma - 1))

```

```

A(i) = (mdot / (rot(i) * Vt(i))) * (1 / (Capphi(i, tip) * Cos(DegToRad(alpha(i, tip))))))
R(i, tip) = (Xu(i, tip) * Vt(i)) / omega
R(i, hub) = Sqr(R(i, tip) ^ 2 - A(i) / (22 / 7))
rht(i) = rhtfunc(R(i, tip), R(i, hub))
' Mean Calculations
R(i, mn) = rmfunc(R(i, tip), R(i, hub))
Xtheta(i, mn) = Xthetafunc(R(i, tip), R(i, mn), Xtheta(i, tip))
Xz(i, mn) = Xz(i, tip)
alpha(i, mn) = alphafunc(Xtheta(i, mn), Xz(i, mn))
Xu(i, mn) = Xufunc(R(i, tip), R(i, mn), Xu(i, tip))
beta(i, mn) = betafunc(Xu(i, mn), Xtheta(i, mn), Xz(i, mn))
x(i, mn) = Xfunc(Xz(i, mn), alpha(i, mn))
M(i, mn) = Mach(gamma, x(i, mn))
Xw(i, mn) = Xwfunc(Xz(i, mn), beta(i, mn))
Mw(i, mn) = Mach(gamma, Xw(i, mn))
Mz(i, mn) = Machz(M(i, mn), alpha(i, mn))

```

End Sub

## 8. Module mdlHubCalc Code

Option Explicit

Option Base 1

Public sigma(3, 3) As Double

' Solidity

Public Sub HubCalc(i As Integer)

' Hub Calculations

Xz(i, hub) = Xz(i, mn) ' Radial Equilibrium

Xtheta(i, hub) = Xthetafunc(R(i, mn), R(i, hub), Xtheta(i, mn))

alpha(i, hub) = alphafunc(Xtheta(i, hub), Xz(i, hub))

x(i, hub) = Xfunc(Xz(i, hub), alpha(i, hub))

Xu(i, hub) = Xufunc(R(i, mn), R(i, hub), Xu(i, mn)) ' for constant wheel speed

beta(i, hub) = betafunc(Xu(i, hub), Xtheta(i, hub), Xz(i, hub))

Xw(i, hub) = Xwfunc(Xz(i, hub), beta(i, hub))

M(i, hub) = Mach(gamma, x(i, hub))

Mw(i, hub) = Mach(gamma, Xw(i, hub))

Mz(i, hub) = Machz(M(i, hub), alpha(i, hub))

End Sub

## 9. Module mdlMeanCalc Code

```
Option Explicit
Option Base 1
Public Y(3, 3) As Double
' Dimensionless Local Velocity
Public Yw(3, 3) As Double
' Dimensionless Local Velocity Relative to the Blade
Public Yz(3, 3) As Double
' Dimensionless Local Velocity along the Axial Component
Public A31 As Double
' Ratio of alpha. Unity for a repeating stage.
Public D(3, 3) As Double
' Diffusion Factor
Public tau As Double
' Total temperature ratio
Public phi21 As Double
' Change in Axial Velocity across the Rotor.
Public phi32 As Double
' Change in Axial Velocity across the Stator.
Public phi2m As Double
' Change in Axial Velocity at the Rotor exit at the Mean Line.
Public phi1m As Double
' ratio of axial velocity to rotation velocity
Public Sub MeanCalc(i As Integer)
    ' Mean Calculations for the Rotor or Stator
    If i = 2 Then
        Dim temp As Double
        beta(i, mn) = Arcsin(SinB2(DiffA(sigma(i, mn), pitch(i), D(i, mn), phi21, beta(i
            - 1, mn)), DiffB(sigma(i, mn), pitch(i)), pitch(i)))
        Xu(i, mn) = pitch(i) * Xu(i - 1, mn)
        phi1m = Xz(i - 1, mn) / Xu(i - 1, mn)
        phi2m = phi21 * phi1m * (1 / pitch(i))
        Xz(i, mn) = phi2m * Xu(i, mn)
        Xtheta(i, mn) = Xu(i, mn) - Xz(i, mn) * Tan(DegToRad(beta(i, mn)))
        alpha(i, mn) = alphafunc(Xtheta(i, mn), Xz(i, mn))
        tau = taufunc(Xu(i, mn), Xtheta(i, mn), Xu(i - 1, mn), Xtheta(i - 1, mn))
    Else
```

```

        alpha(i, mn) = A31 * alpha(i - 2, mn)
        D(i, mn) = Diffusion(phi32, alpha(i - 1, mn), alpha(i, mn), pitch(i), sigma(i,
            mn))
        Xz(i, mn) = phi32 * Xz(i - 1, mn)
        Xtheta(i, mn) = Xz(i, mn) * Tan(DegToRad(alpha(i, mn)))
        Xu(i, mn) = Xu(i - 1, mn) * pitch(i)
        beta(i, mn) = betafunc(Xu(i, mn), Xtheta(i, mn), Xz(i, mn))
    End If
    rst(i, mn) = DofReaction(Xtheta(i - 1, mn), Xu(i - 1, mn), Xtheta(i, mn), Xu(i, mn))
    x(i, mn) = Xfunc(Xz(i, mn), alpha(i, mn))
    Xw(i, mn) = Xwfunc(Xz(i, mn), beta(i, mn))
    Y(i, mn) = Yfunc(x(i, mn), tau)
    Yw(i, mn) = Yfunc(Xw(i, mn), tau)
    M(i, mn) = Mach(gamma, Y(i, mn))
    Mw(i, mn) = Mach(gamma, Yw(i, mn))
    Mz(i, mn) = Machz(M(i, mn), alpha(i, mn))
End Sub

```

## 10. Module mdlStgPerformance

```

Option Explicit
Option Base 1
Public omegasftc(3) As Double
' Secondary flow and tip clearance loss
Public omegap(3) As Double
' Profile Loss
Public omegas(3) As Double
' Shock Loss
Public omegat(3) As Double
' Total Loss (secondary flow + tip clearance + profile)
Public TTt1(3) As Double
' Static to Total Temperature Ratio
Public PPt1(3) As Double
' Static to Total Pressure Ratio
Public Tr1Tt1 As Double
' Total Relative Temperature Ratio
Public Pr1Pt1 As Double
' Total Relative Pressure Ratio

```

```

Public TETt1(3) As Double
Public PEpt1(3) As Double
Public PtPt1(3) As Double
' Total Pressure Ratio
Public TtTt1(3) As Double
' Total Temperature Ratio
Public AA1(3) As Double
' Area constriction ratio
Public delta(3) As Double
' Tip Gap
Public Sub RotorPerf(i As Integer, loopcount As Integer)
    Dim ShLoss As Double
    omegap(i) = 2 * sigma(i, mn) * ((Cos(DegToRad(beta(i - 1, mn))) ^ 2) /
        (Cos(DegToRad(beta(i, mn))) ^ 3)) * (0.005 + (0.16 * (D(i, mn) ^ 4)))
    If loopcount > 1 Then
        If Mw(i - 1, mn) > 1 Then
            ShLoss = ((1 - ShockLoss(Mw(i - 1, mn), gamma)) / (1 - (1 + ((gamma
                - 1) / 2) * Mw(i - 1, mn) ^ 2) ^ (-1 * gg1(gamma))))
        End If
        omegas(i) = ShLoss
        omegasftc(i) = SFTC(beta(i - 1, mn), beta(i, mn), sigma(i, mn), h(i), delta(i),
            S(i))
    Else
        omegas(i) = 0
        omegasftc(i) = 0
    End If
    omegat(i) = omegap(i) + omegasftc(i) + omegas(i)
    If loopcount = 1 Then
        TTt1(i - 1) = 1 - (x(i - 1, mn) ^ 2)
        PPt1(i - 1) = TTt1(i - 1) ^ gg1(gamma)
        Tr1Tt1 = TTt1(i - 1) + (Xw(i - 1, mn) ^ 2)
        Pr1Pt1 = Tr1Tt1 ^ gg1(gamma)
        TETt1(i - 1) = Tr1Tt1 + (Xu(i, mn) ^ 2) - (Xu(i - 1, mn) ^ 2)
        PEpt1(i - 1) = TETt1(i - 1) ^ gg1(gamma)
    End If
    PEpt1(i) = PEpt1(i - 1) - (omegat(i) * (Pr1Pt1 - PPt1(i - 1)))
    TtTt1(i) = tau
    TETt1(i) = TETt1(i - 1)

```

```

PtPt1(i) = PEPt1(i) * ((TtTt1(i) / TETt1(i)) ^ gg1(gamma)) ' Rotor Compression ratio
TtTt1(i) = TtTt1(i) - (x(i, mn) ^ 2)
PPt1(i) = PtPt1(i) * ((TtTt1(i) / tau) ^ gg1(gamma))
Capphi(i, mn) = Y(i, mn) * ((1 - (Y(i, mn) ^ 2)) ^ g1(gamma))
AA1(i) = ((Capphi(i - 1, tip) * Cos(DegToRad(alpha(i - 1, tip)))) / (Capphi(i, mn) *
Cos(DegToRad(alpha(i, mn))))) * ((Sqr(TtTt1(i))) / PtPt1(i))
A(i) = AA1(i) * A(i - 1)
R(i, mn) = R(i - 1, mn) * pitch(i)
h(i) = A(i) / (2 * (22 / 7) * R(i, mn))
rht(i) = rhtfunc2(h(i), R(i, mn))
R(i, tip) = (2 / (1 + rht(i))) * R(i, mn)
R(i, hub) = rht(i) * R(i, tip)

```

End Sub

Public Sub StatorPerf(i As Integer, loopcount As Integer)

Dim ShLoss As Double

```

omegap(i) = 2 * sigma(i, mn) * ((Cos(DegToRad(alpha(i - 1, mn))) ^ 2) /
(Cos(DegToRad(alpha(i, mn))) ^ 3)) * (0.005 + (0.16 * (D(i, mn) ^ 4)))

```

If loopcount > 1 Then

    If M(i - 1, mn) > 1 Then

```

        ShLoss = ((1 - ShockLoss(M(i - 1, mn), gamma)) / (1 - (1 + ((gamma -
1) / 2) * M(i - 1, mn) ^ 2) ^ (-1 * gg1(gamma))))

```

    End If

    omegas(i) = ShLoss

```

    omegasftc(i) = SFTC(alpha(i - 1, mn), alpha(i, mn), sigma(i, mn), h(i), delta(i),
S(i))

```

Else

    omegas(i) = 0

    omegasftc(i) = 0

End If

```

omegat(i) = omegap(i) + omegasftc(i) + omegas(i)

```

```

PtPt1(i) = PtPt1(i - 1) - omegat(i) * (PtPt1(i - 1) - PPt1(i - 1))

```

```

TtTt1(i) = tau

```

```

TtTt1(i) = TtTt1(i) - (x(i, mn) ^ 2)

```

```

PPt1(i) = ((TtTt1(i) / TtTt1(i)) ^ gg1(gamma)) * PtPt1(i)

```

```

Capphi(i, mn) = Y(i, mn) * ((1 - (Y(i, mn) ^ 2)) ^ g1(gamma))

```

```

AA1(i) = ((Capphi(i - 2, tip) * Cos(DegToRad(alpha(i - 2, tip)))) / (Capphi(i, mn) *
Cos(DegToRad(alpha(i, mn))))) * ((Sqr(TtTt1(i))) / PtPt1(i))

```

```

A(i) = AA1(i) * A(i - 2)

```

```

R(i, mn) = R(i - 1, mn) * pitch(i)
h(i) = A(i) / (2 * (22 / 7) * R(i, mn))
rht(i) = rhtfunc2(h(i), R(i, mn))
R(i, tip) = (2 / (1 + rht(i))) * R(i, mn)
R(i, hub) = rht(i) * R(i, tip)

```

End Sub

## 11. Module mdlHubTipCalc Code

Option Explicit

Option Base 1

Dim l As Integer

Public fsigma(3) As Double

' Linear function of sigma

Public Sub HubTipCalc(i As Integer)

' Hub & Tip Calculations for the Rotor or Stator

For l = 1 To 3 Step 2

Xz(i, l) = Xz(i, mn)

Xtheta(i, l) = (R(i, mn) \* Xtheta(i, mn)) / R(i, l) ' Radial Equilibrium

Xu(i, l) = Xufunc(R(i, mn), R(i, l), Xu(i, mn)) 'for constant wheel speed

alpha(i, l) = alphafunc(Xtheta(i, l), Xz(i, l))

beta(i, l) = betafunc(Xu(i, l), Xtheta(i, l), Xz(i, l))

x(i, l) = Xfunc(Xz(i, l), alpha(i, l))

Xw(i, l) = Xwfunc(Xz(i, l), beta(i, l))

Y(i, l) = Yfunc(x(i, l), tau)

Yw(i, l) = Yfunc(Xw(i, l), tau)

M(i, l) = Mach(gamma, Y(i, l))

Mw(i, l) = Mach(gamma, Yw(i, l))

Mz(i, l) = Machz(M(i, l), alpha(i, l))

If l = 1 Then

    sigma(i, l) = sigma(i, mn) \* (2 - fsigma(i))

ElseIf l = 3 Then

    sigma(i, l) = sigma(i, mn) \* fsigma(i)

End If

If i = 2 Then

    D(i, l) = Diffusion(phi21, beta(i - 1, l), beta(i, l), pitch(i), sigma(i, l))

Else



```

                D(i, l) = Diffusion(phi32, alpha(i - 1, l), alpha(i, l), pitch(i), sigma(i, l))
            End If
            rst(i, l) = DofReaction(Xtheta(i - 1, l), Xu(i - 1, l), Xtheta(i, l), Xu(i, l))
        Next l
    End Sub

```

## 12. Module mdlBladeGeometry Code

```

Option Explicit
Option Base 1
Public AR(3) As Double
' Aspect Ratio
Public C(3) As Double
' Chord
Public Crev(3) As Double
' revised chord length
Public ARrev(3) As Double
' revised aspect ratio
Public Z(3) As Double
' Number of Blades calculated
Public intZ(3) As Integer
' Number of Blades chosen by the user.
Public h(3) As Double
' Blade height
Public S(3) As Double
' blade spacing
Public Sub BladeGeo(i As Integer, loopcount As Integer)
    h(i) = R(i, tip) - R(i, hub) ' blade height
    C(i) = h(i) / AR(i) ' Calculated chord length
    Z(i) = 2 * (22 / 7) * R(i, mn) * sigma(i, mn) / C(i) ' Calculated no. of blades
    If loopcount = 1 Then
        If i = 2 Then
            frmZ.lblZ.Caption = "The calculated no. of blades in the rotor (Zr) is "
                & Z(i)
        ElseIf i = 3 Then
            frmZ.lblZ.Caption = "The calculated no. of blades in the stator (Zs) is "
                & Z(i)
        End If
        frmZ.Show vbModal
    End Sub

```

```

        intZ(i) = frmZ.txtZ.Text
    End If
    ARrev(i) = h(i) / ((2 * (22 / 7) * R(i, mn) * sigma(i, mn)) / intZ(i)) ' Revised aspect ratio
    frmZ.txtZ.Text = ""
    Crev(i) = h(i) / ARrev(i) ' Revised chord length
    S(i) = Crev(i) / sigma(i, mn) ' Blade spacing
End Sub

```

### 13. Module mdlIncidence Code

Option Explicit

Option Base 1

```

Public i0(6, 9) As Double, slopen(7, 9) As Double, ikit(6) As Double, i0delta0(6, 9) As Double,
    slopemn(7, 9) As Double, Kit(7, 7) As Double, d0(6, 9) As Double, slopem(7, 9) As
    Double, dkit(6) As Double

```

' X values for 6th order curve fit polynomial.

```

Public i010(3, 3) As Double

```

' Zero-camber incidence angle

```

Public d010(3, 3) As Double

```

' Zero-camber deviation angle

```

Public N(3, 3) As Double

```

' incidence angle slope factor n

```

Public ikt(3, 3) As Double

```

' incidence angle correction factor for thickness

```

Public dkt(3, 3) As Double

```

' deviation angle correction factor for thickness

```

Public i0ref(3, 3) As Double

```

' reference incidence angle

```

Public d0ref(3, 3) As Double

```

' reference deviation angle

```

Public i2d As Double

```

' 2 dimensional incidence angle

```

Public icor(3, 3) As Double

```

' corrected 2 dimensional incidence angle

```

Public dref(3, 3) As Double

```

' deviation angle

```

Public camber(3, 3) As Double

```

' camber angle

```

Public i0d0(3, 3) As Double

```

```

' variation of i0 - d0
Public ktbar(3, 3) As Double
' camber angle correction factor for thickness
Public onemn(3, 3) As Double
' camber angle slope factor 1 -m+n
Public dm(3, 3) As Double
' deviation angle slope factor m
Public tc(3, 3) As Double
' thickness to cord ratio.
Public k As Integer
Dim o As Integer, p As Single
Public Xvar() As Double
Public Yvar() As Double
Public Sub Incidence(i As Integer, j As Integer, slopegraph As Boolean, ksh As Single)
    ' Variation of (i0)10-(delta0)10
    ' Load constants
    ' solidity = 0.4
    i0delta0(6, 1) = -1.72244891587855E-11
    i0delta0(5, 1) = 3.05183134666209E-09
    i0delta0(4, 1) = -2.54582401992831E-07
    i0delta0(3, 1) = 8.9308266844057E-06
    i0delta0(2, 1) = -1.64583732868095E-04
    i0delta0(1, 1) = 2.36162560875073E-02
    ' solidity = 0.6
    i0delta0(6, 2) = -1.21461996934098E-10
    i0delta0(5, 2) = 2.44632274559037E-08
    i0delta0(4, 2) = -1.89083802948353E-06
    i0delta0(3, 2) = 6.51024967552871E-05
    i0delta0(2, 2) = -1.10036026944726E-03
    i0delta0(1, 2) = 4.37180120798075E-02
    ' solidity = 0.8
    i0delta0(6, 3) = -1.56214579635869E-10
    i0delta0(5, 3) = 3.09609686430234E-08
    i0delta0(4, 3) = -2.3589555206982E-06
    i0delta0(3, 3) = 7.92058315148836E-05
    i0delta0(2, 3) = -1.27482005365209E-03
    i0delta0(1, 3) = 5.69282884198401E-02

```

' solidity = 1.0  
i0delta0(6, 4) = -6.93736034940097E-11  
i0delta0(5, 4) = 8.79693724809005E-09  
i0delta0(4, 4) = -3.60272149557694E-07  
i0delta0(3, 4) = -4.42503626629787E-07  
i0delta0(2, 4) = 1.21654421718631E-05  
i0delta0(1, 4) = 6.52732436619772E-02  
' solidity = 1.2  
i0delta0(6, 5) = 1.04197027145803E-10  
i0delta0(5, 5) = -2.10810745440021E-08  
i0delta0(4, 5) = 1.37089527130208E-06  
i0delta0(3, 5) = -3.80616685049517E-05  
i0delta0(2, 5) = 8.34875831969839E-05  
i0delta0(1, 5) = 8.43313899049463E-02  
' solidity = 1.4  
i0delta0(6, 6) = 5.17847890355591E-11  
i0delta0(5, 6) = -1.11055450426056E-08  
i0delta0(4, 6) = 6.3411319506379E-07  
i0delta0(3, 6) = -1.51366527276764E-05  
i0delta0(2, 6) = -1.39016582579643E-04  
i0delta0(1, 6) = 9.70746619623242E-02  
' solidity = 1.6  
i0delta0(6, 7) = -2.08323213348361E-10  
i0delta0(5, 7) = 3.63757529792119E-08  
i0delta0(4, 7) = -2.51178491095239E-06  
i0delta0(3, 7) = 7.46391658452694E-05  
i0delta0(2, 7) = -1.21453189910881E-03  
i0delta0(1, 7) = 0.11686046293471  
' solidity = 1.8  
i0delta0(6, 8) = -1.56143738685847E-10  
i0delta0(5, 8) = 2.10079058766965E-08  
i0delta0(4, 8) = -9.83116558606056E-07  
i0delta0(3, 8) = 6.88832778905635E-06  
i0delta0(2, 8) = 6.30398362773121E-05  
i0delta0(1, 8) = 0.124576532031824  
' solidity = 2  
i0delta0(6, 9) = -3.47201982252689E-10

```

i0delta0(5, 9) = 6.02515059199005E-08
i0delta0(4, 9) = -4.22495870910922E-06
i0delta0(3, 9) = 1.38861665249124E-04
i0delta0(2, 9) = -2.50961937126704E-03
i0delta0(1, 9) = 0.157387592875239

k = 9
ReDim curve(k)
ReDim Xvar(k)
ReDim Yvar(k)
p = 0.4
For o = 1 To k
    Yvar(o) = CurveFit2(i0delta0(1, o), i0delta0(2, o), i0delta0(3, o), i0delta0(4, o),
        i0delta0(5, o), i0delta0(6, o), beta(i, j))
    Xvar(o) = p
    p = p + 0.2
Next o
QuadCoeff k
i0d0(i, j) = Interp(sigma(i, j))
If slopegraph = True Then
    ' NACA 65-(A10)-series blades as equivalent circular arc
    ' Load constants
    ' solidity = 0.4
    slopemn(7, 1) = 2.08333333236381E-11
    slopemn(6, 1) = -4.31089743405371E-09
    slopemn(5, 1) = 3.42948717823449E-07
    slopemn(4, 1) = -1.2816870624599E-05
    slopemn(3, 1) = 1.47926864929815E-04
    slopemn(2, 1) = -3.97852565922108E-03
    slopemn(1, 1) = 0.53497377639842
    ' solidity = 0.6
    slopemn(7, 2) = -3.47222221982991E-12
    slopemn(6, 2) = 7.772435880668E-10
    slopemn(5, 2) = -5.87606836521815E-08
    slopemn(4, 2) = 1.3414189909966E-06
    slopemn(3, 2) = -5.4709838117617E-05
    slopemn(2, 2) = -2.55785261049368E-03
    slopemn(1, 2) = 0.675027681002291

```

' solidity = 0.8  
slopemmn(7, 3) = -5.0821976835258E-21  
slopemmn(6, 3) = -1.28205128154327E-10  
slopemmn(5, 3) = 1.20192307773159E-08  
slopemmn(4, 3) = -6.92016318915023E-07  
slopemmn(3, 3) = -3.31075165860284E-05  
slopemmn(2, 3) = -2.12211544896945E-03  
slopemmn(1, 3) = 0.750014569226494

' solidity = 1.0  
slopemmn(7, 4) = -6.94444444304795E-12  
slopemmn(6, 4) = 1.20192307712444E-09  
slopemmn(5, 4) = -7.6655982672591E-08  
slopemmn(4, 4) = 1.48528553811644E-06  
slopemmn(3, 4) = -4.01670539815768E-05  
slopemmn(2, 4) = -1.64423084743248E-03  
slopemmn(1, 4) = 0.794953380497141

' solidity = 1.2  
slopemmn(7, 5) = -2.77777777637215E-11  
slopemmn(6, 5) = 5.48076922735063E-09  
slopemmn(5, 5) = -4.03579059504722E-07  
slopemmn(4, 5) = 1.27039626889314E-05  
slopemmn(3, 5) = -2.01934244898894E-04  
slopemmn(2, 5) = -3.78525730411639E-04  
slopemmn(1, 5) = 0.824973776832628

' solidity = 1.4  
slopemmn(7, 6) = 6.94444443457762E-12  
slopemmn(6, 6) = -9.1346153644617E-10  
slopemmn(5, 6) = 1.5758547106115E-08  
slopemmn(4, 6) = 1.08027389256193E-06  
slopemmn(3, 6) = -7.76942489579824E-05  
slopemmn(2, 6) = -3.57051379069162E-04  
slopemmn(1, 6) = 0.850023310682502

' solidity = 1.6  
slopemmn(7, 7) = -1.3888888844018E-11  
slopemmn(6, 7) = 3.07692307570384E-09  
slopemmn(5, 7) = -2.60683760439084E-07  
slopemmn(4, 7) = 9.44930068769168E-06

```

slopemn(3, 7) = -1.87603922285007E-04
slopemn(2, 7) = 6.39102459899732E-04
slopemn(1, 7) = 0.870029138228418
' solidity = 1.8
slopemn(7, 8) = -6.944444444643608E-12
slopemn(6, 8) = 1.84294871811291E-09
slopemn(5, 8) = -1.7841880317615E-07
slopemn(4, 8) = 6.76354894046938E-06
slopemn(3, 8) = -1.36371890420151E-04
slopemn(2, 8) = 3.83012708653041E-04
slopemn(1, 8) = 0.889956294448098
' solidity = 2
slopemn(7, 9) = -1.04166666679601E-11
slopemn(6, 9) = 2.3637820511721E-09
slopemn(5, 9) = -2.13141025329211E-07
slopemn(4, 9) = 8.38760196941735E-06
slopemn(3, 9) = -1.82296764080547E-04
slopemn(2, 9) = 1.1642627027868E-03
slopemn(1, 9) = 0.900013112661114
k = 9
ReDim curve(k)
ReDim Xvar(k)
ReDim Yvar(k)
p = 0.4
For o = 1 To k
    Yvar(o) = CurveFit1(slopemn(1, o), slopemn(2, o), slopemn(3, o),
        slopemn(4, o), slopemn(5, o), slopemn(6, o), slopemn(7, o),
        beta(i, j))
    Xvar(o) = p
    p = p + 0.2
Next o
QuadCoeff k
onemn(i, j) = Interp(sigma(i, j))
Else
' Circular arc mean line blades
' Load constants
' solidity = 0.4
slopemn(7, 1) = -4.16666666439411E-11

```

slopemmn(6, 1) = 8.14102563624798E-09  
slopemmn(5, 1) = -5.80929486814364E-07  
slopemmn(4, 1) = 1.81949300572665E-05  
slopemmn(3, 1) = -2.4787150325345E-04  
slopemmn(2, 1) = -3.33942308314938E-03  
slopemmn(1, 1) = 0.350002913822904  
' solidity = 0.6  
slopemmn(7, 2) = 6.94444443965982E-12  
slopemmn(6, 2) = -1.4903846145501E-09  
slopemmn(5, 2) = 1.06303418803688E-07  
slopemmn(4, 2) = -3.08493589651349E-06  
slopemmn(3, 2) = -5.89209358992093E-06  
slopemmn(2, 2) = -2.75032054841517E-03  
slopemmn(1, 2) = 0.545032051554482  
' solidity = 0.8  
slopemmn(7, 3) = -1.04166666603368E-11  
slopemmn(6, 3) = 1.56249999787653E-09  
slopemmn(5, 3) = -7.29166664409364E-08  
slopemmn(4, 3) = 1.18371202617595E-07  
slopemmn(3, 3) = 2.38731068833431E-05  
slopemmn(2, 3) = -3.17708338894818E-03  
slopemmn(1, 3) = 0.649981061002052  
' solidity = 1.0  
slopemmn(7, 4) = -6.94444443796575E-12  
slopemmn(6, 4) = 7.21153844973621E-10  
slopemmn(5, 4) = -2.93803398276893E-09  
slopemmn(4, 4) = -2.18458625589335E-06  
slopemmn(3, 4) = 3.70765356052516E-05  
slopemmn(2, 4) = -2.16987186519191E-03  
slopemmn(1, 4) = 0.715017483006385  
' solidity = 1.2  
slopemmn(7, 5) = 3.47222221644178E-12  
slopemmn(6, 5) = -1.32211538505372E-09  
slopemmn(5, 5) = 1.4369658127289E-07  
slopemmn(4, 5) = -6.95767774239187E-06  
slopemmn(3, 5) = 1.06356110350703E-04  
slopemmn(2, 5) = -2.01842956960263E-03



slopemmn(1, 5) = 0.760024767461402

' solidity = 1.4

slopemmn(7, 6) = -6.7762635780344E-21

slopemmn(6, 6) = -1.2820512967221E-10

slopemmn(5, 6) = 1.20192308605827E-08

slopemmn(4, 6) = -8.43531474004067E-07

slopemmn(3, 6) = -1.71984251977619E-05

slopemmn(2, 6) = -7.05448809185327E-04

slopemmn(1, 6) = 0.794938811805281

' solidity = 1.6

slopemmn(7, 7) = 1.73611111042317E-11

slopemmn(6, 7) = -3.34134615158702E-09

slopemmn(5, 7) = 2.297008545038E-07

slopemmn(4, 7) = -7.7196241337063E-06

slopemmn(3, 7) = 9.70923186827122E-05

slopemmn(2, 7) = -1.42612189358715E-03

slopemmn(1, 7) = 0.825036422577128

' solidity = 1.8

slopemmn(7, 8) = 1.73611110991495E-11

slopemmn(6, 8) = -3.37339743378823E-09

slopemmn(5, 8) = 2.35309829010877E-07

slopemmn(4, 8) = -7.93524184317107E-06

slopemmn(3, 8) = 9.22482045950801E-05

slopemmn(2, 8) = -8.26442413767836E-04

slopemmn(1, 8) = 0.844992716324796

' solidity = 2

slopemmn(7, 9) = 3.47222221135958E-12

slopemmn(6, 9) = -5.84935897461614E-10

slopemmn(5, 9) = 3.55235043048019E-08

slopemmn(4, 9) = -2.03634907514072E-06

slopemmn(3, 9) = 3.84146771352789E-05

slopemmn(2, 9) = -6.8605780506914E-04

slopemmn(1, 9) = 0.859969406337427

k = 9

ReDim curve(k)

ReDim Xvar(k)

ReDim Yvar(k)

```

p = 0.4
For o = 1 To k
    Yvar(o) = CurveFit1(slopemn(1, o), slopemn(2, o), slopemn(3, o),
        slopemn(4, o), slopemn(5, o), slopemn(6, o), slopemn(7, o),
        beta(i, j))
    Xvar(o) = p
    p = p + 0.2
Next o
QuadCoeff k
onemn(i, j) = Interp(sigma(i, j))
End If
' Variation of thickness-correction factor Kt for camber calculation
' Load constants
' beta1 = 10
Kit(7, 1) = 816993.464355469
Kit(6, 1) = -351150.076196289
Kit(5, 1) = 61737.9966625977
Kit(4, 1) = -5315.17809592133
Kit(3, 1) = 142.41942977427
Kit(2, 1) = 13.4581061812941
Kit(1, 1) = 6.50000014506098E-02
' beta1 = 20
Kit(7, 2) = 1077614.37939453
Kit(6, 2) = -459489.065126953
Kit(5, 2) = 79133.1385789185
Kit(4, 2) = -6710.73264049728
Kit(3, 2) = 201.572413791658
Kit(2, 2) = 12.2108848959033
Kit(1, 2) = 7.74781832012336E-02
' beta1 = 30
Kit(7, 3) = 796568.628417969
Kit(6, 3) = -338565.234250488
Kit(5, 3) = 58401.6780760498
Kit(4, 3) = -4855.18434412186
Kit(3, 3) = 103.679839050816
Kit(2, 3) = 15.0572606819245
Kit(1, 3) = 6.05909105273496E-02
' beta1 = 40

```

```

Kit(7, 4) = -183823.529541016
Kit(6, 4) = 137302.036435547
Kit(5, 4) = -32831.3536986084
Kit(4, 4) = 3879.52703175537
Kit(3, 4) = -335.438802558397
Kit(2, 4) = 26.0388210932938
Kit(1, 4) = -3.53636350253408E-02
' beta1 = 50
Kit(7, 5) = -449346.408691406
Kit(6, 5) = 260840.875805664
Kit(5, 5) = -56572.084102478
Kit(4, 5) = 6297.74699841156
Kit(3, 5) = -479.565571368521
Kit(2, 5) = 30.7062532322958
Kit(1, 5) = -7.44999987640929E-02
' beta1 = 60
Kit(7, 6) = 2879901.96362305
Kit(6, 6) = -1181513.95310303
Kit(5, 6) = 193177.319282959
Kit(4, 6) = -15656.7577867749
Kit(3, 6) = 525.58354015793
Kit(2, 6) = 8.91909924834078
Kit(1, 6) = 0.126909092425712
' beta1 = 70
Kit(7, 7) = 5187908.49780273
Kit(6, 7) = -1994626.6972876
Kit(5, 7) = 298546.694419434
Kit(4, 7) = -21587.099794791
Kit(3, 7) = 600.425619817768
Kit(2, 7) = 13.8798799771508
Kit(1, 7) = 9.83181832073486E-02
k = 7
ReDim curve(k)
ReDim Xvar(k)
ReDim Yvar(k)
p = 10
For o = 1 To k

```

Yvar(o) = CurveFit1(Kit(1, o), Kit(2, o), Kit(3, o), Kit(4, o), Kit(5, o), Kit(6, o),  
Kit(7, o), tc(i, j))

Xvar(o) = p

p = p + 10

Next o

QuadCoeff k

ktbar(i, j) = Interp(beta(i, j))

camber(i, j) = camberfunc(beta(i, j), beta((i - 1), j), ksh, ktbar(i, j), i0d0(i, j), onemn(i, j))

' Zero-camber incidence angle

' Load constants

' solidity = 0.4

i0(6, 1) = -4.04805786872846E-14

i0(5, 1) = 3.30321577382553E-10

i0(4, 1) = -1.61193689951489E-07

i0(3, 1) = 1.60266684012811E-05

i0(2, 1) = -6.12705630658184E-04

i0(1, 1) = 3.96414794354314E-02

' solidity = 0.6

i0(6, 2) = 2.77737297393952E-10

i0(5, 2) = -5.8003011805044E-08

i0(4, 2) = 4.49158409132622E-06

i0(3, 2) = -1.58973331821244E-04

i0(2, 2) = 2.41923882140327E-03

i0(1, 2) = 3.77248126474115E-02

' solidity = 0.8

i0(6, 3) = -2.77737297421058E-10

i0(5, 3) = 5.38363451353663E-08

i0(4, 3) = -3.86658408690899E-06

i0(3, 3) = 1.2355666447661E-04

i0(2, 3) = -1.73173878386024E-03

i0(1, 3) = 7.33585199368463E-02

' solidity = 1.0

i0(6, 4) = -6.24048706766443E-10

i0(5, 4) = 1.33904109689276E-07

i0(4, 4) = -1.07952815886492E-05

i0(3, 4) = 3.96289954153417E-04

i0(2, 4) = -6.38683407169083E-03

$i_0(1, 4) = 0.11471689445807$   
 ' solidity = 1.2  
 $i_0(6, 5) = 1.3907105163107E-10$   
 $i_0(5, 5) = -2.85697804719431E-08$   
 $i_0(4, 5) = 2.01009383982154E-06$   
 $i_0(3, 5) = -5.64950093888683E-05$   
 $i_0(2, 5) = 3.77314309162102E-04$   
 $i_0(1, 5) = 0.100321674263796$   
 ' solidity = 1.4  
 $i_0(6, 6) = -1.04116066001981E-10$   
 $i_0(5, 6) = 2.04204313875023E-08$   
 $i_0(4, 6) = -1.67350788249365E-06$   
 $i_0(3, 6) = 6.85083302869316E-05$   
 $i_0(2, 6) = -1.42057624429981E-03$   
 $i_0(1, 6) = 0.123885649683871$   
 ' solidity = 1.6  
 $i_0(6, 7) = -6.59874024969446E-10$   
 $i_0(5, 7) = 1.26238706023296E-07$   
 $i_0(4, 7) = -9.07669856742288E-06$   
 $i_0(3, 7) = 3.00725006795233E-04$   
 $i_0(2, 7) = -4.56882667162972E-03$   
 $i_0(1, 7) = 0.153343047833914$   
 ' solidity = 1.8  
 $i_0(6, 8) = -2.42843032737926E-10$   
 $i_0(5, 8) = 3.99324784211563E-08$   
 $i_0(4, 8) = -2.4176220057015E-06$   
 $i_0(3, 8) = 6.48183223432852E-05$   
 $i_0(2, 8) = -8.29475889986497E-04$   
 $i_0(1, 8) = 0.149069730896372$   
 ' solidity = 2  
 $i_0(6, 9) = -6.5928705639891E-10$   
 $i_0(5, 9) = 1.27699043138418E-07$   
 $i_0(4, 9) = -9.55189003892798E-06$   
 $i_0(3, 9) = 3.42296645044371E-04$   
 $i_0(2, 9) = -5.90334486059874E-03$   
 $i_0(1, 9) = 0.198583259410952$   
 k = 9

```

ReDim curve(k)
ReDim Xvar(k)
ReDim Yvar(k)
p = 0.4
For o = 1 To k
    Yvar(o) = CurveFit2(i0(1, o), i0(2, o), i0(3, o), i0(4, o), i0(5, o), i0(6, o), beta(i,
        j))
    Xvar(o) = p
    p = p + 0.2
Next o
QuadCoeff k
i010(i, j) = Interp(sigma(i, j))
' Minimum loss incidence angle slope factor
' Load constants
' solidity = 0.4
slopen(7, 1) = 5.20833333567409E-12
slopen(6, 1) = -1.00560897412991E-09
slopen(5, 1) = 7.05128204714356E-08
slopen(4, 1) = -2.35449445540326E-06
slopen(3, 1) = 7.51638881979488E-06
slopen(2, 1) = -3.64078518850874E-03
slopen(1, 1) = -5.00123838208282E-02
' solidity = 0.6
slopen(7, 2) = -1.73611110737386E-12
slopen(6, 2) = 2.60416666312754E-10
slopen(5, 2) = -2.25694444522251E-08
slopen(4, 2) = 1.0866477326843E-06
slopen(3, 2) = -5.59643317217251E-05
slopen(2, 2) = -2.28645827399987E-03
slopen(1, 2) = -4.49905306238207E-02
' solidity = 0.8
slopen(7, 3) = 6.94444444474202E-12
slopen(6, 3) = -1.85897435877984E-09
slopen(5, 3) = 1.70806623789321E-07
slopen(4, 3) = -7.15544871177087E-06
slopen(3, 3) = 1.05446046163138E-04
slopen(2, 3) = -2.7290063578107E-03

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slopen(1, 3) = -4.00160259214886E-02  
' solidity = 1.0  
slopen(7, 4) = -5.2083333280508E-12  
slopen(6, 4) = 9.57532051044929E-10  
slopen(5, 4) = -7.77243589489274E-08  
slopen(4, 4) = 3.08220425893069E-06  
slopen(3, 4) = -8.76518800509984E-05  
slopen(2, 4) = -8.65945466387075E-04  
slopen(1, 4) = -3.49963580541726E-02  
' solidity = 1.2  
slopen(7, 5) = 2.6041666658887E-11  
slopen(6, 5) = -5.73317307430571E-09  
slopen(5, 5) = 4.60336538235517E-07  
slopen(4, 5) = -1.68285620523179E-05  
slopen(3, 5) = 2.38823935717392E-04  
slopen(2, 5) = -2.12556085602955E-03  
slopen(1, 5) = -2.99817892565741E-02  
' solidity = 1.4  
slopen(7, 6) = 1.56249999943168E-11  
slopen(6, 6) = -3.43349358927075E-09  
slopen(5, 6) = 2.74038461367532E-07  
slopen(4, 6) = -1.01127258078648E-05  
slopen(3, 6) = 1.33344623499454E-04  
slopen(2, 6) = -1.06402239998715E-03  
slopen(1, 6) = -2.49992717449814E-02  
' solidity = 1.6  
slopen(7, 7) = 1.56249999951638E-11  
slopen(6, 7) = -3.32131410091599E-09  
slopen(5, 7) = 2.54407051133998E-07  
slopen(4, 7) = -8.82776077215652E-06  
slopen(3, 7) = 9.46172051285998E-05  
slopen(2, 7) = -2.87900609066583E-04  
slopen(1, 7) = -1.99978148450413E-02  
' solidity = 1.8  
slopen(7, 8) = -5.20833332889783E-12  
slopen(6, 8) = 1.11778846096679E-09  
slopen(5, 8) = -9.01442307604805E-08

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slopen(4, 8) = 2.80612616787579E-06
slopen(3, 8) = -5.87438087080727E-05
slopen(2, 8) = 3.75240412154199E-04
slopen(1, 8) = -0.014986159811361
' solidity = 2
slopen(7, 9) = 1.2152777732163E-11
slopen(6, 9) = -2.31971153754913E-09
slopen(5, 9) = 1.6159188022391E-07
slopen(4, 9) = -5.68345716178698E-06
slopen(3, 9) = 7.84089690597511E-05
slopen(2, 9) = -3.66426257727426E-04
slopen(1, 9) = -9.98615979092321E-03
k = 9
ReDim curve(k)
ReDim Xvar(k)
ReDim Yvar(k)
p = 0.4
For o = 1 To k
    Yvar(o) = CurveFit1(slopen(1, o), slopen(2, o), slopen(3, o), slopen(4, o),
        slopen(5, o), slopen(6, o), slopen(7, o), beta(i, j))
    Xvar(o) = p
    p = p + 0.2
Next o
QuadCoeff k
N(i, j) = Interp(sigma(i, j))
' Maximum thickness correction factor
' Load constants
ikit(6) = -748795.365783691
ikit(5) = 243951.67288208
ikit(4) = -28087.2979736328
ikit(3) = 1612.26135325431
ikit(2) = -137.429116554558
ikit(1) = 18.8187430176185
ikt(i, j) = CurveFit2(ikit(1), ikit(2), ikit(3), ikit(4), ikit(5), ikit(6), tc(i, j))
i0ref(i, j) = ksh * ikt(i, j) * i010(i, j)
i2d = i0ref(i, j) + N(i, j) * camber(i, j)
If i = 2 Then

```



```

    If ksh = 0.7 Then
        icor(i, j) = 0.7238 * Mw(i - 1, j) + 7.5481 + i2d
    ElseIf ksh = 1.1 Then
        icor(i, j) = 1.3026 * Mw(i - 1, j) + 5.738 + i2d
    ElseIf ksh = 1 Then
        icor(i, j) = i2d
    End If
ElseIf i = 3 Then
    If ksh = 0.7 Then
        icor(i, j) = 0.7238 * M(i - 1, j) + 7.5481 + i2d
    ElseIf ksh = 1.1 Then
        icor(i, j) = 1.3026 * M(i - 1, j) + 5.738 + i2d
    ElseIf ksh = 1 Then
        icor(i, j) = i2d
    End If
End If
' Zero-camber deviation angle
' Load constants
' solidity = 0.4
d0(6, 1) = -6.95861265439764E-11
d0(5, 1) = 1.57394588647108E-08
d0(4, 1) = -1.36278903151155E-06
d0(3, 1) = 5.7135006738207E-05
d0(2, 1) = -1.06391418466956E-03
d0(1, 1) = 1.59951786608872E-02
' solidity = 0.6
d0(6, 2) = -7.08410313374729E-14
d0(5, 2) = -4.63603904397869E-10
d0(4, 2) = 1.86661040402214E-07
d0(3, 2) = -1.62241633923088E-05
d0(2, 2) = 6.30890134971196E-04
d0(1, 2) = 5.06008922957335E-03
' solidity = 0.8
d0(6, 3) = -1.72852100539214E-11
d0(5, 3) = 3.54731371186856E-09
d0(4, 3) = -1.83872938541718E-07
d0(3, 3) = 1.7208295339799E-06

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d0(2, 3) = 2.60107809708643E-04  
d0(1, 3) = 9.95347546358971E-03  
' solidity = 1.0  
d0(6, 4) = 1.91189805496704E-10  
d0(5, 4) = -3.92754785100841E-08  
d0(4, 4) = 3.08863831766093E-06  
d0(3, 4) = -1.10622510739233E-04  
d0(2, 4) = 2.00666089165225E-03  
d0(1, 4) = 9.99963312096952E-04  
' solidity = 1.2  
d0(6, 5) = -2.95336231991993E-10  
d0(5, 5) = 6.09853177350322E-08  
d0(4, 5) = -4.62262480382947E-06  
d0(3, 5) = 1.62505009349445E-04  
d0(2, 5) = -2.28780804479811E-03  
d0(1, 5) = 2.54709629980425E-02  
' solidity = 1.4  
d0(6, 6) = -1.75483338526582E-11  
d0(5, 6) = 1.52773729431011E-09  
d0(4, 6) = 2.26701400096729E-07  
d0(3, 6) = -2.11891579624535E-05  
d0(2, 6) = 8.81687814285215E-04  
d0(1, 6) = 7.87309303404982E-03  
' solidity = 1.6  
d0(6, 7) = -3.46716215172916E-11  
d0(5, 7) = 7.92043135938725E-09  
d0(4, 7) = -5.62396773595708E-07  
d0(3, 7) = 2.2674997246952E-05  
d0(2, 7) = -1.57381818780777E-04  
d0(1, 7) = 0.017343983408864  
' solidity = 1.8  
d0(6, 8) = 6.30485119950015E-11  
d0(5, 8) = -1.41425240546278E-08  
d0(4, 8) = 1.37167452307629E-06  
d0(3, 8) = -5.62863600421792E-05  
d0(2, 8) = 1.32778646161569E-03  
d0(1, 8) = 8.46711704980407E-03

```

'solidity = 2
d0(6, 9) = 8.67296545047297E-11
d0(5, 9) = -1.60473137209016E-08
d0(4, 9) = 1.29498405332384E-06
d0(3, 9) = -4.33874967669112E-05
d0(2, 9) = 8.78086666489253E-04
d0(1, 9) = 1.43381905636488E-02
k = 9
ReDim curve(k)
ReDim Xvar(k)
ReDim Yvar(k)
p = 0.4
For o = 1 To k
    Yvar(o) = CurveFit2(d0(1, o), d0(2, o), d0(3, o), d0(4, o), d0(5, o), d0(6, o),
        beta(i, j))
    Xvar(o) = p
    p = p + 0.2
Next o
QuadCoeff k
d010(i, j) = Interp(sigma(i, j))
If slopegraph = True Then
    ' NACA 65-(A10)-series blades as equivalent circular arc
    ' Load constants
    ' solidity = 0.4
    slopem(7, 1) = 6.944444443457762E-12
    slopem(6, 1) = -1.49038461433326E-09
    slopem(5, 1) = 1.06303418845322E-07
    slopem(4, 1) = -3.16069348027526E-06
    slopem(3, 1) = 7.70624526893471E-05
    slopem(2, 1) = -7.91987265529315E-04
    slopem(1, 1) = 0.412494173012831
    ' solidity = 0.6
    slopem(7, 2) = 2.08333333206735E-11
    slopem(6, 2) = -4.48717948388355E-09
    slopem(5, 2) = 3.52964743544071E-07
    slopem(4, 2) = -1.22224650365155E-05
    slopem(3, 2) = 2.05185752662373E-04

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slopem(2, 2) = -8.88621860667627E-04

slopem(1, 2) = 0.277498543514405

' solidity = 0.8

slopem(7, 3) = 1.04166666611838E-11

slopem(6, 3) = -2.20352563908184E-09

slopem(5, 3) = 1.64262820512295E-07

slopem(4, 3) = -4.77163461454211E-06

slopem(3, 3) = 6.08733981977139E-05

slopem(2, 3) = 2.12339688573593E-04

slopem(1, 3) = 0.210016025961522

' solidity = 1.0

slopem(7, 4) = 3.47222221813584E-12

slopem(6, 4) = -1.19391025581519E-09

slopem(5, 4) = 1.31677350481696E-07

slopem(4, 4) = -5.84899476141487E-06

slopem(3, 4) = 1.26963627380405E-04

slopem(2, 4) = -5.62980817107928E-04

slopem(1, 4) = 0.170010198410182

' solidity = 1.2

slopem(7, 5) = 5.2083333305919E-12

slopem(6, 5) = -1.51842948674721E-09

slopem(5, 5) = 1.55048076988518E-07

slopem(4, 5) = -6.59036276573488E-06

slopem(3, 5) = 1.3337230542021E-04

slopem(2, 5) = -5.56330170923047E-04

slopem(1, 5) = 0.142489073668344

' solidity = 1.4

slopem(7, 6) = 2.25694444314355E-11

slopem(6, 6) = -4.79567307436549E-09

slopem(5, 6) = 3.83947649437721E-07

slopem(4, 6) = -1.38976908479194E-05

slopem(3, 6) = 2.37974820819886E-04

slopem(2, 6) = -1.0776442692304E-03

slopem(1, 6) = 0.122499271780747

' solidity = 1.6

slopem(7, 7) = -1.0416666620308E-11

slopem(6, 7) = 1.94711538320687E-09

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slopem(5, 7) = -1.29807692192396E-07
slopem(4, 7) = 4.01260197557818E-06
slopem(3, 7) = -4.06300984678865E-05
slopem(2, 7) = 3.55929451188786E-04
slopem(1, 7) = 0.107513112087279
' solidity = 1.8
slopem(7, 8) = 1.21527777736398E-11
slopem(6, 8) = -2.80048076742312E-09
slopem(5, 8) = 2.45726495706755E-07
slopem(4, 8) = -9.71317744902223E-06
slopem(3, 8) = 1.83019983943211E-04
slopem(2, 8) = -8.29567340645099E-04
slopem(1, 8) = 9.50021854990979E-02
' solidity = 2
slopem(7, 9) = -3.47222222152398E-12
slopem(6, 9) = 6.00961538020119E-10
slopem(5, 9) = -3.31196580577453E-08
slopem(4, 9) = 8.84688224900287E-07
slopem(3, 9) = 4.18366859378239E-07
slopem(2, 9) = 1.88301250858558E-04
slopem(1, 9) = 8.74956295422606E-02
k = 9
ReDim curve(k)
ReDim Xvar(k)
ReDim Yvar(k)
p = 0.4
For o = 1 To k
    Yvar(o) = CurveFit1(slopem(1, o), slopem(2, o), slopem(3, o),
        slopem(4, o), slopem(5, o), slopem(6, o), slopem(7, o), beta(i,
            j))
    Xvar(o) = p
    p = p + 0.2
Next o
QuadCoeff k
dm(i, j) = Interp(sigma(i, j))
Else
' Circular arc mean line blades
' Load constants

```

' solidity = 0.4  
slopem(7, 1) = -5.0821976835258E-21  
slopem(6, 1) = 6.73076922756005E-10  
slopem(5, 1) = -1.1258012813653E-07  
slopem(4, 1) = 6.10941141054866E-06  
slopem(3, 1) = -1.28908069711997E-04  
slopem(2, 1) = 1.04214733619301E-03  
slopem(1, 1) = 0.602489802490481

' solidity = 0.6  
slopem(7, 2) = 5.20833332212157E-12  
slopem(6, 2) = -1.08573717811505E-09  
slopem(5, 2) = 8.45352564893265E-08  
slopem(4, 2) = -3.08293269490889E-06  
slopem(3, 2) = 5.90424689903557E-05  
slopem(2, 2) = -9.9919948297611E-05  
slopem(1, 2) = 0.409991987649079

' solidity = 0.8  
slopem(7, 3) = 1.73611110229166E-12  
slopem(6, 3) = -1.9631410169349E-10  
slopem(5, 3) = 9.34829047505303E-10  
slopem(4, 3) = 6.51405884788403E-07  
slopem(3, 3) = -1.73966821961358E-05  
slopem(2, 3) = 6.07932628156505E-04  
slopem(1, 3) = 0.310002185699076

' solidity = 1.0  
slopem(7, 4) = -6.94444444474202E-12  
slopem(6, 4) = 1.66666666600625E-09  
slopem(5, 4) = -1.47569444275408E-07  
slopem(4, 4) = 6.10795453948043E-06  
slopem(3, 4) = -1.06196337540609E-04  
slopem(2, 4) = 1.0979166113998E-03  
slopem(1, 4) = 0.249981060934445

' solidity = 1.2  
slopem(7, 5) = -1.2152777719458E-11  
slopem(6, 5) = 2.57612179309884E-09  
slopem(5, 5) = -2.01255341752971E-07  
slopem(4, 5) = 7.28529282589818E-06

slopem(3, 5) = -1.10063251923975E-04

slopem(2, 5) = 1.03774033499349E-03

slopem(1, 5) = 0.210013840616803

' solidity = 1.4

slopem(7, 6) = -6.94444444135388E-12

slopem(6, 6) = 1.53846153871928E-09

slopem(5, 6) = -1.19925213509786E-07

slopem(4, 6) = 4.09965034364745E-06

slopem(3, 6) = -4.48436278688291E-05

slopem(2, 6) = 3.82051237181713E-04

slopem(1, 6) = 0.182514569024661

' solidity = 1.6

slopem(7, 7) = -2.25694444348236E-11

slopem(6, 7) = 4.50721153650614E-09

slopem(5, 7) = -3.28258546761218E-07

slopem(4, 7) = 1.07734192780207E-05

slopem(3, 7) = -1.40615408163569E-04

slopem(2, 7) = 8.60176240280452E-04

slopem(1, 7) = 0.160005099306115

' solidity = 1.8

slopem(7, 8) = 1.73611110991495E-12

slopem(6, 8) = -5.48878204605779E-10

slopem(5, 8) = 6.78418804189729E-08

slopem(4, 8) = -3.58591929172647E-06

slopem(3, 8) = 9.18654094732574E-05

slopem(2, 8) = -3.68509653696947E-04

slopem(1, 8) = 0.142494901151593

' solidity = 2

slopem(7, 9) = -5.20833333567409E-12

slopem(6, 9) = 1.14983974338484E-09

slopem(5, 9) = -9.05448717253288E-08

slopem(4, 9) = 3.42894084548462E-06

slopem(3, 9) = -5.49887086620515E-05

slopem(2, 9) = 7.85977528323656E-04

slopem(1, 9) = 0.1275007286422

k = 9

ReDim curve(k)

```

ReDim Xvar(k)
ReDim Yvar(k)
p = 0.4
For o = 1 To k
    Yvar(o) = CurveFit1(slopem(1, o), slopem(2, o), slopem(3, o),
        slopem(4, o), slopem(5, o), slopem(6, o), slopem(7, o), beta(i,
            j))
    Xvar(o) = p
    p = p + 0.2
Next o
QuadCoeff k
dm(i, j) = Interp(sigma(i, j))
End If
' Maximum thickness correction factor
' Load constants
dkit(6) = 618823.625244141
dkit(5) = -202775.302703857
dkit(4) = 25013.8597869873
dkit(3) = -1269.01561832427
dkit(2) = 41.3428950682282
dkit(1) = 7.56794627627824
dkt(i, j) = CurveFit2(ikit(1), ikit(2), ikit(3), ikit(4), ikit(5), ikit(6), tc(i, j))
d0ref(i, j) = ksh * dkt(i, j) * d010(i, j)
dref(i, j) = d0ref(i, j) + dm(i, j) * camber(i, j)
End Sub

```

## 14. Module mdlInterpolation Code

```

Option Explicit
Option Base 1
Public Ainterp() As Double
Public Binterp() As Double
Public Cinterp() As Double
Dim o As Integer
Public Sub QuadCoeff(k As Integer)
    ReDim Ainterp(k)
    ReDim Binterp(k)
    ReDim Cinterp(k)
    For o = 2 To k - 1

```



```

Ainterp(o) = interpA(Xvar(o + 1), Xvar(o - 1), Xvar(o), Yvar(o), Yvar(o + 1),
                    Yvar(o - 1))
Binterp(o) = interpB(Yvar(o), Yvar(o - 1), Xvar(o), Xvar(o - 1), Ainterp(o))
Cinterp(o) = interpC(Yvar(o), Ainterp(o), Binterp(o), Xvar(o))
Next o
Ainterp(1) = Ainterp(2)
Binterp(1) = Binterp(2)
Cinterp(1) = Cinterp(2)
Ainterp(k) = Ainterp(k - 1)
Binterp(k) = Binterp(k - 1)
Cinterp(k) = Cinterp(k - 1)
For o = 1 To k - 1
    Ainterp(o) = (Ainterp(o) + Ainterp(o + 1)) / 2
    Binterp(o) = (Binterp(o) + Binterp(o + 1)) / 2
    Cinterp(o) = (Cinterp(o) + Cinterp(o + 1)) / 2
Next o
End Sub
Public Function Interp(Xval As Double)
    o = 2
    Do
        If Xval < Xvar(o) Then
            Interp = Ainterp(o) * Xval ^ 2 + Binterp(o) * Xval + Cinterp(o)
            Exit Do
        Else
            If Xval > Xvar(o) And Xval < Xvar(o + 1) Then
                Interp = Ainterp(o) * Xval ^ 2 + Binterp(o) * Xval +
                    Cinterp(o)
                Exit Do
            Else
                o = o + 1
            End If
        End If
    If o = k - 1 Then
        Interp = Ainterp(o) * Xval ^ 2 + Binterp(o) * Xval + Cinterp(o)
        Exit Do
    End If
    Loop Until o = k
End Function

```

## 15. Module mdlFunctions Code

Option Explicit

Option Base 1

Public Function Diffusion(phi1 As Double, beta1 As Double, beta2 As Double, pitch\_ml As Double, solidity As Double) As Double

$$\text{Diffusion} = 1 - \text{phi1} * (\text{Cos}(\text{DegToRad}(\text{beta1})) / \text{Cos}(\text{DegToRad}(\text{beta2}))) +$$
$$(((\text{Tan}(\text{DegToRad}(\text{beta1})) - \text{pitch\_ml} * \text{phi1} * \text{Tan}(\text{DegToRad}(\text{beta2}))) * \text{Cos}(\text{DegToRad}(\text{beta1}))) / ((1 + \text{pitch\_ml}) * \text{solidity}))$$

End Function

Public Function gg1(g As Double) As Double

$$\text{gg1} = g / (g - 1)$$

End Function

Public Function g1(g As Double) As Double

$$g1 = 1 / (g - 1)$$

End Function

Public Function g1g(g As Double) As Double

$$g1g = (g - 1) / g$$

End Function

Public Function Mach(g As Double, X1 As Double) As Double

$$\text{Mach} = \text{Sqr}(((2 / (g - 1)) * (\text{X1} ^ 2)) / (1 - (\text{X1} ^ 2)))$$

End Function

Public Function DegToRad(angle As Double) As Double

$$\text{DegToRad} = \text{angle} * ((22 / 7) / 180)$$

End Function

Public Function RadToDeg(radians As Double) As Double

$$\text{RadToDeg} = \text{radians} * (180 / (22 / 7))$$

End Function

Public Function Arccos(ratio As Double) As Double

$$\text{Arccos} = \text{RadToDeg}(\text{Atn}(-\text{ratio} / \text{Sqr}(-\text{ratio} * \text{ratio} + 1)) + 2 * \text{Atn}(1))$$

End Function

Public Function Arcsin(ratio As Double) As Double

$$\text{Arcsin} = \text{RadToDeg}(\text{Atn}(\text{ratio} / \text{Sqr}(-\text{ratio} * \text{ratio} + 1)))$$

End Function

Public Function DofReaction(Xtheta1 As Double, Xu1 As Double, Xtheta2 As Double, XU2 As Double) As Double

$$\text{DofReaction} = (1 - 0.5 * ((\text{Xtheta1} / \text{Xu1}) + (\text{Xtheta2} / \text{XU2})))$$

End Function

```

Public Function SFTC(beta1 As Double, beta2 As Double, solidity As Double, height As Double,
tipgap As Double, spacing As Double)

Dim CDi As Double
Dim CL As Double
Dim betainf As Double

betainf = Atn((Tan(DegToRad(beta1)) + Tan(DegToRad(beta2))) / 2)
CL = (2 / solidity) * (Tan(DegToRad(beta1)) - Tan(DegToRad(beta2))) *
Cos(DegToRad(betainf))

CDi = (0.25 * (CL ^ 2) * solidity * (tipgap / height) * (1 / Cos(DegToRad(beta2)))) +
(0.04 * (CL ^ 2) * solidity * (spacing / height))

SFTC = CDi * ((Cos(DegToRad(beta1)) ^ 2) / (Cos(DegToRad(betainf)) ^ 3)) * solidity

End Function

Public Function taufunc(XU2 As Double, Xtheta2 As Double, Xu1 As Double, Xtheta1 As
Double) As Double

taufunc = 1 + 2 * ((XU2 * Xtheta2) - (Xu1 * Xtheta1))

End Function

Public Function Xfunc(Xz1 As Double, alpha1 As Double) As Double

Xfunc = Xz1 / Cos(DegToRad(alpha1))

End Function

Public Function Xthetafunc(r1 As Double, r2 As Double, Xtheta1 As Double) As Double

Xthetafunc = (r1 / r2) * Xtheta1

End Function

Public Function Xufunc(r1 As Double, r2 As Double, Xu1 As Double) As Double

Xufunc = (r2 / r1) * Xu1

End Function

Public Function Xwfunc(Xz1 As Double, beta1 As Double) As Double

Xwfunc = Xz1 / Cos(DegToRad(beta1))

End Function

Public Function Yfunc(X1 As Double, tau1 As Double) As Double

Yfunc = X1 / Sqr(tau1)

End Function

Public Function Machz(M1 As Double, alpha1 As Double) As Double

Machz = M1 * Cos(DegToRad(alpha1))

End Function

Public Function alphafunc(Xtheta1 As Double, Xz1 As Double) As Double

alphafunc = RadToDeg(Atn(Xtheta1 / Xz1))

End Function

Public Function betafunc(Xu1 As Double, Xtheta1 As Double, Xz1 As Double) As Double

```

```

        betafunc = RadToDeg(Atn((Xu1 - Xtheta1) / Xz1))
End Function

Public Function rhfunc1(rt As Double, A1 As Double) As Double
    rhfunc1 = Sqr(rt ^ 2 - (A1 / (22 / 7)))
End Function

Public Function rhfunc2(rm As Double, rt As Double) As Double
    rhfunc2 = 2 * rm - rt
End Function

Public Function rtfunc(A1 As Double, rm As Double) As Double
    rtfunc = (A1 / (4 * rm * (22 / 7))) + rm
End Function

Public Function rmfunc(rt As Double, rh As Double) As Double
    rmfunc = (rt + rh) / 2
End Function

Public Function rhtfunc(rt As Double, rh As Double) As Double
    rhtfunc = rh / rt
End Function

Public Function rhtfunc2(h As Double, rm As Double) As Double
    Dim hrm As Double
    hrm = h / (2 * rm)
    rhtfunc2 = (1 - hrm) / (1 + hrm)
End Function

Public Function CurveFit1(const0 As Double, const1 As Double, const2 As Double, const3 As
    Double, const4 As Double, const5 As Double, const6 As Double, polyvar As Double)
    ' No y intercept
    CurveFit1 = (const6 * (polyvar ^ 6)) + (const5 * (polyvar ^ 5)) + (const4 * (polyvar ^ 4))
        + (const3 * (polyvar ^ 3)) + (const2 * (polyvar ^ 2)) + (const1 * polyvar) +
        const0
End Function

Public Function CurveFit2(const1 As Double, const2 As Double, const3 As Double, const4 As
    Double, const5 As Double, const6 As Double, polyvar As Double)
    ' y intercept
    CurveFit2 = (const6 * (polyvar ^ 6)) + (const5 * (polyvar ^ 5)) + (const4 * (polyvar ^ 4))
        + (const3 * (polyvar ^ 3)) + (const2 * (polyvar ^ 2)) + (const1 * polyvar)
End Function

Public Function camberfunc(beta2 As Double, beta1 As Double, kshape As Single, kthick As
    Double, idelta As Double, slope As Double)
    camberfunc = ((beta2 - beta1) - (kshape * kthick * idelta)) / slope
End Function

```

```
Public Function interpA(Xip1 As Double, Xim1 As Double, Xi As Double, Yi As Double, Yip1
As Double, Yim1 As Double)
```

```
    interpA = (1 / (Xip1 - Xim1)) * (((Yip1 - Yi) / (Xip1 - Xi)) - ((Yi - Yim1) / (Xi - Xim1)))
```

```
End Function
```

```
Public Function interpB(Yi As Double, Yim1 As Double, Xi As Double, Xim1 As Double, Ai As
Double)
```

```
    interpB = ((Yi - Yim1) / (Xi - Xim1)) - Ai * (Xi + Xim1)
```

```
End Function
```

```
Public Function interpC(Yi As Double, Ai As Double, Bi As Double, Xi As Double)
```

```
    interpC = Yi - Ai * Xi ^ 2 - Bi * Xi
```

```
End Function
```

```
Public Function ShockLoss(M As Double, g As Double)
```

```
    Dim ystar As Double
```

```
    ystar = (1 / (4 * g * M ^ 2)) * (((g + 1) * M ^ 2) - (3 - g) + Sqr((g + 1) * ((g + 1) * M ^ 4)
- (2 * (3 - g) * M ^ 2) + g + 9)))
```

```
    ShockLoss = ((g + 1) / (2 * g * M ^ 2 * ystar - (g - 1))) ^ g1(g) * (((g + 1) * M ^ 2 *
ystar) / (2 + (g - 1) * M ^ 2 * ystar)) ^ gg1(g)
```

```
End Function
```

```
Public Function DiffB(sigma As Double, R As Double)
```

```
    DiffB = 2 * sigma * R * (1 + R)
```

```
End Function
```

```
Public Function DiffA(sigma As Double, R As Double, D As Double, phi As Double, beta1 As
Double)
```

```
    DiffA = (1 + R) * sigma * ((1 - D) / (phi * Cos(DegToRad(beta1)))) +
(Tan(DegToRad(beta1)) / phi)
```

```
End Function
```

```
Public Function SinB2(A As Double, B As Double, R As Double)
```

```
    SinB2 = (-B + Sqr(B ^ 2 + (4 * (A ^ 2 - (B ^ 2 / (4 * R ^ 2))) * (R ^ 2 + A ^ 2)))) / (2 * (R
^ 2 + A ^ 2))
```

```
End Function
```

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## APPENDIX C. CALCULATION RESULTS

### C1. HAND CALCULATIONS

Inputs derived from Sanger [Ref. 13].

$$\dot{m} = 17.091 \text{ lbm/sec}$$

$$P_{t1} = 14.69 \text{ psia}$$

$$T_{t1} = 517.8^\circ \text{ R}$$

$$M_{w1t} = 1.28$$

$$\omega = 2836.33 \text{ rad/sec}$$

$$R = 53.35 \text{ ft} \cdot \text{ lbf} / \text{ lbm} \cdot ^\circ \text{ R}$$

$$\gamma = 1.4$$

$$\alpha_{t1} = 0^\circ$$

$$U_{t1} = \omega \cdot r_t = 2836.33 \cdot (5.5 \text{ inches} / 12 \text{ inches per ft}) = 1300 \text{ ft/sec}$$

$$X_{U_{t1}} = \frac{U_{t1}}{\sqrt{2 \cdot C_p \cdot g \cdot T_{t1}}} \text{ where } C_p = \left( \frac{\gamma}{\gamma-1} \right) \cdot R = \left( \frac{1.4}{1.4-1} \right) \cdot 53.35 = 186.725$$

$$\therefore X_{U_{t1}} = \frac{1300}{\sqrt{2 \cdot 186.725 \cdot 32.2 \cdot 517.8}} = 0.5210$$

$$\sin^2 \beta_{t1} = \left( \frac{X_{U_{t1}}^2}{1 + X_{U_{t1}}^2} \right) \cdot \left( \frac{1 + \frac{\gamma-1}{2} \cdot M_{w1t}^2}{\frac{\gamma-1}{2} \cdot M_{w1t}^2} \right) = \left( \frac{0.5210^2}{1 + 0.5210^2} \right) \cdot \left( \frac{1 + \frac{1.4-1}{2} \cdot 1.28^2}{\frac{1.4-1}{2} \cdot 1.28^2} \right)$$

$$\sin^2 \beta_{t1} = 0.8649$$

$$\sin \beta_{t1} = 0.9300 \Rightarrow \beta_{t1} = \sin^{-1}(0.9300) = 68.438^\circ$$

$$M_{z1t} = M_{w1t} \cdot \cos \beta_{t1} = 1.28 \cdot \cos(68.438^\circ) = 0.4704$$

$$D_{2m} = 0.455; R_{21} = 1.0687; \phi_{21} = 0.956$$

$$\sigma_{2m} = 1.52; f_{\sigma_2}(\sigma_{2t} / \sigma_{2m}) = 0.8553$$

$$\delta_2 = 0.0045; AR_2 = 1.2$$

$$(t/c)_{2\text{max}} = 0.037 \text{ at tip; } 0.056 \text{ at mean; } 0.08 \text{ at hub}$$

$$D_{3m} = 0.52; R_{32} = 1.0259; \phi_{32} = 1.0371$$

$$\sigma_{3m} = 1.25; f_{\sigma_3}(\sigma_{3t} / \sigma_{3m}) = 0.8$$

$$\delta_3 = 0.003; AR_3 = 1.2$$

$$(t/c)_{3\text{max}} = 0.07 \text{ at tip; } 0.06 \text{ at mean; } 0.05 \text{ at hub}$$

Applying equations from Appendix A yields the followings results.

## 1. Inlet Conditions

$$M_{1t} = \frac{0.4704}{\cos 0} = 0.4704$$

$$X_{1t} = \sqrt{\frac{\frac{1.4-1}{2} \cdot 0.4704^2}{1 + \frac{1.4-1}{2} \cdot 0.4704^2}} = 0.2059$$

$$X_{z1t} = (0.2059) \cdot \cos 0 = 0.2059$$

$$X_{\theta 1t} = (0.2059) \cdot \tan 0 = 0$$

$$X_{u1t} = 0 + (0.2059) \cdot \tan(68.438) = 0.5210$$

$$\rho_{t1} = \frac{14.69}{53.35 \cdot 517.8} \cdot 144 = 0.07658 \text{ lbm/ft}^3$$

$$V_{t1} = \sqrt{2 \cdot 32.2 \cdot 186.725 \cdot 517.8} = 2495.3139 \text{ ft/sec}$$

$$\Phi_{1t} = 0.2059 \cdot (1 - 0.2059^2)^{\frac{1}{1.41}} = 0.1847$$

$$A_1 = \left( \frac{17.09}{0.07658 \cdot 2495.3139} \right) \cdot \frac{1}{0.1847 \cdot \cos 0} = 0.4841 \text{ ft}^2 \text{ or } 69.7144 \text{ in}^2$$

$$r_{1t} = \frac{0.5210 \cdot 2495.3139}{2836.33} = 0.4583 \text{ ft or } 5.5 \text{ in}$$

$$r_{1h} = \sqrt{5.5^2 - 69.7144 / \pi} = 2.8389 \text{ in or } 0.2366 \text{ ft}$$

$$r_{1ht} = 2.8389 / 5.5 = 0.5162$$

$$r_{1m} = \frac{5.5 + 2.8389}{2} = 4.1695 \text{ in or } 0.3475 \text{ ft}$$

$$X_{\theta 1m} = \frac{5.5}{4.1695} \cdot 0 = 0$$

$$X_{z1m} = X_{z1t} = 0.2058$$

$$\alpha_{1m} = \tan^{-1} \left( \frac{5.5}{4.1695} \cdot \tan 0 \right) = 0$$

$$X_{u1m} = \frac{4.1695}{5.5} \cdot 0.5210 = 0.3949$$

$$\beta_{1m} = \tan^{-1} \left( \frac{0.3949 - 0}{0.2058} \right) = 62.4685^\circ$$

$$X_{1m} = \frac{0.2058}{\cos 0} = 0.2058$$



$$M_{1m} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.2058^2}{1-0.2058^2}} = 0.4704$$

$$X_{w1m} = \frac{0.2058}{\cos 62.4685} = 0.4454$$

$$M_{w1m} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.4454^2}{1-0.4454^2}} = 1.1123$$

## 2. Rotor Conditions at Mean Line

$$0.455 = 1 - (0.956) \cdot \frac{\cos 62.4685}{\cos \beta_{2m}} + \frac{\tan 62.4685 - 1.0687 \cdot 0.956 \cdot \tan \beta_{2m}}{(1+1.0687) \cdot 1.52} \cdot \cos 62.4685$$

Solve for  $\beta_{2m}$

$$\sin \beta_{2m} = \frac{-B + \sqrt{B^2 + 4(R_{21}^2 + A^2) \cdot \left[ A^2 - \frac{B^2}{4 \cdot R_{21}^2} \right]}}{2 \cdot (R_{21}^2 + A^2)}$$

$$\text{Where } A = \left( (1 + R_{21}) \cdot \sigma_{2m} \cdot \left[ \frac{1 - D_{2m}}{\phi_{21} \cdot \cos \beta_{1m}} \right] + \frac{\tan \beta_{1m}}{\phi_{21}} \right)$$

$$A = \left( (1 + 1.0687) \cdot 1.52 \cdot \left[ \frac{1 - 0.455}{0.956 \cdot \cos 62.4685} \right] + \frac{\tan 62.4685}{0.956} \right) = 5.8848$$

$$\text{and } B = 2 \cdot \sigma_{2m} \cdot R_{21} \cdot (1 + R_{21}) = 2 \cdot 1.52 \cdot 1.0687 \cdot (1 + 1.0687) = 6.7209$$

$$\therefore \sin \beta_{2m} = \frac{-6.7209 + \sqrt{6.7209^2 + 4(1.0687^2 + 5.8848^2) \cdot \left[ 5.8848^2 - \frac{6.7209^2}{4 \cdot 1.0687^2} \right]}}{2 \cdot (1.0687^2 + 5.8848^2)}$$

$$\sin \beta_{2m} = 0.7430$$

$$\beta_{2m} = 47.9895^\circ$$

$$X_{u2m} = 1.0687 \cdot 0.3949 = 0.4221$$

$$\phi_{1m} = \frac{0.2059}{0.3949} = 0.5213$$

$$\phi_{2m} = 0.956 \cdot 0.5213 \cdot \left( \frac{1}{1.0687} \right) = 0.4663$$

$$X_{z2m} = 0.4663 \cdot 0.4213 = 0.1968$$

$$X_{\theta 2m} = 0.4221 - 0.1968 \tan 47.9895 = 0.2036$$

$$\alpha_{2m} = \tan^{-1}\left(\frac{0.2036}{0.1968}\right) = 45.9677^\circ$$

$$r_{st_m} = \left[1 - \frac{1}{2}\left(\frac{0.0}{0.3949} + \frac{0.2036}{0.4221}\right)\right] = 0.7588$$

$$\tau = 1 + 2 \cdot [0.4221 \cdot 0.2036 - 0.3949 \cdot 0.0] = 1.1718$$

$$X_{2m} = \frac{0.1968}{\cos(45.9677)} = 0.2832$$

$$X_{w2m} = \frac{0.1968}{\cos(47.9894)} = 0.2941$$

$$Y_{2m} = \frac{0.2832}{\sqrt{1.1718}} = 0.2616$$

$$Y_{w2m} = \frac{0.2941}{\sqrt{1.1718}} = 0.2717$$

$$M_{2m} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.2616^2}{1-0.2616^2}} = 0.6060$$

$$M_{w2m} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.2717^2}{1-0.2717^2}} = 0.6312$$

### 3. Stator Conditions at Mean Line

$$\alpha_{3m} = 1 \cdot 0 = 0^\circ$$

$$D_{3m} = 1 - 1.0371 \cdot \frac{\cos 45.9677}{\cos 0} + \frac{(\tan 45.9677 - 1.0259 \cdot 1.0371 \cdot \tan 0) \cdot \cos 45.9677}{(1 + 1.0259) \cdot 1.25} = 0.5631$$

$$X_{z3m} = 1.0371 \cdot 0.1968 = 0.2041$$

$$X_{\theta 3m} = 0.2041 \cdot \tan 0 = 0$$

$$X_{U3m} = 0.4221 \cdot 1.0259 = 0.4330$$

$$\beta_{3m} = \tan^{-1}\left(\frac{0.4330 - 0}{0.2041}\right) = 64.7615^\circ$$

$$X_{3m} = \frac{0.2041}{\cos 0} = 0.2041$$

$$X_{w3m} = \frac{0.2041}{\cos 64.7615} = 0.4787$$

$$Y_{3m} = \frac{0.2041}{\sqrt{1.1718}} = 0.1886$$

$$Y_{w3m} = \frac{0.4787}{\sqrt{1.1718}} = 0.4422$$

$$M_{3m} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.1885^2}{1-0.1885^2}} = 0.4293$$

$$M_{w3m} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.4422^2}{1-0.4422^2}} = 1.1025$$

#### 4. Iteration #1

##### *Rotor Performance*

Initially set  $\tilde{\omega}_{s_2}$  and  $\tilde{\omega}_{s_{FTC_2}} = 0$

$$\tilde{\omega}_{P_2} = 2 \cdot 1.52 \cdot \frac{\cos^2 62.4685}{\cos^3 47.9894} \cdot [0.005 + 0.16 \cdot 0.455^4] = 0.02569$$

$$\tilde{\omega}_{T_2} = 0 + 0 + 0.02569$$

$$T_1 / T_{u1} = 1 - 0.2059^2 = 0.9576$$

$$P_1 / P_{u1} = (0.9576)^{3.5} = 0.8594$$

$$T_{R1} / T_{u1} = 0.9576 + 0.4454^2 = 1.1560$$

$$P_{R1} / P_{u1} = (1.1560)^{3.5} = 1.6608$$

$$T_{E1} / T_{u1} = 1.1560 + 0.4221^2 - 0.3949^2 = 1.1781$$

$$T_{E2} / T_{u1} = 1.1781$$

$$P_{E1} / P_{u1} = (1.1781)^{3.5} = 1.7750$$

$$P_{E2} / P_{u1} = 1.7750 - 0.02569 \cdot [1.6608 - 0.8594] = 1.7544$$

$$P_{I2} / P_{u1} = 1.7544 \cdot \left[ \frac{1.1718}{1.1781} \right]^{3.5} = 1.7218$$

$$T_2 / T_{u1} = 1.1718 - 0.2832^2 = 1.0917$$

$$P_2 / P_{u1} = 1.7218 \cdot \left( \frac{1.0917}{1.1718} \right)^{3.5} = 1.3435$$

$$\Phi_{2m} = 0.2616 \cdot (1 - 0.2616^2)^{2.5} = 0.2191$$

$$A_2/A_1 = \frac{0.1847 \cdot \cos 0}{0.2191 \cdot \cos 45.9677} \cdot \frac{\sqrt{1.1718}}{1.7218} = 0.7627$$

$$A_2 = 0.7627 \cdot 69.7144 = 53.1725 \text{ in}^2 \text{ or } 0.3693 \text{ ft}^2$$

$$r_{2m} = 4.1694 \cdot 1.0687 = 4.4559 \text{ in or } 0.3713 \text{ ft}$$

$$H_2 = \frac{53.1725}{2 \cdot \pi \cdot 4.4559} = 1.8992 \text{ in or } 0.1583 \text{ ft}$$

$$r_{ht2} = \frac{1 - \frac{1.8992}{2 \cdot 4.4559}}{1 + \frac{1.8992}{2 \cdot 4.4559}} = 0.6487$$

$$r_{2t} = \left( \frac{2}{1 + 0.6487} \right) \cdot 4.4559 = 5.4055 \text{ in or } 0.4505 \text{ ft}$$

$$r_{2h} = 0.6487 \cdot 5.4055 = 3.5063 \text{ in or } 0.2922 \text{ ft}$$

### ***Stator Performance***

Initially set  $\tilde{\omega}_s$  and  $\tilde{\omega}_{\text{SFTC}_3} = 0$

$$\tilde{\omega}_p = 24.25 \cdot \frac{\cos^2 45.9677}{\cos^3 0} \cdot [0.005 + 0.16 \cdot 0.5631^4] = 0.02546$$

$$\tilde{\omega}_r = 0 + 0 + 0.02546$$

$$P_{i3}/P_{ti} = 1.7218 - 0.02546 \cdot (1.7218 - 1.3435) = 1.7121$$

$$T_{i3}/T_{ti} = \tau = 1.1718$$

$$T_3/T_{ti} = 1.1718 - 0.2041^2 = 1.1302$$

$$P_3/P_{ti} = \left( \frac{1.1302}{1.1718} \right)^{3.5} = 1.5084$$

$$\Phi_{3m} = 0.1886 \cdot (1 - 0.1886^2)^{2.5} = 0.1722$$

$$A_3/A_1 = \frac{0.1847 \cdot \cos 0}{0.1722 \cdot \cos 0} \cdot \frac{\sqrt{1.1718}}{1.7121} = 0.6782$$

$$A_3 = 0.6782 \cdot 69.7144 = 47.2778 \text{ in}^2 \text{ or } 0.3233 \text{ ft}^2$$

$$r_{3m} = 1.0259 \cdot 4.4559 = 4.5713 \text{ in or } 0.3809 \text{ ft}$$

$$H_3 = \frac{47.2778}{2 \cdot \pi \cdot 4.5713} = 1.6460 \text{ in or } 0.1372 \text{ ft}$$

$$r_{ht3} = \frac{1 - \frac{1.6460}{2 \cdot 4.5713}}{1 + \frac{1.6460}{2 \cdot 4.5713}} = 0.6949$$

$$r_{3t} = \left( \frac{2}{1 + 0.6949} \right) \cdot 4.5713 = 5.3943 \text{ in or } 0.4495 \text{ ft}$$

$$r_{3h} = 0.6949 \cdot 5.3943 = 3.7483 \text{ in or } 0.3124 \text{ ft}$$

### ***Rotor Hub Calculations***

$$X_{\theta 2h} = 0.2036 \frac{4.4559}{3.5063} = 0.2587$$

$$X_{U 2h} = 0.4221 \frac{3.5063}{4.4559} = 0.3321$$

$$\alpha_{2h} = \tan^{-1} \left( \frac{0.2587}{0.1968} \right) = 52.7381^\circ$$

$$\beta_{2h} = \tan^{-1} \left( \frac{0.3321 - 0.2587}{0.1968} \right) = 20.4569^\circ$$

$$X_{2h} = \frac{0.1968}{\cos 52.7381} = 0.3251$$

$$X_{w 2h} = \frac{0.1968}{\cos 20.4569} = 0.2101$$

$$Y_{2h} = \frac{0.3251}{\sqrt{1.1718}} = 0.3003$$

$$Y_{w 2h} = \frac{0.2101}{\sqrt{1.1718}} = 0.1940$$

$$M_{2h} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.3003^2}{1 - 0.3003^2}} = 0.7039$$

$$M_{w 2h} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.1940^2}{1 - 0.1940^2}} = 0.4423$$

### ***Rotor Tip Calculations***

$$X_{\theta 2t} = 0.2036 \cdot \frac{4.4559}{5.4055} = 0.1678$$

$$X_{U 2t} = 0.4221 \cdot \frac{5.4055}{4.4559} = 0.5120$$

$$\alpha_{2t} = \tan^{-1}\left(\frac{0.1678}{0.1968}\right) = 40.4526^\circ$$

$$\beta_{2t} = \tan^{-1}\left(\frac{0.5120 - 0.1678}{0.1968}\right) = 60.2402^\circ$$

$$X_{2t} = \frac{0.1968}{\cos 40.4526} = 0.2586$$

$$X_{w2t} = \frac{0.1968}{\cos 60.2402} = 0.3965$$

$$Y_{2t} = \frac{0.2586}{\sqrt{1.1718}} = 0.2389$$

$$Y_{w2t} = \frac{0.3965}{\sqrt{1.1718}} = 0.3663$$

$$M_{2t} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.2389^2}{1-0.2389^2}} = 0.5502$$

$$M_{w2t} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.3663^2}{1-0.3663^2}} = 0.8802$$

### ***Stator Hub Calculations***

$$X_{03h} = 0.0 \cdot \frac{4.5713}{3.7483} = 0.0$$

$$X_{U3h} = 0.4330 \cdot \frac{3.7483}{4.5713} = 0.3550$$

$$\alpha_{3h} = \tan^{-1}\left(\frac{0.0}{0.2041}\right) = 0.0^\circ$$

$$\beta_{3h} = \tan^{-1}\left(\frac{0.3550 - 0.0}{0.2041}\right) = 60.1058^\circ$$

$$X_{3h} = \frac{0.2041}{\cos 0} = 0.2041$$

$$X_{w3h} = \frac{0.2041}{\cos 60.1058} = 0.4095$$

$$Y_{3h} = \frac{0.2041}{\sqrt{1.1718}} = 0.1886$$

$$Y_{w3h} = \frac{0.4095}{\sqrt{1.1718}} = 0.3783$$

$$M_{3h} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.1886^2}{1-0.1886^2}} = 0.4293$$

$$M_{w3h} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.3783^2}{1-0.3783^2}} = 0.9139$$

### ***Stator Tip Calculations***

$$X_{\theta 3t} = 0.0 \cdot \frac{4.5713}{5.3943} = 0.0$$

$$X_{U 3t} = 0.4330 \cdot \frac{5.3943}{4.5713} = 0.5110$$

$$\alpha_{3t} = \tan^{-1}\left(\frac{0.0}{0.2041}\right) = 0.0^\circ$$

$$\beta_{3t} = \tan^{-1}\left(\frac{0.5110 - 0.0}{0.2041}\right) = 68.2250^\circ$$

$$X_{3t} = \frac{0.2041}{\cos 0} = 0.2041$$

$$X_{w 3t} = \frac{0.2041}{\cos 68.2250} = 0.5502$$

$$Y_{3t} = \frac{0.2041}{\sqrt{1.1718}} = 0.1886$$

$$Y_{w 3t} = \frac{0.5502}{\sqrt{1.1718}} = 0.5083$$

$$M_{3t} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.1886^2}{1-0.1886^2}} = 0.4293$$

$$M_{w 3t} = \sqrt{\frac{\frac{2}{1.4-1} \cdot 0.5083^2}{1-0.5083^2}} = 1.3197$$

### ***Rotor Blade Geometry***

$$H_2 = 5.4055 - 3.5063 = 1.8992 \text{ in}$$

$$C_2' = \frac{1.8992}{1.2} = 1.5827 \text{ in}$$

$$Z_2' = \frac{2 \cdot \pi \cdot 4.559}{1.5827} \cdot 1.52 = 26.8884 \text{ blades}$$

Choose  $Z_2$  to match transonic compressor rotor. Therefore,  $Z_2 = 22$ .

$$AR_{Rev2} = \frac{1.8992}{\frac{2 \cdot \pi \cdot 4.559 \cdot 1.52}{22}} = 0.9818$$

$$C_{Rev2} = \frac{1.8992}{0.9818} = 1.9343 \text{ in}$$

$$S_2 = \frac{1.9343}{1.52} = 1.2726 \text{ in}$$

### ***Stator Blade Geometry***

$$H_3 = 5.3943 - 3.7483 = 1.6460 \text{ in}$$

$$C'_3 = \frac{1.6460}{1.2} = 1.3717 \text{ in}$$

$$Z_3 = \frac{2 \cdot \pi \cdot 4.5713}{1.3717} \cdot 1.25 = 26.1740 \text{ blades}$$

Choose  $Z_3$  to match transonic compressor rotor. Therefore,  $Z_3 = 27$ .

$$AR_{Rev3} = \frac{1.6460}{\frac{2 \cdot \pi \cdot 4.5713 \cdot 1.25}{27}} = 1.2379$$

$$C_{Rev3} = \frac{1.6460}{1.2379} = 1.3297 \text{ in}$$

$$S_3 = \frac{1.3297}{1.25} = 1.0638 \text{ in}$$

The design calculations have to iterated until the losses converge to a chosen criteria. A criterion of 0.0001 was chosen for both the hand and computer calculations.

## **5. Iteration #2**

Only the results will be shown for all subsequent iterations.

<b>ROTOR</b>		<b>STATOR</b>	
$\beta_\infty$	56.560435987322300	$\beta_\infty$	27.347157421794000
$C_L$	0.586010932091710	$C_L$	1.470018487969480
$C_{Di}$	0.014452454402386	$C_{Di}$	0.071059015271782
$\omega_{SFTC2}$	0.028049370920909	$\omega_{SFTC3}$	0.061233413235418
$y^*$	0.908770674133602	$y^*$	1.978417070245130
$P_{te}/P_{ti}$	0.999746596870648	$P_{te}/P_{ti}$	1.005788072708940
$\omega_{S2}$	0.000470350655165	$\omega_{S3}$	-0.026347850522881
$\omega_{P2}$	0.025691775310535	$\omega_{P3}$	0.025461335476916
$\omega_{T2}$	0.054211496886609	$\omega_{T3}$	0.086694748712334
$T_1/T_{t1}$	0.957618541339988	$P_{t3}/P_{t1}$	1.666977507638590
$P_1/P_{t1}$	0.859357579736388	$T_{t3}/T_{t1}$	1.171843486972510
$T_{R1}/T_{t1}$	1.15597584087194	$T_3/T_{t1}$	1.130182173979650



$P_{R1}/P_{t1}$	1.660812680211420	$P_3/P_{t1}$	1.468607319851730
$T_{E1}/T_{t1}$	1.178143079024150	$\Phi_{3m}$	0.172237922031280
$P_{E1}/P_{t1}$	1.774978623835910	$A_3/A_1$	0.696539265527826
$P_{E2}/P_{t1}$	1.731530543151750	$A_3$ (in)	48.558787505362500
$P_{t2}/P_{t1}$	1.699341511605150	$r_{3m}$ (in)	4.571286972682070
$T_2/T_{t1}$	1.091667880043820	$h_3$ (in)	1.690633536728720
$P_2/P_{t1}$	1.326031657810530	$r_{ht3}$	0.687879413456575
$\Phi_{2m}$	0.219098107941022	$r_{3t}$ (in)	5.416603741046430
$A_2/A_1$	0.772787543503894	$r_{3h}$ (in)	3.725970204317710
$A_2$ (in)	53.874387229785800		
$r_{2m}$ (in)	4.455879688743610		
$h_2$ (in)	1.924283336313540		
$r_{ht2}$	0.644836516957841		
$r_{2t}$ (in)	5.418021356900380		
$r_{2h}$ (in)	3.493738020586840		

Table C1. Stage Performance Results (Iteration #2)

HUB		TIP	
$X_{\theta 2h}$	0.259634095360950	$X_{\theta 2t}$	0.167421545736055
$X_{U 2h}$	0.330933976012678	$X_{U 2t}$	0.513206010065825
$\alpha_{2h}$	52.836925539652200	$\alpha_{2t}$	40.387101220022500
$\beta_{2h}$	19.914379724264200	$\beta_{2t}$	60.352859069903200
$X_{2h}$	0.325797182731520	$X_{2t}$	0.258387141279412
$X_{W 2h}$	0.209326572089755	$X_{W 2t}$	0.397870376597357
$Y_{2h}$	0.300962592479341	$Y_{2t}$	0.238691026272198
$Y_{W 2h}$	0.193370204379153	$Y_{W 2t}$	0.367541852288360
$M_{2h}$	0.705691535783612	$M_{2t}$	0.549615692085776
$M_{W 2h}$	0.440706882771685	$M_{W 2t}$	0.883701501259568
$M_{Z 2h}$	0.426298128621960	$M_{Z 2t}$	0.418633587082212

Table C2. Rotor Results (Iteration #2)

HUB		TIP	
$X_{\theta 3h}$	0.000000000000000	$X_{\theta 3t}$	0.000000000000000
$X_{U 3h}$	0.352931481111029	$X_{U 3t}$	0.513071730606907
$\alpha_{3h}$	0.000000000000000	$\alpha_{3t}$	0.000000000000000
$\beta_{3h}$	59.957896644744600	$\beta_{3t}$	68.306267419874700
$X_{3h}$	0.204111031041579	$X_{3t}$	0.204111031041579
$X_{W 3h}$	0.407703254036660	$X_{W 3t}$	0.552181051595238
$Y_{3h}$	0.188552229153336	$Y_{3t}$	0.188552229153336
$Y_{W 3h}$	0.376625197518214	$Y_{W 3t}$	0.510089864537044

M <sub>3h</sub>	0.429316175796641	M <sub>3t</sub>	0.429316175796641
M <sub>W3h</sub>	0.909100497709792	M <sub>W3t</sub>	1.326087214551410
M <sub>Z3h</sub>	0.429316175796641	M <sub>Z3t</sub>	0.429316175796641

Table C3. Stator Results (Iteration #2)

ROTOR		STATOR	
H <sub>2</sub>	1.924283336313540	H <sub>3</sub>	1.690633536728720
C <sub>2</sub> '	1.603569446927950	C <sub>3</sub> '	1.408861280607270
Z <sub>2</sub> '	26.538058032755800	Z <sub>3</sub> '	25.483562094627500
Z <sub>2</sub>	22.000000000000000	Z <sub>3</sub>	27.000000000000000
AR'	0.994797734160298	AR'	1.271407814954980
C <sub>2</sub>	1.934346320096740	C <sub>3</sub>	1.329733478780440
S <sub>2</sub>	1.272596263221540	S <sub>3</sub>	1.063786783024350

Table C4. Blade Geometry Results (Iteration #2)

Compare  $\tilde{\omega}_T$  (iteration #2) and  $\tilde{\omega}_T$  (iteration #1).

$$|\tilde{\omega}_{T2_{\text{iteration2}}} - \tilde{\omega}_{T2_{\text{iteration1}}}| = 0.05421 - 0.02569 = 0.02852$$

$$|\tilde{\omega}_{T3_{\text{iteration2}}} - \tilde{\omega}_{T3_{\text{iteration1}}}| = 0.08669 - 0.02546 = 0.06123$$

## 6. Iteration #3

ROTOR		STATOR	
$\beta_\infty$	56.560435987322300	$\beta_\infty$	27.347157421794000
C <sub>L</sub>	0.586010932091710	C <sub>L</sub>	1.470018487969480
C <sub>Di</sub>	0.014264158667470	C <sub>Di</sub>	0.069184495778439
$\omega_{SFTC2}$	0.027683925940807	$\omega_{SFTC3}$	0.059618090727575
y*	0.908770674133602	y*	1.978417070245130
P <sub>te</sub> /P <sub>ti</sub>	0.999746596870648	P <sub>te</sub> /P <sub>ti</sub>	1.005788072708940
$\omega_{S2}$	0.000470350655165	$\omega_{S3}$	-0.026347850522881
$\omega_{P2}$	0.025691775310535	$\omega_{P3}$	0.025461335476916
$\omega_{T2}$	0.053846051906507	$\omega_{T3}$	0.085079426204491
T <sub>1</sub> /T <sub>t1</sub>	0.957618541339988	P <sub>t3</sub> /P <sub>t1</sub>	1.667862594069170
P <sub>1</sub> /P <sub>t1</sub>	0.859357579736388	T <sub>t3</sub> /T <sub>t1</sub>	1.171843486972510
T <sub>R1</sub> /T <sub>t1</sub>	1.15597584087194	T <sub>3</sub> /T <sub>t1</sub>	1.130182173979650
P <sub>R1</sub> /P <sub>t1</sub>	1.660812680211420	P <sub>3</sub> /P <sub>t1</sub>	1.469387081069080
T <sub>E1</sub> /T <sub>t1</sub>	1.178143079024150	$\Phi_{3m}$	0.172237922031280
P <sub>E1</sub> /P <sub>t1</sub>	1.774978623835910	A <sub>3</sub> /A <sub>1</sub>	0.696169632289165
P <sub>E2</sub> /P <sub>t1</sub>	1.731823430894990	A <sub>3</sub> (in)	48.533018761546700
P <sub>t2</sub> /P <sub>t1</sub>	1.699628954585760	r <sub>3m</sub> (in)	4.571286972682070
T <sub>2</sub> /T <sub>t1</sub>	1.091667880043820	h <sub>3</sub> (in)	1.689736366417590
P <sub>2</sub> /P <sub>t1</sub>	1.326255955569100	r <sub>ht3</sub>	0.688019209608545
$\Phi_{2m}$	0.219098107941022	r <sub>3t</sub> (in)	5.416155155890860
A <sub>2</sub> /A <sub>1</sub>	0.772656848887118	r <sub>3h</sub> (in)	3.726418789473280

$A_2$ (in)	53.865275938523100		
$r_{2m}$ (in)	4.455879688743610		
$h_2$ (in)	1.923957899554990		
$r_{ht2}$	0.644885917495964		
$r_{2t}$ (in)	5.417858638521100		
$r_{2h}$ (in)	3.493900738966110		

Table C5. Stage Performance Results (Iteration #3)

HUB		TIP	
$X_{\theta 2h}$	0.259622003649605	$X_{\theta 2t}$	0.167426574025716
$X_{U 2h}$	0.330949389028739	$X_{U 2t}$	0.513190597049764
$\alpha_{2h}$	52.835640920353900	$\alpha_{2t}$	40.387950481631600
$\beta_{2h}$	19.921457676992400	$\beta_{2t}$	60.351402895843300
$X_{2h}$	0.325787546694057	$X_{2t}$	0.258390399380250
$X_{W 2h}$	0.209335942224263	$X_{W 2t}$	0.397852611427487
$Y_{2h}$	0.300953690969537	$Y_{2t}$	0.238694036017300
$Y_{W 2h}$	0.193378860255026	$Y_{W 2t}$	0.367525441306733
$M_{2h}$	0.705668584925989	$M_{2t}$	0.549623041103662
$M_{W 2h}$	0.440727376594600	$M_{W 2t}$	0.883655881142935
$M_{Z 2h}$	0.426296872834759	$M_{Z 2t}$	0.418633906000314

Table C6. Rotor Results (Iteration #3)

HUB		TIP	
$X_{\theta 3h}$	0.000000000000000	$X_{\theta 3t}$	0.000000000000000
$X_{U 3h}$	0.352973972009957	$X_{U 3t}$	0.513029239707979
$\alpha_{3h}$	0.000000000000000	$\alpha_{3t}$	0.000000000000000
$\beta_{3h}$	59.960885862080200	$\beta_{3t}$	68.304637549438200
$X_{3h}$	0.204111031041579	$X_{3t}$	0.204111031041579
$X_{W 3h}$	0.407740037167485	$X_{W 3t}$	0.552141570422119
$Y_{3h}$	0.188552229153336	$Y_{3t}$	0.188552229153336
$Y_{W 3h}$	0.376659176775861	$Y_{W 3t}$	0.510053392901174
$M_{3h}$	0.429316175796641	$M_{3t}$	0.429316175796641
$M_{W 3h}$	0.909196076420228	$M_{W 3t}$	1.325959056752780
$M_{Z 3h}$	0.429316175796641	$M_{Z 3t}$	0.429316175796641

Table C7. Stator Results (Iteration #3)

ROTOR		STATOR	
$H_2$	1.923957899554990	$H_3$	1.689736366417590
$C_2'$	1.603298249629160	$C_3'$	1.408113638681320

Z <sub>2</sub> '	26.542546935338600	Z <sub>3</sub> '	25.497092664122100
Z <sub>2</sub>	22.000000000000000	Z <sub>3</sub>	27.000000000000000
AR'	0.994629492953864	AR'	1.270733115606990
C <sub>2</sub>	1.934346320096740	C <sub>3</sub>	1.329733478780440
S <sub>2</sub>	1.272596263221540	S <sub>3</sub>	1.063786783024350

Table C8. Blade Geometry Results (Iteration #3)

Compare  $\tilde{\omega}_T$  (iteration #3) and  $\tilde{\omega}_T$  (iteration #2).

$$|\tilde{\omega}_{T2, \text{iteration3}} - \tilde{\omega}_{T2, \text{iteration2}}| = 0.05385 - 0.05421 = 0.0003654$$

$$|\tilde{\omega}_{T3, \text{iteration3}} - \tilde{\omega}_{T3, \text{iteration2}}| = 0.08508 - 0.08669 = 0.001615$$

### 7. Iteration #4

ROTOR		STATOR	
$\beta_\infty$	56.560435987322300	$\beta_\infty$	27.347157421794000
C <sub>L</sub>	0.586010932091710	C <sub>L</sub>	1.470018487969480
C <sub>Di</sub>	0.014266571444569	C <sub>Di</sub>	0.069221229482487
$\omega_{SFTC2}$	0.027688608666518	$\omega_{SFTC3}$	0.059649745121757
y*	0.908770674133602	y*	1.978417070245130
P <sub>te</sub> /P <sub>ti</sub>	0.999746596870648	P <sub>te</sub> /P <sub>ti</sub>	1.005788072708940
$\omega_{S2}$	0.000470350655165	$\omega_{S3}$	-0.026347850522881
$\omega_{P2}$	0.025691775310535	$\omega_{P3}$	0.025461335476916
$\omega_{T2}$	0.053850734632218	$\omega_{T3}$	0.085111080598674
T <sub>1</sub> /T <sub>t1</sub>	0.957618541339988	P <sub>t3</sub> /P <sub>t1</sub>	1.667847160812340
P <sub>1</sub> /P <sub>t1</sub>	0.859357579736388	T <sub>3</sub> /T <sub>t1</sub>	1.171843486972510
T <sub>R1</sub> /T <sub>t1</sub>	1.15597584087194	T <sub>3</sub> /T <sub>t1</sub>	1.130182173979650
P <sub>R1</sub> /P <sub>t1</sub>	1.660812680211420	P <sub>3</sub> /P <sub>t1</sub>	1.469373484368560
T <sub>E1</sub> /T <sub>t1</sub>	1.178143079024150	$\Phi_{3m}$	0.172237922031280
P <sub>E1</sub> /P <sub>t1</sub>	1.774978623835910	A <sub>3</sub> /A <sub>1</sub>	0.696176074225205
P <sub>E2</sub> /P <sub>t1</sub>	1.731819677900590	A <sub>3</sub> (in)	48.533467856980100
P <sub>t2</sub> /P <sub>t1</sub>	1.699625271359260	r <sub>3m</sub> (in)	4.571286972682070
T <sub>2</sub> /T <sub>t1</sub>	1.091667880043820	h <sub>3</sub> (in)	1.689752002224000
P <sub>2</sub> /P <sub>t1</sub>	1.326253081470570	r <sub>ht3</sub>	0.688016773055056
$\Phi_{2m}$	0.219098107941022	r <sub>3t</sub> (in)	5.416162973794070
A <sub>2</sub> /A <sub>1</sub>	0.772658523297490	r <sub>3h</sub> (in)	3.726410971570070
A <sub>2</sub> (in)	53.865392668966700		
r <sub>2m</sub> (in)	4.455879688743610		
h <sub>2</sub> (in)	1.923962068928580		
r <sub>ht2</sub>	0.644885284576048		
r <sub>2t</sub> (in)	5.417860723207900		
r <sub>2h</sub> (in)	3.493898654279320		

Table C9. Stage Performance Results (Iteration #4)

HUB		TIP	
X <sub>θ2h</sub>	0.259622158556950	X <sub>θ2t</sub>	0.167426509603247
X <sub>U2h</sub>	0.330949191562962	X <sub>U2t</sub>	0.513190794515540
α <sub>2h</sub>	52.835657378138000	α <sub>2t</sub>	40.387939601023500
β <sub>2h</sub>	19.921367002758800	β <sub>2t</sub>	60.351421552757200
X <sub>2h</sub>	0.325787670140640	X <sub>2t</sub>	0.258390357637089
X <sub>W2h</sub>	0.209335822159843	X <sub>W2t</sub>	0.397852839028210
Y <sub>2h</sub>	0.300953805006140	Y <sub>2t</sub>	0.238693997456101
Y <sub>W2h</sub>	0.193378749342774	Y <sub>W2t</sub>	0.367525651558102
M <sub>2h</sub>	0.705668878946494	M <sub>2t</sub>	0.549622946947096
M <sub>W2h</sub>	0.440727113995883	M <sub>W2t</sub>	0.883656465604799
M <sub>Z2h</sub>	0.426296888922253	M <sub>Z2t</sub>	0.418633901914269

Table C10. Rotor Results (Iteration #4)

HUB		TIP	
X <sub>θ3h</sub>	0.000000000000000	X <sub>θ3t</sub>	0.000000000000000
X <sub>U3h</sub>	0.352973231482253	X <sub>U3t</sub>	0.513029980235682
α <sub>3h</sub>	0.000000000000000	α <sub>3t</sub>	0.000000000000000
β <sub>3h</sub>	59.960833770877400	β <sub>3t</sub>	68.304665956674600
X <sub>3h</sub>	0.204111031041579	X <sub>3t</sub>	0.204111031041579
X <sub>W3h</sub>	0.407739396104768	X <sub>W3t</sub>	0.552142258492756
Y <sub>3h</sub>	0.188552229153336	Y <sub>3t</sub>	0.188552229153336
Y <sub>W3h</sub>	0.376658584579527	Y <sub>W3t</sub>	0.510054028522148
M <sub>3h</sub>	0.429316175796641	M <sub>3t</sub>	0.429316175796641
M <sub>W3h</sub>	0.909194410621443	M <sub>W3t</sub>	1.325961290180600
M <sub>Z3h</sub>	0.429316175796641	M <sub>Z3t</sub>	0.429316175796641

Table C11. Stator Results (Iteration #4)

ROTOR		STATOR	
H <sub>2</sub>	1.923962068928580	H <sub>3</sub>	1.689752002224000
C <sub>2</sub> '	1.603301724107150	C <sub>3</sub> '	1.408126668520000
Z <sub>2</sub> '	26.542489415600500	Z <sub>3</sub> '	25.496856731509300
Z <sub>2</sub>	22.000000000000000	Z <sub>3</sub>	27.000000000000000
AR'	0.994631648397049	AR'	1.270744874208740
C <sub>2</sub>	1.934346320096740	C <sub>3</sub>	1.329733478780440
S <sub>2</sub>	1.272596263221540	S <sub>3</sub>	1.063786783024350

Table C12. Blade Geometry Results (Iteration #4)

Compare  $\tilde{\omega}_r$  (iteration #4) and  $\tilde{\omega}_r$  (iteration #3).

$$|\tilde{\omega}_{r2_{\text{iteration4}}} - \tilde{\omega}_{r2_{\text{iteration3}}}| = 0.05385 - 0.05385 = 0.000004683$$

$$|\tilde{\omega}_{r3_{\text{iteration4}}} - \tilde{\omega}_{r3_{\text{iteration3}}}| = 0.08511 - 0.08508 = 0.00003165$$

Both the rotor and stator losses satisfy the criterion after the fourth iteration.

$$\Pi_c = \frac{P_{i3}}{P_{ti}} = 1.6678$$

$$\tau_c = \frac{T_{t2}}{T_{ti}} = 1.1718$$

$$\eta_c = \frac{1.6678^{\frac{1.41}{1.4}} - 1}{1.1718 - 1} = 0.9158 \text{ or } 91.58\%$$

## C2. CODE RESULTS

HUB		MEAN		TIP	
$\beta_{1h}$	52.195176449181800	$\beta_{1m}$	62.343578122316700	$\beta_{1t}$	68.410458367312200
$\alpha_{1h}$	0.000000000000000	$\alpha_{1m}$	0.000000000000000	$\alpha_{1t}$	0.000000000000000
$X_{1h}$	0.205867575543143	$X_{1m}$	0.205867575543143	$X_{1t}$	0.205867575543143
$X_{U1h}$	0.265557741712975	$X_{U1m}$	0.393264467850964	$X_{U1t}$	0.520971193988953
$r_{1h}$	2.794827442941060	$r_{1m}$	4.138860046006270	$r_{1t}$	5.482892649071480
$X_{\theta 1h}$	0.000000000000000	$X_{\theta 1m}$	0.000000000000000	$X_{\theta 1t}$	0.000000000000000
$X_{Z1h}$	0.205867575543143	$X_{Z1m}$	0.205867575543143	$X_{Z1t}$	0.205867575543143
$M_{Z1h}$	0.470410144688393	$M_{Z1m}$	0.470410144688393	$M_{Z1t}$	0.470410144688393
$X_{W1h}$	0.336009483264546	$X_{W1m}$	0.443890076859253	$X_{W1t}$	0.560171798313952
$M_{1h}$	0.470410144688393	$M_{1m}$	0.470410144688393	$M_{1t}$	0.470410144688393
$M_{W1h}$	0.797720638371130	$M_{W1m}$	1.107676776722660	$M_{W1t}$	1.280000000000000
		$A_1$	69.931875719909200		
		$r_{ht1}$	0.509735940829400		
		$\omega$	2836.334567415990000		
		mdot	17.090000000000000		
		$P_{t1}$	14.690000000000000		
		$T_{t1}$	517.800000000000000		
		R	53.350000000000000		
		$\gamma$	1.400000000000000		

Table C13. Inlet Results

HUB		MEAN		TIP	
$\beta_{2h}$	19.153113641505600	$\beta_{2m}$	47.808100398602100	$\beta_{2t}$	60.322721543344400
$\alpha_{2h}$	52.844869054566300	$\alpha_{2m}$	45.871861712689900	$\alpha_{2t}$	40.226189216790300
$X_{2h}$	0.326016514230627	$X_{2m}$	0.282758297008589	$X_{2t}$	0.257833958315095
$X_{U2h}$	0.328294695162428	$X_{U2m}$	0.420281736792325	$X_{U2t}$	0.512268778422222
$r_{2h}$	3.455094238614300	$r_{2m}$	4.423199731166900	$r_{2t}$	5.391305223719500
$X_{\theta 2h}$	0.259909266378080	$X_{\theta 2m}$	0.203022938914057	$X_{\theta 2t}$	0.166566531027495

X <sub>Z2h</sub>	0.196809402219245	X <sub>Z2m</sub>	0.196809402219245	X <sub>Z2t</sub>	0.196809402219245
M <sub>Z2h</sub>	0.426564947028765	M <sub>Z2m</sub>	0.421383869310173	M <sub>Z2t</sub>	0.421383869310173
X <sub>W2h</sub>	0.208351884253337	X <sub>W2m</sub>	0.293147277076569	X <sub>W2t</sub>	0.397798924905110
M <sub>2h</sub>	0.706608604848915	M <sub>2m</sub>	0.605406977153977	M <sub>2t</sub>	0.548663539641709
M <sub>W2h</sub>	0.438807084275359	M <sub>W2m</sub>	0.629379184024538	M <sub>W2t</sub>	0.629379184024538
Y <sub>2h</sub>	0.301318214114674	Y <sub>2m</sub>	0.261337145088495	Y <sub>2t</sub>	0.238301019937484
Y <sub>W2h</sub>	0.192567599892291	Y <sub>W2m</sub>	0.270939078683619	Y <sub>W2t</sub>	0.367662545905120
D <sub>2h</sub>	0.539065878334816	D <sub>2m</sub>	0.455000000000000	D <sub>2t</sub>	0.390436898079840
r <sub>st2h</sub>	0.604152503515955	r <sub>st2m</sub>	0.758468045193244	r <sub>st2t</sub>	0.837422718264700
		$\tau$	1.170653666750960		
		r <sub>ht2</sub>	0.640864149819104		
		$\sigma_{2m}$	1.520000000000000		
		f $\sigma_2$	0.855300000000000		
		R <sub>21</sub>	1.068700000000000		
		$\phi_{21}$	0.956000000000000		

Table C14. Rotor Results

HUB		MEAN		TIP	
$\beta_{3h}$	59.760648493304300	$\beta_{3m}$	64.641480976070200	$\beta_{3t}$	68.231904833353900
$\alpha_{3h}$	0.000000000000000	$\alpha_{3m}$	0.000000000000000	$\alpha_{3t}$	0.000000000000000
X <sub>3h</sub>	0.204111031041579	X <sub>3m</sub>	0.204111031041579	X <sub>3t</sub>	0.204111031041579
X <sub>U3h</sub>	0.350482583299427	X <sub>U3m</sub>	0.431167033775246	X <sub>U3t</sub>	0.511851484251066
r <sub>3h</sub>	3.688607742179240	r <sub>3m</sub>	4.537760604204120	r <sub>3t</sub>	5.386913466229010
X <sub><math>\theta</math>3h</sub>	0.000000000000000	X <sub><math>\theta</math>3m</sub>	0.000000000000000	X <sub><math>\theta</math>3t</sub>	0.000000000000000
X <sub>Z3h</sub>	0.204111031041579	X <sub>Z3m</sub>	0.204111031041579	X <sub>Z3t</sub>	0.204111031041579
M <sub>Z3h</sub>	0.429542339664783	M <sub>Z3m</sub>	0.429542339664783	M <sub>Z3t</sub>	0.429542339664783
X <sub>W3h</sub>	0.405585199667217	X <sub>W3m</sub>	0.477039122093147	X <sub>W3t</sub>	0.551047416220125
M <sub>3h</sub>	0.429542339664783	M <sub>3m</sub>	0.429542339664783	M <sub>3t</sub>	0.429542339664783
M <sub>W3h</sub>	0.904138170145811	M <sub>W3m</sub>	1.098406365761990	M <sub>W3t</sub>	1.098406365761990
Y <sub>3h</sub>	0.188648024471074	Y <sub>3m</sub>	0.188648024471074	Y <sub>3t</sub>	0.188648024471074
Y <sub>W3h</sub>	0.374858949472163	Y <sub>W3m</sub>	0.440899678567374	Y <sub>W3t</sub>	0.509301265734333
D <sub>3h</sub>	0.636269323766171	D <sub>3m</sub>	0.561674862453015	D <sub>3t</sub>	0.527244214226719
r <sub>st3h</sub>	0.604152503515955	r <sub>st3m</sub>	0.758468045193244	r <sub>st3t</sub>	0.837422718264700
		A <sub>31</sub>	1.000000000000000		
		r <sub>ht3</sub>	0.684734916442117		
		$\sigma_{3m}$	1.250000000000000		
		f $\sigma_3$	0.800000000000000		
		R <sub>32</sub>	1.025900000000000		
		$\phi_{32}$	1.037100000000000		

Table C15. Stator Results

ROTOR		STATOR			
$\omega_{SFTC2}$	0.015092502816179	$\omega_{SFTC3}$	0.052221964041667	$\Pi_C$	1.674703502643810
$\omega_{S2}$	0.000415286496133	$\omega_{S3}$	0.000000000000000	$\tau_C$	1.170653666750960
$\omega_{P2}$	0.025621919830276	$\omega_{P3}$	0.025342625084949	$\eta_C$	1.170653666750960
$\omega_{T2}$	0.041129709142588	$\omega_{T3}$	0.077564589126615		
$T_1/T_{t1}$	0.957618541339988	$P_{t3}/P_{t1}$	1.674703502643810		
$P_1/P_{t1}$	0.859357579736388	$T_{t3}/T_{t1}$	1.170653666750960		
$T_{R1}/T_{t1}$	1.15465694167410	$T_3/T_{t1}$	1.128992353758110		
$P_{R1}/P_{t1}$	1.654190026081820	$P_3/P_{t1}$	1.475220458598720		
$T_{E1}/T_{t1}$	1.176636738281170	$\Phi_{3m}$	0.172309288336835		
$P_{E1}/P_{t1}$	1.767048277556160	$A_3/A_1$	0.692686802248097		
$P_{E2}/P_{t1}$	1.734357050220880	$A_3$ (in)	48.440887367635200		
$P_{t2}/P_{t1}$	1.703686175109830				
$T_2/T_{t1}$	1.090701412223770				
$P_2/P_{t1}$	1.330027617869200				
$\Phi_{2m}$	0.218975111752094				
$A_2/A_1$	0.769783662636916				
$A_2$ (in)	53.832415426741300				

Table C16. Stage Performance Results

ROTOR		STATOR	
$H_2$	1.936210985105210	$H_3$	1.698305724049770
$C_2'$	1.613509154254340	$C_3'$	1.415254770041480
$Z_2'$	26.191679106060200	$Z_3'$	25.192519448425300
$Z_2$	22.000000000000000	$Z_3$	27.000000000000000
$AR'$	1.007953705186150	$AR'$	1.277177533055250
$C_2$	1.920932454678200	$C_3$	1.320512345138770
$S_2$	1.263771351761970	$S_3$	1.056409876111010
$i_{2h}^*$	3.027273612963370	$i_{3h}^*$	-14.428782843997100
$i_{2m}^*$	6.757152202149710	$i_{3m}^*$	-1.724296488710650
$i_{2t}^*$	10.291562745234000	$i_{3t}^*$	3.241975399750170
$\phi_{2h}^*$	-42.100896728952500	$\phi_{3h}^*$	76.083582934974900
$\phi_{2m}^*$	-24.523123063313700	$\phi_{3m}^*$	26.611448616369400
$\phi_{2t}^*$	-19.983188007865800	$\phi_{3t}^*$	8.263624315276530
$\delta_{2h}^*$	-5.757137628140870	$\delta_{3h}^*$	21.988386237067600
$\delta_{2m}^*$	-2.833187565346610	$\delta_{3m}^*$	8.688685825842080
$\delta_{2t}^*$	-1.152333894067850	$\delta_{3t}^*$	4.391711979088870

Table C17. Blade Geometry Results



## APPENDIX D. COMPARISON OF RESULTS

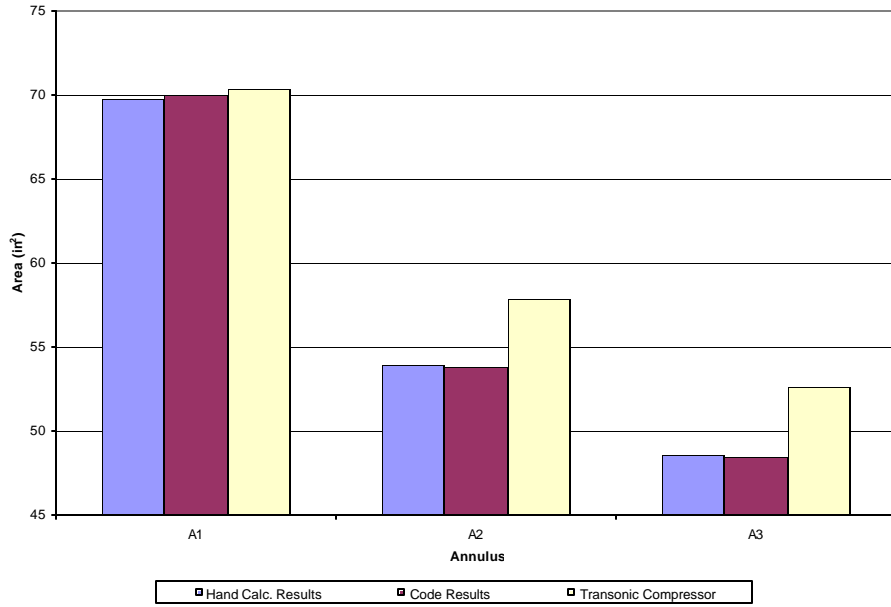


Figure D1. Annulus Comparison

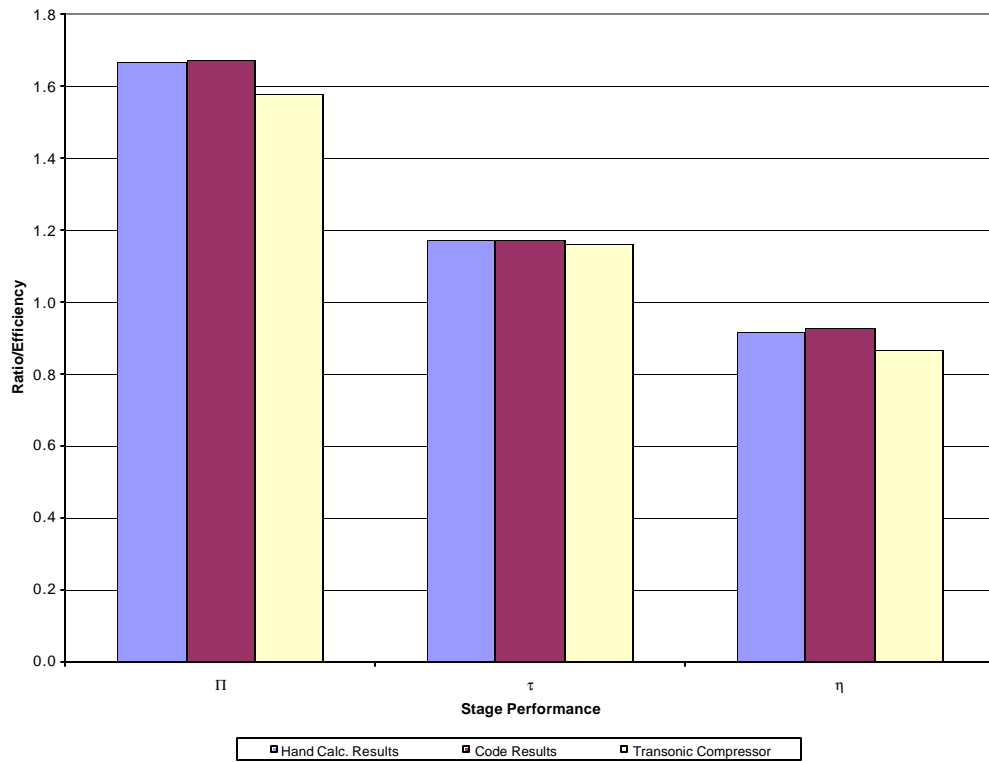


Figure D2. Stage Performance Comparison

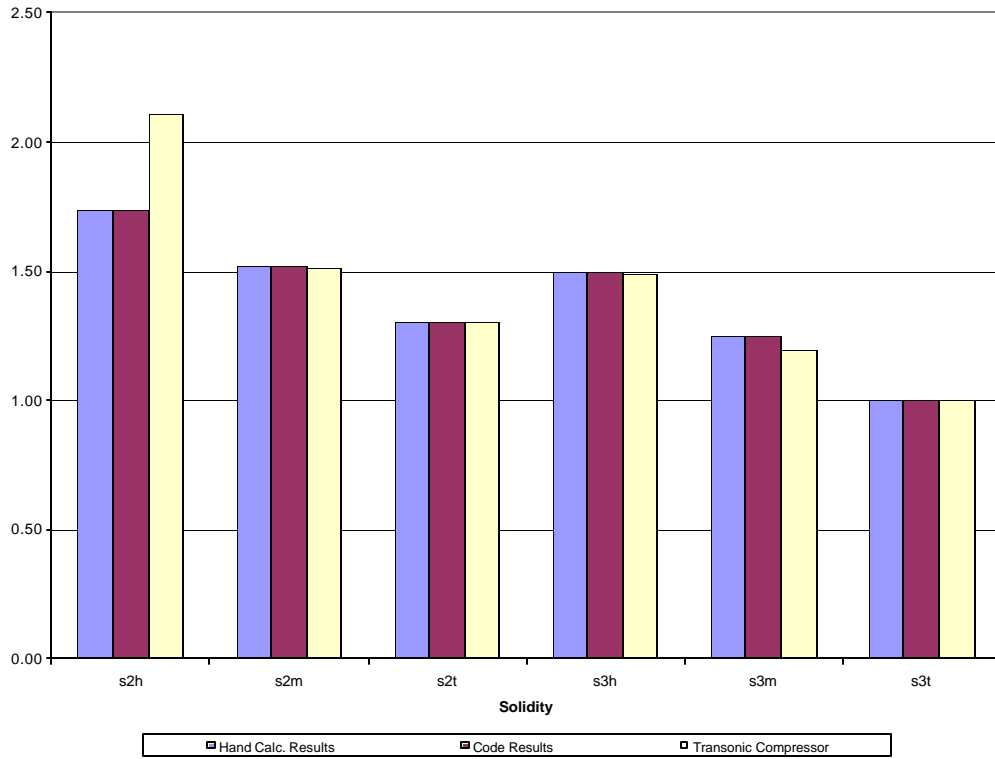


Figure D3. Solidity Comparison

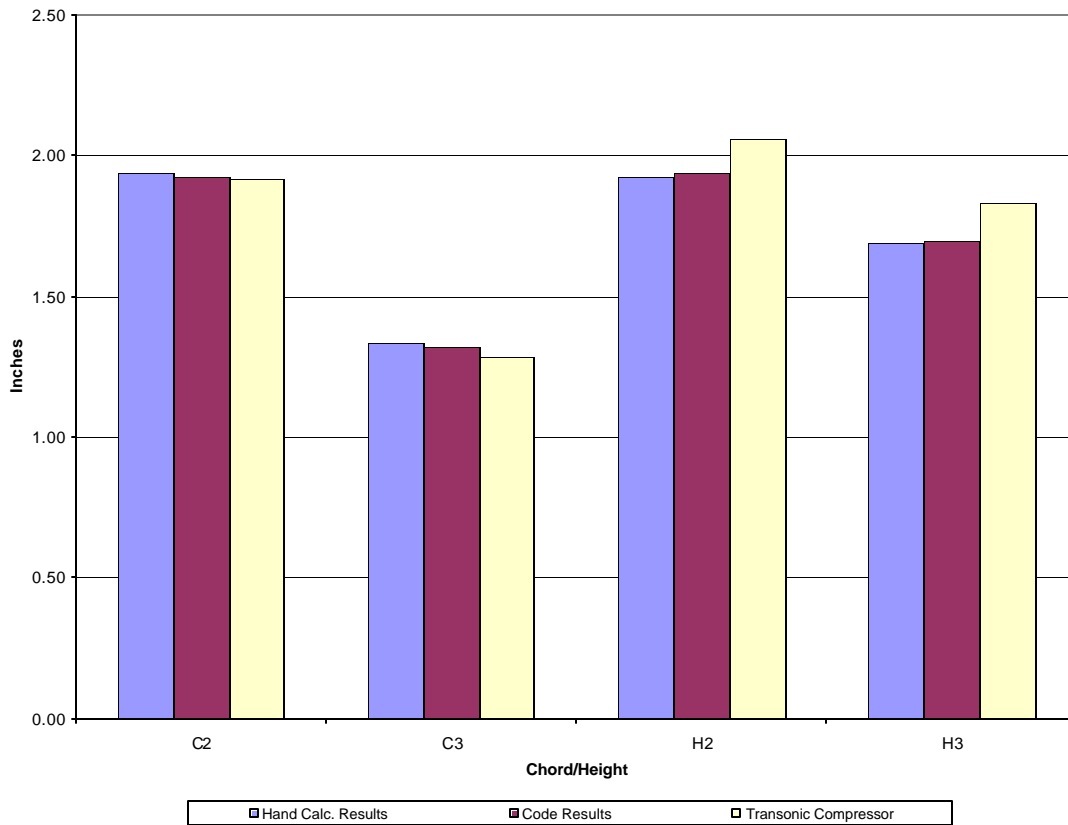


Figure D4. Chord and Blade Height Comparison

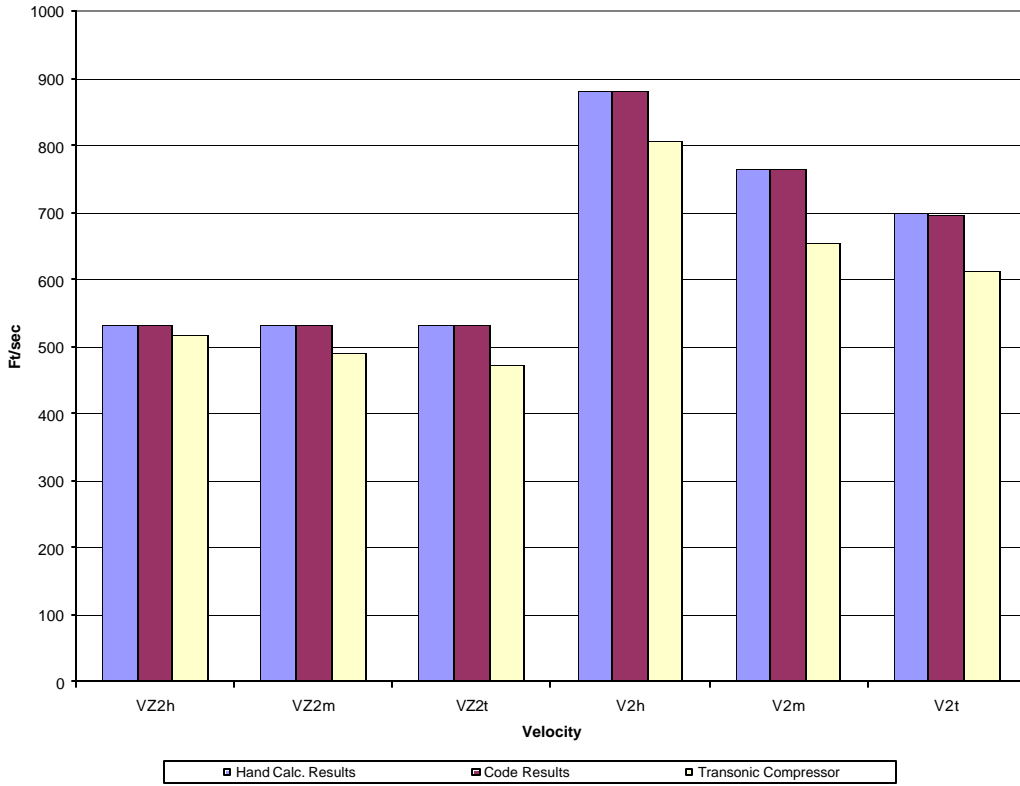


Figure D5. Rotor Velocity Comparison

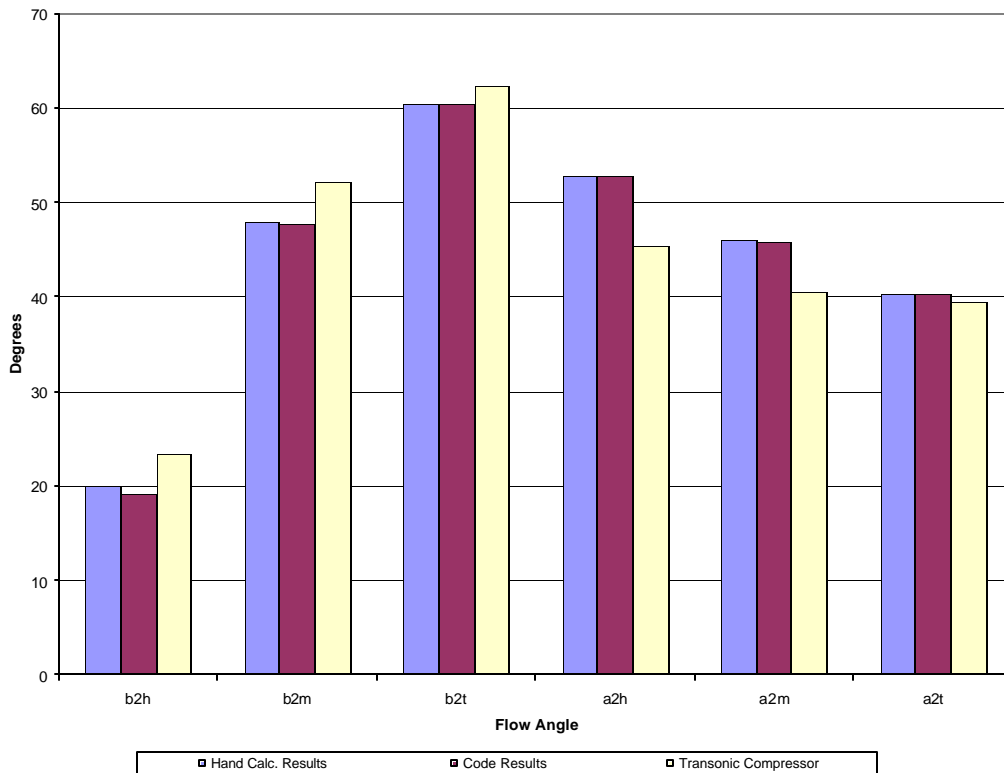


Figure D6. Rotor Flow Angle Comparison

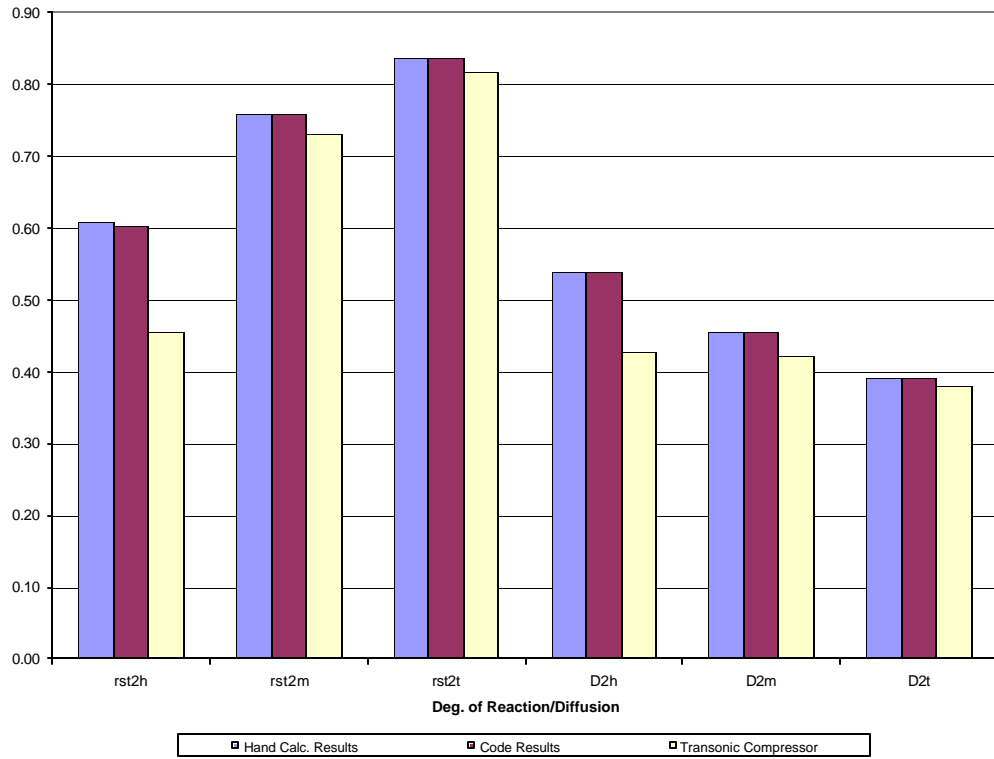


Figure D7. Rotor Degree of Reaction and Diffusion Comparison

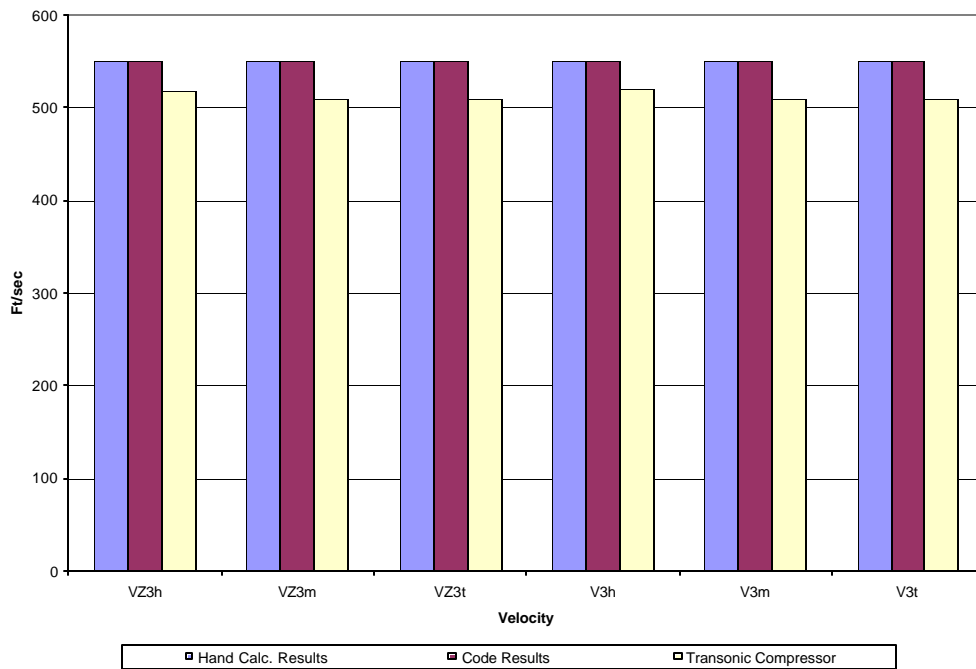


Figure D8. Stator Velocity Comparison

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Naval Postgraduate School  
shreeve@nps.navy.mil
5. Dr. Garth V. Hobson, Code AA/HG  
Department of Aeronautics and Astronautics  
Naval Postgraduate School  
gvhobson@nps.navy.mil
6. Naval Air Warfare Center – Aircraft Division  
AIR-4.4.3.3 (Attn: Mr. J. Zidzik)  
Propulsion and Power Engineering, Bldg. 106  
Zidzikj@navair.navy.mil
7. Naval Air Warfare Center – Aircraft Division  
AIR-4.4.3.3 (Attn: Mr. M. Klein)  
Propulsion and Power Engineering, Bldg. 106  
Kleinma@navair.navy.mil
8. Naval Air Warfare Center – Aircraft Division  
AIR-4.4T (Attn: Mr. C. Gorton)  
Propulsion and Power Engineering, Building 106  
Gortonca@navair.navy.mil
9. Naval Air Warfare Center – Aircraft Division  
AIR-4.4.3.2 (Attn: Mr. R. Ramakdawala)  
Propulsion and Power Engineering, Building 3197  
Ramakdawalr@navair.navy.mil