IMPLEMENTATION OF A MICROTURBINE IN A HYDROGEN ENERGY STORAGE AND GENERATION SYSTEM

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IMPLEMENTATION OF A MICROTURBINE IN A HYDROGEN ENERGY STORAGE AND GENERATION SYSTEM

by

Brianna M. Kaufmann

June 2019

Thesis Advisor: Anthony J. Gannon
Co-Advisor: Andrea D. Holmes

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The energy needs of the Navy and the Department of Defense demand renewability, reliability, and resilience. Diverse means of energy production, including hydrogen gas combustion, support these requirements. The overarching goal of this research is to develop a system that produces and stores hydrogen and then combusts the hydrogen in a commercial microturbine to produce electricity. This thesis focuses on fueling a Capstone C30 MicroTurbine with hydrogen. Future research will produce a complete system that uses renewable resources, reliably produces electricity to meet demand, and demonstrates fuel resiliency.

The implementation of the C30 enables the use of a renewable resource in a reliable and resilient system. A system component with the capability to produce energy from hydrogen (in addition to methane and propane) indicates resilience in fuel choices. If the primary fuel is unavailable, secondary fuels fulfill the demand for energy. Resilient technologies must use several fuels with varying properties. Computational fluid dynamic models establish expected operating differences between different types of fuel. Data collected from the C30 establish operating differences between light hydrocarbon fuels (natural gas, propane) and hydrogen gas. Benefits and challenges of using hydrogen gas-fueled microturbines and recommended improvements are discussed.
IMPLEMENTATION OF A MICROTURBINE IN A HYDROGEN ENERGY STORAGE AND GENERATION SYSTEM

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from the

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June 2019

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ABSTRACT

The energy needs of the Navy and the Department of Defense demand renewability, reliability, and resilience. Diverse means of energy production, including hydrogen gas combustion, support these requirements. The overarching goal of this research is to develop a system that produces and stores hydrogen and then combusts the hydrogen in a commercial microturbine to produce electricity. This thesis focuses on fueling a Capstone C30 MicroTurbine with hydrogen. Future research will produce a complete system that uses renewable resources, reliably produces electricity to meet demand, and demonstrates fuel resiliency.

The implementation of the C30 enables the use of a renewable resource in a reliable and resilient system. A system component with the capability to produce energy from hydrogen (in addition to methane and propane) indicates resilience in fuel choices. If the primary fuel is unavailable, secondary fuels fulfill the demand for energy. Resilient technologies must use several fuels with varying properties. Computational fluid dynamic models establish expected operating differences between different types of fuel. Data collected from the C30 establish operating differences between light hydrocarbon fuels (natural gas, propane) and hydrogen gas. Benefits and challenges of using hydrogen gas-fueled microturbines and recommended improvements are discussed.
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<th>Acronym</th>
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<td>Capstone Remote Monitoring System</td>
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<td>Department of the Navy</td>
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</tr>
<tr>
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<td>turbine exit temperature</td>
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<td>Turbopropulsion Laboratory</td>
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I. INTRODUCTION

The energy needs of the Department of the Navy (DoN) and the Department of Defense (DoD) demand renewability, reliability, and resilience. Diverse means of energy production support these requirement, including hydrogen gas (H₂) combustion. This thesis is one of several researching and developing a H₂ energy storage and generation system.

A. MOTIVATION

H₂ combusts in air to produce heat like gaseous hydrocarbons such as methane (CH₄, the primary component of natural gas) or propane (C₃H₈). However, H₂ produces more energy per unit mass and emits no carbon compounds. Figure 1 visually compares lower heating values (LHV) of mass energy densities. Existing renewable and reliable production methods enable the development of energy resilience with respect to hydrogen-based systems [1].

Figure 1. Mass energy densities of various fuels (LHV) Source: [2].
Recent policy takes a two-pronged approach to energy: first, reduce energy use and second, implement renewable energy technologies where energy use is required. The Energy Policy Act of 2005 focuses on reduced energy use [3]. Among the renewable energy technologies discussed in the act, Title VIII specifically discusses the purposes of hydrogen and hydrogen fuel cells: “to sharply decrease the dependency of the United States on imported oil, eliminate most emissions from the transportation sector, and greatly enhance our energy security and...to create, strengthen, and protect a sustainable national energy economy” [3]. H₂ has been recognized as an energy source for many years, but the enabling technology required for robust and interconnected systems requires more research.

This thesis builds on the work of several other theses. Previous work examined H₂ generation via solar power, automated the production and storage process, and fueled a small turbojet engine with H₂ [4]–[7]. This work focuses on testing a commercial off-the-shelf (COTS) microturbine with H₂ for implementation in a small H₂ generation, storage, and energy generation system. The implementation of a COTS microturbine in a H₂ system demonstrates the use of a renewable resource in a reliable and resilient system. A component with the capability to produce energy from H₂ (in addition to CH₄ and C₃H₈) indicates resilience in fuel choices. If the primary fuel is unavailable, secondary fuels fulfill the demand for energy. This work is sponsored by the Office of Naval Research Energy Systems Technology Evaluation Program under the technical monitoring of Marissa Brand. This research intends to contribute to the efforts of the DoD and DoN to use more renewable energy to increase energy resilience.
B. OBJECTIVES

The primary objective of this research is to fuel a COTS microturbine with H$_2$, demonstrating its role in a larger renewable energy system and ultimately a hydrogen economy. The specific COTS microturbine used is the Capstone Turbine Corporation’s C30 MicroTurbine (C30). The secondary objective is to make design recommendations for improved operation with H$_2$. Enabling objectives include:

1. Installing a low pressure natural gas supply line;
2. Constructing self-contained fuel supply systems for both C$_3$H$_8$ and H$_2$;
3. Implementing remote monitoring software to collect real-time data from the C30;
4. Fueling the COTS microturbine with natural gas and collecting data;
5. Fueling the COTS microturbine with C$_3$H$_8$ and collecting data;
6. Developing a computational fluid dynamics (CFD) model of H$_2$, natural gas, and C$_3$H$_8$ combustion processes.

C. BACKGROUND AND LITERATURE REVIEW

The development of a hydrogen economy is predicted to most heavily impact the transportation, grid services, and some “niche markets” including “remote and backup power” systems [8]. Because this thesis focuses on using small gas turbine technology to produce electricity, emphasis is placed on the significance of grid electricity on the microgrid scale. Melaina [8] specifically identifies turbines as an enabling technology to overcome the challenges of a H$_2$ grid: “The conversion of hydrogen back to grid electricity … is challenging economically for grid-connected systems because of significant energy losses. Where reconversion to grid electricity is viable, it may be achieved by using either stationary fuel cells or thermal conversion units, such as turbines” (emphasis added). More research is required to develop economically viable large-scale H$_2$ grids; smaller or more isolated grids are suited to H$_2$ fuel.
Current means of H₂ production, storage, and transportation are the limiting factors of wide distribution to economically viable large-scale grids. Smaller grids address production and storage on-site and reduce or eliminate transportation demands. Today, the majority of industrial H₂ production “is by steam reforming of the natural gas, and gives rise to a lot of carbon dioxide” [9]. Large volumes of H₂ are produced via electrolysis of water on U.S. Navy submarines, but because oxygen is the only desired result, H₂ is dumped overboard. Instead of fossil fuels and discarded H₂, production means are focused on electrolysis using electricity from renewable sources [1]. Levene describes the vast resources of solar and wind energy as mathematically feasible for H₂ production: “certainly enough renewable energy resources exist to provide the electricity needs for renewable hydrogen generation, but the most economic configuration has yet to be identified” [1]. The current system at the Naval Postgraduate School (NPS) Turbopropulsion Laboratory (TPL) uses solar power, photovoltaic cells, and dehumidifiers to produce H₂ from atmospheric water using only renewable energy [4]–[6]. The electrolysis process is well-understood but not yet implemented on a large- and/or economically feasible scale. However, at high temperatures (between 700ºC and 900ºC) electrolysis becomes more thermodynamically favorable and at even higher temperatures (above 900 ºC) H₂ may be thermochemically produced [9]. Coupling waste heat-intensive renewable and/or carbon-neutral energy production (e.g., nuclear power) with H₂ production may make H₂ more economically feasible [9].

Storage challenges compound the challenges of production. Although H₂ has a high mass energy density, its volumetric energy density pales in comparison to heavier hydrocarbon fuels. Figure 2 visually compares the LHV of volumetric energy densities of various fuels. Even liquid H₂ struggles to attain a third of the energy per unit volume that liquid gasoline or liquid diesel can provide [2].
H₂ may be stored in gaseous form, liquid form, or within solid media [2]. Metallic cylinders (typically steel or aluminum) can store H₂ at high pressures and atmospheric temperatures. These cylinders are compact and portable but contain only small amounts of H₂; additionally, over long-term use “hydrogen may degrade the mechanical behavior of metallic materials used in the hydrogen infrastructure (e.g., storage tanks)” [2]. Liquid storage requires moderate pressures and low temperatures. The Linde cycle and the Claude cycle are two common methods of liquefaction but require significant amounts of energy [2]. Solid media include metal hydrides, non-carbon porous materials, and new materials such as boron nitride nanotubes [2]. Although these media have potential for improved volumetric storage capacity at low pressures, the technologies are not yet mature and face weight-to-power ratio drawbacks [2]. The current system at the TPL and this research store and use H₂ in gaseous form [4]. For the same reasons of material degradation and volumetric energy density, continuously transporting large masses of H₂ over long distances becomes challenging.

Despite these infrastructure challenges, H₂ combustion has undisputable benefits of being emissions-free and completely renewable. The DoD and DoN have invested in hydrogen-based technologies and support research to develop a hydrogen economy. This research contributes to one small aspect of a larger effort.
D. APPROACH

This thesis approached the challenges of increasing energy resilience and using H\textsubscript{2} in a microgrid by testing the feasibility of fueling a COTS microturbine with H\textsubscript{2}. Simulation used computational fluid dynamics (CFD) tools to predict the different volumetric flow rates required for and temperatures produced during combustion of C\textsubscript{3}H\textsubscript{8}, natural gas, and H\textsubscript{2}. Experimental testing began with baseline performance of the C30 using the specified fuels of natural gas and C\textsubscript{3}H\textsubscript{8} and proceeded to testing with H\textsubscript{2}.
II. SIMULATION

Because H₂ is less dense at the same temperature and pressure and has different properties from current hydrocarbon fuels (CH₄, C₃H₈, kerosene, etc.), simulation is necessary to predict the effects of using a different fuel than the power generation system specifies. For example, fuel nozzle designs take into account the mass and volumetric flow rates and the laminar flame speed of the intended fuel. Two programs modeled aspects of the C30’s expected performance using H₂: the ANSYS CFX suite and GasTurb 11.

A. ANSYS CFX CFD COMBUSTION SIMULATION

The ANSYS CFX suite of combustion simulation tools developed a CFD simulation of H₂ burning in air in a combustion chamber. The information gained from the simulation predicted some of the effects of using H₂ in the fuel nozzles and combustion chamber and the associated possible technical design changes. The C30 has a fuel nozzle and combustion chamber indicated for use with C₃H₈ or natural gas. Future power generation systems will require redesigned or improved fuel nozzles indicated for use with one or more types of fuels, including H₂.

Using the principles contained within “Chapter 20: Radiation and Combustion in a Can Combustor” of ANSYS CFX Tutorials, 16th ed. and guidance from ANSYS CFX-Solver Theory Guide, 15th ed., a model of a generic fuel nozzle was developed and evaluated for C₃H₈-air combustion [10], [11]. Subsequently, the performance of the same nozzle with CH₄-air combustion and H₂-air combustion was evaluated. CH₄ is the simplified composition of natural gas for the purposes of this simulation. In Chapter IV, Section B natural gas test runs are labeled “CH₄” for brevity and to identify CH₄ as the primary component of natural gas.

Data on fuel inlet velocity, maximum temperature achieved, and mass air-fuel ratios were collected and compared for each fuel type. Design improvements to the fuel nozzle for use with H₂ were recommended.
1. Procedure

The following procedure is paraphrased from chapter 20 of the ANSYS CFX Tutorials [10].

1. Create a standalone CFX system in the ANSYS Workbench environment.

2. Download the CombustorMesh.gtm mesh file from the ANSYS Customer Portal and import the mesh into standalone CFX system. The provided mesh was determined to have sufficient resolution and was unchanged.

3. Create a reacting variable composition mixture by selecting the appropriate H2 -, CH4-, or C3H8-air reacting mixture. The mixtures are simplified: the “NO PDF reaction specifies complete combustion of the fuel into its products in a single-step reaction” [10]. Additionally, “setting the radiation properties explicitly will significantly shorten the solution time” [10]. These selections reduce the computational and time demands of the simulation without significantly affecting the result [11].

4. Develop the simulation domain and create boundaries of the following types: inlet, outlet, and wall. This process establishes the fuel and air flow paths. The independent variable controlled in this simulation is the fuel inlet velocity. Use the default k-ε turbulence model and the default turbulence intensity option, Medium (Intensity = 5%).

5. Set the solver control settings. The tutorial recommends a maximum of 100 iterations and a physical timescale of 0.025 seconds (s). However, the physical time step was changed to 0.015 s, the maximum iterations to 500, and the RMS to 1e-5 to ensure convergence of the solution.

6. Obtain the solution and collect the specified data. The data collected included the fuel inlet velocity and a map of the temperatures achieved inside the combustion chamber. Additionally, ANSYS’s function calculator collected mass flow rates at the fuel inlet and both the primary and secondary air inlets. The actual mass air-fuel ratio and the
stoichiometric air-fuel ratio were compared for each air-fuel mixture and inlet velocity.

7. Repeat steps 3 through 6 until all data has been collected for the desired fuel inlet velocities and fuel-air mixtures.

2. **Propane-Air Combustion (Eddy Dissipation Model)**

C₃H₈-air combustion occurred with a fuel inlet velocity of 40 meters per second (m/s) [10]. The maximum temperature achieved inside the combustion chamber is 2392.49 Kelvin (K). The mass air-fuel ratio at the inlets is 12.91, less than the amount of air required for a stoichiometric mass air-fuel ratio of 15.67 [12]. This combustion chamber runs rich. The temperature map, shown in Figure 3, reveals turbulent air-fuel mixing and a developed flame that is centered in the combustion chamber but impinges on the combustion chamber walls near the outlet. Temperatures near the combustion chamber side walls are half those found in the flame.
In Figure 3 and subsequent temperature maps, ANSYS CFX varies the temperature scales (shown on the left-hand side of each figure) from the maximum to the minimum temperatures achieved in the simulation. The scale changes with each fuel scenario.

Figure 4 shows the fuel mass fraction compared to all combustion products and reactants inside the combustion chamber. Some C$_3$H$_8$ is observed leaving the combustion chamber due to the rich mass air-fuel ratio and incomplete combustion. C$_3$H$_8$ still undergoing combustion at the combustion chamber outlet may cause a flame to impinge upon the walls of the combustion chamber.
Figure 4. Fuel mass fraction inside the combustion chamber (C₃H₈-air reaction, 40 m/s)

3. Methane-Air Combustion (Eddy Dissipation Model)

CH₄-air combustion occurred with a fuel inlet velocity of 40 m/s [10]. The maximum temperature achieved inside the combustion chamber is 2225.44 K. The mass air-fuel ratio at the inlet is 35.46, which is approximately twice the amount of air required for a stoichiometric mass air-fuel ratio of 17.19 [12]. This combustion chamber runs lean, typical of most gas turbines. (ANSYS’s tutorial specifies the use of CH₄; the resulting flame pattern factor and mass air-fuel ratio are ideal for the design of the can combustor [10].) These data support the conclusion that for fuels of a higher volumetric energy density, the volume flow rate must be reduced (e.g., C₃H₈), and that inversely, fuels (e.g., CH₄ and H₂) with a lower volumetric energy density require an increased volume flow rate [2]. For an inlet orifice of constant area, the same fuel inlet velocity produces the same volumetric flow rate for a fluid. With the same fuel inlet velocity, C₃H₈ and CH₄
have the same volumetric flow rate. However, the higher volumetric energy density of C₃H₈ produces rich combustion while the lower volumetric energy density of CH₄ produces lean combustion.

The temperature map, shown in Figure 5, reveals turbulent air-fuel mixing and a developed flame that is centered in the combustion chamber and connects near the outlet. Temperatures near the combustion chamber side walls are less than half those found in the flame. This flame-to-wall temperature ratio is slightly higher than the same temperature ratio for C₃H₈. A high temperature ratio, or steeper temperature gradient, between the flame and the walls reduces the thermal load on the materials that comprise the combustion chamber.

Figure 5. Temperature inside the combustion chamber (CH₄-air reaction, 40 m/s)
Figure 6 shows the fuel mass fraction compared to all combustion products and reactants inside the combustion chamber. CH$_4$ is observed to undergo complete combustion. No flame will impinge upon the walls of the combustion chamber.

![Figure 6. Fuel mass fraction inside the combustion chamber (CH$_4$-air reaction, 40 m/s)](image)

4. **Hydrogen-Air Combustion (Eddy Dissipation Model)**

H$_2$-air combustion occurred with a fuel inlet velocity from 10 m/s to 60 m/s in increments of 5 m/s, with an additional data point at 165 m/s. The fuel inlet velocity was varied to determine the volumetric flow rate at which the flame pattern factor and mass air-fuel ratio most resembled operation with CH$_4$ at a fuel inlet velocity of 40 m/s [10]. Table 1 contains fuel inlet velocities, maximum temperatures, and mass flow ratios for H$_2$-air combustion. The equivalence ratio compares the simulated mass air-fuel ratio to the stoichiometric mass air-fuel ratio of 34.3 for H$_2$ [12].
Table 1. H₂-air combustion chamber data

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</table>

Figure 7 shows the temperature map for a H₂ fuel inlet velocity of 40 m/s (the same fuel inlet velocity tested for CH₄ and C₃H₈). The maximum temperature inside the combustion chamber is 2151.32 K. The mass air-fuel ratio at the inlets is 282.0, which is an order of magnitude higher than the stoichiometric mass air-fuel ratio of 34.3 [12]. This combustion chamber runs lean at all fuel inlet velocities tested. The high laminar flame speed of H₂, coupled with the low volumetric energy density, produces a poorly developed flame [12].
The last row in Table 1 fuels the combustion chamber at a mass air-fuel ratio twice that of the mass air-fuel stoichiometric ratio. This operating point was chosen because the CH4-fueled chamber uses this mass air-fuel ratio at its design performance. An inversely proportional relationship exists between fuel inlet velocity and the mass air-fuel ratio through a constant cross-sectional area. Extrapolating the results from 10 m/s to 60 m/s, the resulting velocity is 165 m/s. Appendix A contains the pertinent calculations. Additionally, all results from all simulations are tabulated in Appendix B and temperature maps for all fuel inlet velocities simulated are contained in Appendix C. At this velocity, the maximum temperature achieved in the H2-air combustion chamber is 2491.92 K, 266.48 K higher than the maximum temperature achieved in the CH4-air combustion chamber at 2225.44 K and 99.43 K higher than the maximum temperature achieved in the
C₃H₈-air combustion chamber at 2392.49 K. This combustion chamber runs lean at all fuel inlet velocities tested.

Figure 8 shows the temperature map for a H₂ fuel inlet velocity of 165 m/s (the calculated fuel inlet speed required to maintain a mass air-fuel ratio twice that of the stoichiometric air-fuel ratio). The maximum temperature inside the combustion chamber is 2491.92 K. The mass air-fuel ratio at the inlets is 68.43, which is twice that of the stoichiometric mass air-fuel ratio of 34.3 [12]. This combustion chamber runs lean. The flame reveals turbulent air-fuel mixing and a developed flame that is centered in the combustion chamber and connects near the outlet in a pattern factor similar to that found in the CH₄-fueled combustion chamber. However, temperatures near the combustion chamber side walls are higher than those found in the CH₄-fueled combustion chamber.

Figure 8. Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 165 m/s)
There are two challenges associated with the fuel inlet velocity of 165 m/s and resulting temperature. First, as the material composition of this generic combustion chamber is unknown, it is uncertain whether the increased temperature will cause immediate and/or long-term damage to the combustion chamber. A key challenge in using H₂ in the place of light hydrocarbon fuels is the increased flame temperature. The adiabatic flame temperatures of C₃H₈, CH₄, and H₂ in air are 1980 K, 1963 K, and 2254 K, respectively [12]. Second, the fuel nozzle design of this combustion chamber may not be able to supply the H₂ at the required volumetric flow rate.

Figure 9 shows the fuel mass fraction compared to all combustion products and reactants inside the combustion chamber. This data was taken with a fuel inlet velocity at 165 m/s. H₂ is observed to undergo complete combustion, with the fuel mass fraction reaching zero by one-quarter the length of the combustion chamber. No flame will impinge upon the walls of the combustion chamber.
Figure 9. Fuel mass fraction inside the combustion chamber (H$_2$-air reaction, 165 m/s)
Figure 10 compares inlet velocity to the resulting maximum temperature in the H$_2$-air combustion chamber. The maximum temperatures achieved using CH$_4$ and C$_3$H$_8$ are included.

The maximum temperature increases with fuel inlet velocity. For lean combustion, more fuel in the same amount of air will produce more heat. (For the same inlet velocity, CH$_4$ and C$_3$H$_8$ produce more heat because the greater fuel density allows proportionally more fuel.) Due to the unstable nature of the H$_2$ flame, the maximum temperature achieved is also unstable at low fuel inlet velocities and is not directly proportional to the fuel inlet velocity, as shown.
Figure 11 compares inlet velocity to the mass air-fuel ratio. For a constant inlet velocity, H$_2$ produces a higher mass air-fuel ratio than CH$_4$ or C$_3$H$_8$ because of its lower density at the same temperature and pressure.

![Diagram showing mass air-fuel ratio vs. fuel inlet velocity](image)

**Figure 11.** The mass air-fuel ratio is inversely proportional to the fuel inlet velocity.

Future simulation work should redesign the nozzle and ensure that all materials in the combustion chamber are suitable for the increased temperature. This information will contribute to an improved microturbine design for operation with H$_2$.

**B. GASTURB SIMULATION**

GasTurb 11 is a program that allows analysis of gas turbine performance, both on- and off-design, for several types of gas turbines with widely varying parameters. It was
used to model the expected performance and fuel mass flow rate at the full power output, 30 kilowatts (kW), of the C30 using H₂ and natural gas. Although the C30 was only tested at idle speeds, this model predicted the change in fuel demands as a function of different types of fuel. Appendix D contains the full input decks used and several output decks.

1. **Data Input**

   The C30 specifications identified in the thermodynamic model validation by Gimelli and Sannino were used to develop data inputs for GasTurb [13]. The inputs and GasTurb program environment are shown in Figure 12. For these same inputs, the drop-down menu was used to select natural gas or H₂ fuel. Then a single on-design cycle was run and data was collected.

![Figure 12. GasTurb 11 input parameters using H₂](image)
2. **Data Output and Results**

For natural gas, the calculated fuel mass flow rate was 0.00230 kilograms per second (kg/s). H₂ produced a fuel mass flow rate of 0.00095548 kg/s. Both data points were simulated at full power (30 kW) although experimental testing was only completed at idle speeds and no power output. These calculations confirm the high mass energy density of H₂ compared to natural gas and also present an upper bound on the expected fuel consumption during test runs of the C30. Figure 13 shows a temperature-entropy plot of the C30 simulated with H₂.

![Figure 13. GasTurb 11 output temperature-entropy plot using H₂](image)

Figure 13. GasTurb 11 output temperature-entropy plot using H₂
III. SYSTEM DESIGN

Previous research focused primarily on the production, compression, and storage of H2 [4]–[6]. Beginning with Penley’s research on the operation of a small gas turbine, each power generation system required the construction of a fuel supply system [7]. This research used C30 engines and constructed three fuel supply systems, one each for C₃H₈, natural gas, and H₂ systems.

A. KEY ENABLING TECHNOLOGY

1. Capstone C30 MicroTurboine

The C30 is an “adaptable, low-emission, and low maintenance power generation system” [14]. It is rated up to 30 kW. A single spool turbogenerator for electricity generation, it incorporates air bearings to reduce the frequency of maintenance required. A diagram of its typical engine is shown in Figure 14. This technology was chosen for its ability to “efficiently use a wide range of approved hydrocarbon-based gaseous and liquid fuels” [14]. This flexibility indicated capable technology and the potential for using H₂. The CRMS enabled remote operation, increasing safety during operation, and allowed data collection essential to this research.

This research used two C30 engines both rated for use with natural gas and C₃H₈, one with a high-pressure inlet and one with a low-pressure inlet. Commercial natural gas lines into buildings supply fuel at low pressures (between 1.72 and 34.5 kilopascals (kPa) depending on the location in the supply line). The C30 requires fuel from 350–380 kPa at the inlet [14]. The low-pressure C30 contains a booster pump to increase the fuel pressure if the supply pressure is too low. The high-pressure C30 contains no such pump and requires the fuel supply to be at an adequate pressure. The different C30s at the TPL provided flexibility in using different fuel supplies, including a low-pressure natural gas line and high-pressure cylinders of C₃H₈ and H₂.
2. Additional Components

Each fuel supply system required components suitable for use with each type of fuel. H₂ is more flammable than C₃H₈ or CH₄. The fuel supply system for H₂ required additional safety precautions in the form of component selections and procedures for operation. Components were selected on the basis of material properties (e.g., resistance to H₂ embrittlement) and availability at the TPL.
B. PROPANE-FUELED SYSTEM

The C_3H_8-fueled system connects a tank of C_3H_8 to the high-pressure C30 via a brass regulator and flexible hose tubing. These components are well-tested for C_3H_8 use. The high-pressure C30 was selected because the C_3H_8 tank supplies fuel at or above the specified pressure [14]. Figure 15 shows the tank, regulator, and flexible hose tubing.

Figure 15. C_3H_8 tank, regulator, and flexible tubing assembly
C. NATURAL GAS-FUELED SYSTEM

The natural gas-fueled system required the installation of a low-pressure natural gas line. Naval Facilities Engineering Command at NPS installed the natural gas line and connected it to the low-pressure C30. The line supplies natural gas at 34.5 kPa and has a manual shutoff valve 40 centimeters from the connection to the C30. It is stored in a shed for protection from the elements. A duct guides exhaust air from the C30 out of the shed, as in Figure 16.

Figure 16. Low-pressure C30 inside the protective shed with the exhaust duct visible near the top of the image
D. HYDROGEN-FUELED SYSTEM

The H₂-fueled system required the construction of a separate, H₂-rated fuel supply system to fuel the high-pressure C30. The high-pressure C30 was selected because the H₂ tank supplies H₂ at or above the specified pressure [14]. A H₂ tank leads to a regulator with inlet and outlet pressure gauges, a manual shutoff valve, a check valve, tubing, two solenoid valves, and a flame arrestor. The tubing, regulators, and valves used in the H₂ system are comprised of copper and stainless steel. The flame arrestor is brass. Figures 17 through 19 show the experimental setup.

Figure 17. H₂ regulator assembly, including the regulator, pressure gauges, manual shutoff valve, and check valve

The H₂ tank is visible on the right side of Figure 17. The regulator, manual shutoff valve, and check valve are attached. The regulator, including the inlet and outlet pressure...
valves, leads to the manual shutoff valve. A check valve is downstream of the shutoff valve to prevent flow towards the H₂ tank in the event of flashback. Stainless steel tubing connects the regulator assembly to the vertically mounted components, including two solenoid valves and the flame arrestor.

Figure 18 shows a section of the vertically mounted stainless steel tubing, connected to the flame arrestor and a solenoid valve. The flame arrestor comprises a heat sink and a one-way check valve that will extinguish a flame and prevent further propagation if one travels upstream (“flashback”) towards a fuel source and an overpressure relief valve. The solenoid valves control H₂ flow into the engine or through a vent and are controlled remotely.

Figure 18. Flame arrestor and solenoid valve, vertically mounted on a steel panel
Figure 19 shows the entire fuel supply system. The H₂ tank and the high-pressure C30 are connected to the system. The system was remotely controlled for safety. The procedure for operating the H₂ fuel supply system can be briefly described as manually opening the H₂ tank, evacuating the area, remotely actuating the solenoid valves, and remotely starting the C30. The procedure is described in detail in Appendix E.
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IV. OPERATION OF CAPSTONE C30 MICROTURBINE

The Capstone Remote Monitoring System (CRMS) enabled the collection of detailed operational data from both C30s. The low-pressure C30 ran on natural gas; the high-pressure C30 ran on C₃H₈ and H₂. Operation times ranged from 1 minute, 28 seconds to 1 hour, 9 minutes, and 45 seconds. Table 2 summarizes the data. A primary method of measuring whether combustion occurred and achieved steady-state operation inside the C30 is the turbine exit temperature (TET). The TET should rise quickly and then stabilize.

For all test runs, the start command was given by the user via the control mode in CRMS. C₃H₈ and natural gas test runs were shut down by a user command. The three H₂ runs shut down automatically in accordance with the C30’s operating software with a fault code of 6012 (“FLAMEOUT_LOAD”) [15].

A. RESULTS

Table 2 describes the pressure, duration of run, and temperature data collected from four test runs of the high-pressure C30 with C₃H₈ and H₂ and one test run of the low-pressure C30 with natural gas. Maximum TET and the change in TET (the initial TET subtracted from the maximum TET achieved) are both included in Table 2. The change in TET is included because the C30 was not cooled to ambient temperatures between H₂ runs. Complete cooling was time-prohibitive during testing; the raised initial temperature did not affect operation.

In addition to the quantitative data collected, qualitative observations of the sound produced by the C30 during operation indicates that natural gas has the smoothest operation. Operation with C₃H₈ produced a throbbing sound representative of an unstable flame inside the combustion chamber. The C30 was run at idle speeds, producing only the power required to charge the internal battery. Producing power may stabilize the C₃H₈ flame. The internal battery provides power at startup, bringing the turbine speed to 25000 revolutions per minute (RPM) prior to ignition. Initial operation with H₂ produced sounds akin to operation with natural gas: the C30 engine speed and sound correlated at startup and H₂ produced an audible “pop” sound at ignition. Although the flameout was not
audible, the slowing turbine could be heard following the fault code and automatic shutdown process.

Table 2. Runtime data for C30 tests

<table>
<thead>
<tr>
<th>Fuel</th>
<th>C₃H₈</th>
<th>Natural Gas</th>
<th>H₂ Run 1</th>
<th>H₂ Run 2</th>
<th>H₂ Run 3</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input Pressure [kPa]</td>
<td>414</td>
<td>34.5</td>
<td>276</td>
<td>448</td>
<td>517</td>
</tr>
<tr>
<td>Fuel Valve Exit Pressure [kPa]</td>
<td>409</td>
<td>310</td>
<td>35.2</td>
<td>51.0</td>
<td>53.8</td>
</tr>
<tr>
<td>(TET_{maximum} – TET_{initial}) [ºC]</td>
<td>625</td>
<td>636</td>
<td>189</td>
<td>399</td>
<td>429</td>
</tr>
<tr>
<td>Maximum TET [ºC]</td>
<td>676</td>
<td>674</td>
<td>235</td>
<td>517</td>
<td>604</td>
</tr>
<tr>
<td>Total Runtime [HH:MM:SS]</td>
<td>01:09:45</td>
<td>00:34:14</td>
<td>00:01:28</td>
<td>00:01:31</td>
<td>00:01:33</td>
</tr>
<tr>
<td>Time to Achieve 95% of Maximum TET [s]</td>
<td>18</td>
<td>22</td>
<td>15</td>
<td>15</td>
<td>17</td>
</tr>
</tbody>
</table>

1. Propane-Fueled Operation, High-Pressure C30, Run 1 of 1

Figure 20 displays the engine speed profile for the entire duration of the test. The maximum engine speed achieved was 45338 RPM. Figure 21 displays the TET profile. The C30 operated for an extended period of time at steady-state. The sudden drop in TET visible in Figure 21 occurs when combustion is extinguished; air flow through the C30 continues as the compressor and turbine slow. The brief spike in TET in the final seconds of operation occur when the compressor and turbine have stopped the cooling airflow.
Figure 20. Total runtime vs. engine speed (C$_3$H$_8$-fueled operation with high-pressure C30)

Figure 21. Total runtime vs. turbine exit temperature (C$_3$H$_8$-fueled operation with high-pressure C30)
2. Natural Gas (CH₄)-Fueled Operation, Low-Pressure C30, Run 1 of 1

Figure 22 displays the engine speed profile for the entire duration of the test. The maximum engine speed achieved was 51674 revolutions per minute (RPM). Figure 23 displays the TET profile. The C30 operated for an extended period of time at steady-state. During shutdown, the C30 will continue to operate to recharge the battery if its charge is less than 90% [14]. The “step” decrease in engine speed observed during the shutdown process, more visible than in the C₃H₈ run, is the result of this process. The C₃H₈ run operated for 1 hour, 9 minutes, and 45 seconds and charged the internal battery for more time than the natural gas run, which operated for 34 minutes and 14 seconds.

Figure 22. Total runtime vs. engine speed (natural gas (CH₄)-fueled operation with low-pressure C30)
3. **Hydrogen-Fueled Operation, High-Pressure C30, Run 1 of 3**

Figure 24 displays the engine speed profile for the entire duration of the test. The maximum engine speed achieved was 46218 revolutions per minute (RPM). Figure 25 displays the TET profile. Ignition occurred at 53 s. The C30 operated for a short period of time and did not achieve steady-state.
Figure 24. Total runtime vs. engine speed (H$_2$-fueled operation with high-pressure C30, Run 1)

Figure 25. Total runtime vs. turbine exit temperature (H$_2$-fueled operation with high-pressure C30, Run 1)
4. Hydrogen-Fueled Operation, High-Pressure C30, Run 2 of 3

Figure 26 displays the engine speed profile for the entire duration of the test. The maximum engine speed achieved was 45636 revolutions per minute (RPM). Figure 27 displays the TET profile. Ignition occurred at 53 s. The C30 operated for a short period of time and did not achieve steady-state.

Figure 26. Total runtime vs. engine speed (H₂-fueled operation with high-pressure C30, Run 2)
5. **Hydrogen-Fueled Operation, High-Pressure C30, Run 3 of 3**

Figure 28 displays the engine speed profile for the entire duration of the test. The maximum engine speed achieved was 45402 revolutions per minute (RPM). Figure 29 displays the TET profile. Ignition occurred at 53 s. The C30 operated for a short period of time and did not achieve steady-state.
Figure 28. Total runtime vs. engine speed (H₂-fueled operation with high-pressure C30, Run 3)

Figure 29. Total runtime vs. turbine exit temperature (H₂-fueled operation with high-pressure C30, Run 3)
B. ANALYSIS

The engine speed and TET profiles of C$_3$H$_8$, natural gas, and H$_2$ combustion trend together at startup (from the time at which the C30’s internal fuel valve opens to the time at which 95% of the maximum TET for each run is achieved) as shown in Figures 30 and 31. These trends indicate that the C30 combusts the three fuels similarly. Appendix F contains calculations of the mass energy density and volumetric energy density of the fuels used at the temperatures and pressures used in the fuel supply systems. The similarity of the final TET, despite the differences in fuel energy densities, indicates that TET is a programmed set point within the C30.

Figure 30. Engine speed from start command to time at which 95% of maximum TET is achieved
Figure 31. TET from start command to time at which 95% of maximum TET is achieved

C₃H₈ and natural gas operated at steady-state, maintaining constant speed and temperature on the timescale of minutes to hours. H₂ operated for approximately 1 minute and 30 seconds for each of the three test runs; each caused the C30 to stop automatically in accordance with its programming due to a fault code 6012 (“FLAMEOUT_LOAD”) [15]. The cause of the flameout is predicted to be a lean blowout. The insufficient volumetric H₂ flow coupled with the fast laminar flame speed of H₂ could not sustain combustion. Increasing the fuel supply pressure and therefore the fuel supply velocity and volumetric flow rate increased the runtime for the three runs. Figure 32 plots the total runtime against the fuel system supply pressure. The text describes the pressure data at the C30’s internal fuel valve outlet collected from CRMS. This is lower than the actual fuel supply pressure due to pressure losses in a real system.
Figure 32. Effect of increasing fuel supply pressure on the duration of H₂ operation

As the H₂ supply pressure increased measured at the regulator, the fuel valve outlet pressure did not increase proportionally. The internal fuel supply system is predicted to have choked the flow, preventing higher pressures, velocities, and volumetric flow rates necessary to sustain combustion in the C30. This concern is readdressed in the Recommendations section of Chapter V.
V. CONCLUSION AND FUTURE WORK

This thesis set out to operate a COTS microturbine on H₂. This goal was achieved, albeit for a short period of time. This research approached the challenges of increasing energy resilience using H₂ using the Capstone C30 MicroTurbine. Following baseline testing with natural gas and C₃H₈, a H₂ fuel supply system was designed, developed, and implemented. The CRMS aided data collection and enabled safe remote operation of the C30. This research demonstrated that a COTS microturbine can operate using H₂, indicating its role in a larger hydrogen energy storage and generation system and a future hydrogen economy.

A. DISCUSSION OF RESULTS

In conclusion, the C30 demonstrates an ability to operate on H₂ instead of light hydrocarbons such as natural gas or C₃H₈. Figures 30 and 31 show that the C30 starts up with H₂ following the same procedure and trends as with natural gas and C₃H₈. However, combustion was not sustained. Each of three test runs caused a fault and automatic shutdown in succession. The TET rose with each test run, culminating on the third run with a TET comparable in magnitude to the steady-state operating TET of natural gas and C₃H₈. Due to the short runtimes, the steady-state operating TET of H₂ is not known; however, it is predicted to be very similar to natural gas and C₃H₈ because the TET and engine speed are set operating parameters within the C30 based on load.

B. RECOMMENDATIONS

Following the results of the CFD simulations, analysis of the materials used in the C30’s combustion chamber is strongly recommended. Although the TET appears to be a set point, the temperature inside the combustion chamber is not measured and the effects of combusting H₂ within it are unknown. Any effects did not preclude the C30 from operating normally using C₃H₈ six days after the H₂ test runs.

The H₂ fuel supply system should be redesigned to provide greater volumetric flow rates and the ability to control the flow rate. The design may be a limiting factor in the
operation of the C30 during this research. Other limiting factors include the design of the internal fuel supply system within the C30 causing choked flow or the fuel nozzle design inside the combustion chamber.

Incorporating a resistor bank to test the C30 at full power is strongly recommended. The increased fuel demand may stabilize the flame in the combustion chamber, especially for operation with C₃H₈.

C. FUTURE WORK

The next stage of this research should first incorporate a resistor bank to test the C30 at full power and compare results to this research. Next, future work might focus on constructing an improved H₂ fuel supply system, capable of greater volumetric flow rates and containing more instrumentation in the form of flow meters, pressure gauges, and thermocouples or focus on improving the internal design of the C30’s fuel nozzles and combustion chamber. Instrumentation could be added to the combustion chamber or combustion chamber outlet of the C30, especially if changing components within the chamber. Collecting data from the combustion chamber while operating with H₂ at steady-state operation would provide more information to improve the technology of a future hydrogen economy.
APPENDIX A. FUEL INLET VELOCITY CALCULATION

For an inversely proportional relationship between fuel inlet velocity and mass air-fuel ratio, it can be shown that:

\[ MAF = \frac{k}{v} \]

Where \( v \) is the fuel inlet velocity, \( k \) is a constant, and \( MAF \) is the mass air-fuel ratio. Substituting simulation values for \( v \) and \( MAF \) and averaging the calculated \( k \) values:

\[ k = 11300 \]

Calculating the mass air-fuel ratio twice that of the stoichiometric mass air-fuel ratio for H \(_2\) [12]:

\[ MAF = 2 \times \Phi_{H_2} = 2 \times 34.3 = 68.6 \]

Substituting and calculating for \( v \):

\[ v = \frac{k}{MAF} = \frac{11300}{68.6} = 165 \left[ \frac{m}{s} \right] \]
APPENDIX B. CFD COMBUSTION SIMULATION DATA

A. PROPANE-AIR COMBUSTION

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<td>0.0059932</td>
<td>0.0689049</td>
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B. METHANE-AIR COMBUSTION

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C. HYDROGEN-AIR COMBUSTION

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<td>0.00844978</td>
<td>68.43</td>
<td>1.995</td>
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</table>
APPENDIX C. CFD COMBUSTION SIMULATION IMAGE

ANSYS CFX produces temperature scales from the minimum to the maximum temperatures calculated. The scales, visible in on the left-hand side of each figure, vary with each scenario.

A. PROPANE-AIR COMBUSTION

Temperature inside the combustion chamber (propane-air reaction, 40 m/s)
B. METHANE-AIR COMBUSTION

Temperature inside the combustion chamber (methane-air reaction, 40 m/s)
C. HYDROGEN-AIR COMBUSTION

Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 10 m/s)
Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 15 m/s)
Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 20 m/s)
Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 25 m/s)
Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 30 m/s)
Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 35 m/s)
Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 40 m/s)
Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 45 m/s)
Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 50 m/s)
Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 55 m/s)
Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 60 m/s)
Temperature inside the combustion chamber (H₂-air reaction, inlet velocity 165 m/s)
## APPENDIX D. GASTURB INPUT AND OUTPUT DECKS

### A. NATURAL GAS INPUTS

<table>
<thead>
<tr>
<th>Basic Data</th>
<th>Air System</th>
<th>Comp Efficiency</th>
<th>Comp Design</th>
<th>Turb Efficiency</th>
<th>Tip Clear.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Heat Exchanger</td>
<td>Exhaust Loss</td>
<td>Application</td>
<td>Steam Cooling</td>
<td>Water/Steam</td>
<td></td>
</tr>
</tbody>
</table>

#### Fuel:
- **Natural Gas**

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Unit</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Total Temperature T1</td>
<td>K</td>
<td>268.15</td>
</tr>
<tr>
<td>Total Pressure P1</td>
<td>kPa</td>
<td>101.325</td>
</tr>
<tr>
<td>Ambient Pressure Pamb</td>
<td>kPa</td>
<td>101.325</td>
</tr>
<tr>
<td>Relative Humidity (%)</td>
<td></td>
<td>0</td>
</tr>
<tr>
<td>Inlet Corr. Flow W2Rstd</td>
<td>kg/s</td>
<td>0.30745</td>
</tr>
<tr>
<td>Intake Pressure Ratio</td>
<td></td>
<td>0.99</td>
</tr>
<tr>
<td>Pressure Ratio</td>
<td></td>
<td>3.39</td>
</tr>
<tr>
<td>Burner Exit Temperature</td>
<td>K</td>
<td>1132</td>
</tr>
<tr>
<td>Burner Design Efficiency</td>
<td></td>
<td>0.9999</td>
</tr>
<tr>
<td>Burner Partload Constant</td>
<td></td>
<td>1.6</td>
</tr>
<tr>
<td>Fuel Heating Value</td>
<td>MJ/kg</td>
<td>49.7365</td>
</tr>
<tr>
<td>Overboard Bled</td>
<td>kg/s</td>
<td>0</td>
</tr>
<tr>
<td>Mechanical Efficiency</td>
<td></td>
<td>0.9785</td>
</tr>
<tr>
<td>Burner Pressure Ratio</td>
<td></td>
<td>0.98</td>
</tr>
<tr>
<td>Turbine Exit Duct Press Ratio</td>
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</tr>
<tr>
<td>Design Exhaust Pressure Ratio</td>
<td></td>
<td>1.03</td>
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</table>

**Basic data inputs (natural gas, SI units)**

<table>
<thead>
<tr>
<th>Basic Data</th>
<th>Air System</th>
<th>Comp Efficiency</th>
<th>Comp Design</th>
<th>Turb Efficiency</th>
<th>Tip Clear.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Heat Exchanger</td>
<td>Exhaust Loss</td>
<td>Application</td>
<td>Steam Cooling</td>
<td>Water/Steam</td>
<td></td>
</tr>
</tbody>
</table>

#### Fuel:
- **Natural Gas**

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Unit</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Heat Exchanger Effectiveness</td>
<td>0.8</td>
<td></td>
</tr>
<tr>
<td>Heat Exchanger Design P3/P3</td>
<td></td>
<td>0.99</td>
</tr>
<tr>
<td>Heat Exchanger Design P7/P7</td>
<td></td>
<td>0.9</td>
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**Heat exchanger data inputs (natural gas, SI units)**
Air system data inputs (natural gas, SI units)

Compressor efficiency data inputs (natural gas, SI units)
Compressor design data inputs (natural gas, SI units)

<table>
<thead>
<tr>
<th>Basic Data</th>
<th>Air System</th>
<th>Comp Efficiency</th>
<th>Comp Design</th>
<th>Turb Efficiency</th>
<th>Tip Clear</th>
</tr>
</thead>
<tbody>
<tr>
<td>Fuel:</td>
<td>Natural Gas</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

- **Compressor Tip Speed**: m/s | 350
- **Compressor Inlet Radius Ratio**: 0.5
- **Compressor Inlet Mach Number**: 0.54
- **Engine Infl/Compr Tip Diam Ratio**: 1
- **min Compr Inlet Hub Diameter**: m

Turbine efficiency data inputs (natural gas, SI units)

- **Isentropic Turbine Efficiency**: 0.8655
## B. NATURAL GAS OUTPUTS

### Summary of outputs (natural gas, SI units)

<table>
<thead>
<tr>
<th>Station</th>
<th>W</th>
<th>T</th>
<th>P</th>
<th>WR std</th>
<th>PWSD</th>
<th>FSFC</th>
<th>Heat Rate</th>
<th>Thrm Eff</th>
</tr>
</thead>
<tbody>
<tr>
<td>amb</td>
<td>0.304</td>
<td>288.15</td>
<td>101.325</td>
<td>0.307</td>
<td>28.4 kW</td>
<td>0.2877 kg/(kW*h)</td>
<td>14308.2 kW/(kW*h)</td>
<td>0.256</td>
</tr>
<tr>
<td>1</td>
<td>0.304</td>
<td>288.15</td>
<td>101.325</td>
<td>0.307</td>
<td>28.4 kW</td>
<td>0.2877 kg/(kW*h)</td>
<td>14308.2 kW/(kW*h)</td>
<td>0.256</td>
</tr>
<tr>
<td>2</td>
<td>0.301</td>
<td>439.90</td>
<td>340.057</td>
<td>0.112</td>
<td>28.4 kW</td>
<td>0.2877 kg/(kW*h)</td>
<td>14308.2 kW/(kW*h)</td>
<td>0.256</td>
</tr>
<tr>
<td>3</td>
<td>0.301</td>
<td>439.90</td>
<td>340.057</td>
<td>0.112</td>
<td>28.4 kW</td>
<td>0.2877 kg/(kW*h)</td>
<td>14308.2 kW/(kW*h)</td>
<td>0.256</td>
</tr>
<tr>
<td>4</td>
<td>0.298</td>
<td>589.38</td>
<td>336.656</td>
<td>0.352</td>
<td>28.4 kW</td>
<td>0.2877 kg/(kW*h)</td>
<td>14308.2 kW/(kW*h)</td>
<td>0.256</td>
</tr>
<tr>
<td>5</td>
<td>0.304</td>
<td>912.38</td>
<td>118.327</td>
<td>0.464</td>
<td>28.4 kW</td>
<td>0.2877 kg/(kW*h)</td>
<td>14308.2 kW/(kW*h)</td>
<td>0.256</td>
</tr>
<tr>
<td>6</td>
<td>0.304</td>
<td>912.38</td>
<td>118.327</td>
<td>0.464</td>
<td>28.4 kW</td>
<td>0.2877 kg/(kW*h)</td>
<td>14308.2 kW/(kW*h)</td>
<td>0.256</td>
</tr>
<tr>
<td>7</td>
<td>0.304</td>
<td>549.39</td>
<td>104.365</td>
<td>0.403</td>
<td>28.4 kW</td>
<td>0.2877 kg/(kW*h)</td>
<td>14308.2 kW/(kW*h)</td>
<td>0.256</td>
</tr>
<tr>
<td>8</td>
<td>0.304</td>
<td>549.39</td>
<td>104.365</td>
<td>0.403</td>
<td>28.4 kW</td>
<td>0.2877 kg/(kW*h)</td>
<td>14308.2 kW/(kW*h)</td>
<td>0.256</td>
</tr>
</tbody>
</table>

### Compressor data outputs (natural gas, SI units)

<table>
<thead>
<tr>
<th>Summary</th>
<th>Compressor</th>
<th>Air System</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input:</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Compressor Tip Speed</td>
<td>m/s</td>
<td>350.00000</td>
</tr>
<tr>
<td>Compressor Inlet Radius Ratio</td>
<td></td>
<td>0.50000</td>
</tr>
<tr>
<td>Compressor Inlet Mach Number</td>
<td></td>
<td>0.54000</td>
</tr>
<tr>
<td>Engine Inl/Compr Tip Diam Ratio</td>
<td></td>
<td>1.00000</td>
</tr>
<tr>
<td>min Compr Inlet Hub Diameter</td>
<td>m</td>
<td>0.00000</td>
</tr>
<tr>
<td>Output:</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Compressor Tip circumsf. Mach No</td>
<td></td>
<td>1.05803</td>
</tr>
<tr>
<td>Compressor Tip relative Mach No</td>
<td></td>
<td>1.13757</td>
</tr>
<tr>
<td>Design Spool Speed</td>
<td>[RPM]</td>
<td>127511.63</td>
</tr>
<tr>
<td>Compr Inlet Tip Diameter</td>
<td>m</td>
<td>0.05242</td>
</tr>
<tr>
<td>Compr Inlet Hub Diameter</td>
<td>m</td>
<td>0.02621</td>
</tr>
<tr>
<td>Calculated Compr Radius Ratio</td>
<td></td>
<td>0.50000</td>
</tr>
<tr>
<td>Aerodynamic Interface Plane</td>
<td>m²</td>
<td>0.00216</td>
</tr>
<tr>
<td>Corr.Flow/Area Compr</td>
<td>kg/(s²m²)</td>
<td>189.92577</td>
</tr>
</tbody>
</table>
Air system outputs (natural gas, SI units)
Enthalpy-entropy diagram (natural gas, SI units)
Shaft power delivered-power specific fuel consumption diagram
(natural gas, SI units)
C. HYDROGEN INPUTS

Basic data inputs (H₂, SI units)

Heat exchanger data inputs (H₂, SI units)
### Air system data inputs (H₂, SI units)

<table>
<thead>
<tr>
<th>Basic Data</th>
<th>Air System</th>
<th>Comp Efficiency</th>
<th>Comp Design</th>
<th>Steam Cooling</th>
<th>Turb Efficiency</th>
<th>Tip Clear</th>
</tr>
</thead>
<tbody>
<tr>
<td>Rel. Handling Bleed</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Rel. Enthalpy of Handling Bleed</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Rel. Overboard Bleed W Bld/W2</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Rel. Enthalpy of Overb. Bleed</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Recirculating Bleed W rec/W2</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Rel. Enthalpy of Recirc Bleed</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>NGV Cooling Air W Cl NG/V/W2</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Rotor Cooling Air W Cl/W2</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Cooling Air Pumping Diameter</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

### Compressor efficiency data inputs (H₂, SI units)

<table>
<thead>
<tr>
<th>Basic Data</th>
<th>Air System</th>
<th>Comp Efficiency</th>
<th>Comp Design</th>
<th>Steam Cooling</th>
<th>Turb Efficiency</th>
<th>Tip Clear</th>
</tr>
</thead>
<tbody>
<tr>
<td>Fuel: Hydrogen</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Isentropic Compr. Efficiency</td>
<td>0.787</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

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Compressor design data inputs (H₂, SI units)

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Compressor Tip Speed</td>
<td>350 m/s</td>
</tr>
<tr>
<td>Compressor Inlet Radius Ratio</td>
<td>0.5</td>
</tr>
<tr>
<td>Compressor Inlet Mach Number</td>
<td>0.54</td>
</tr>
<tr>
<td>Engine Inh/Compr Tip Diam Ratio</td>
<td>1</td>
</tr>
<tr>
<td>min Compr Inlet Hub Diameter</td>
<td>0</td>
</tr>
</tbody>
</table>

Turbine efficiency data inputs (H₂, SI units)

<table>
<thead>
<tr>
<th>Efficiency Type</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Isentropic Turbine Efficiency</td>
<td>0.8555</td>
</tr>
</tbody>
</table>
### D. HYDROGEN OUTPUTS

#### Summary of outputs (H₂, SI units)

<table>
<thead>
<tr>
<th>Station</th>
<th>W (kg/s)</th>
<th>T (K)</th>
<th>P (kPa)</th>
<th>WRstd (kg/s)</th>
<th>PWSD (kW)</th>
</tr>
</thead>
<tbody>
<tr>
<td>amb</td>
<td>0.304</td>
<td>288.15</td>
<td>101.325</td>
<td>0.307</td>
<td>29.0</td>
</tr>
</tbody>
</table>

**Compressor data outputs (H₂, SI units):**

- PSFC: 0.1135 kg/(kW*h)
- Heat Rate: 14029.1 kJ/(kW*h)

**Spool mech Eff:** 0.5785

**Nom Spd:** 12751.11 rpm

<table>
<thead>
<tr>
<th>Summary: Compressor Air System</th>
</tr>
</thead>
</table>

### Summary: Compressor Air System

**Input:**
- Compressor Tip Speed: 350.00000 m/s
- Compressor Inlet Radius Ratio: 0.50000
- Compressor Inlet Mach Number: 0.34000
- Engine Inl/Compr Tip Diam Ratio: 1.00000
- min Compr Inlet Hub Diameter: 0.00000

**Output:**
- Compressor Tip circumfl. Mach No: 1.05803
- Compressor Tip relative Mach No: 1.18707
- Design Spool Speed: 127511.03 RPM
- Compr Inlet Tip Diameter: 0.05242
- Compr Inlet Hub Diameter: 0.02521
- Calculated Compr Radius Ratio: 0.50000
- Aerodynamic Interface Plane: 0.00216
- Corr Flow/Area Compr: 189.92399 kg/(s*m²)
Air system outputs (H₂, SI units)
Enthalpy-entropy diagram (H₂, SI units)

Shaft power delivered-power specific fuel consumption diagram (H₂, SI units)
APPENDIX E. PROCEDURE FOR OPERATING WITH HYDROGEN

1. Verify that there are no leaks and that no power is supplied to the solenoid valves.

2. Move the battery isolation switch to the ON position, accessible via the panel labeled “BATTERY CIRCUIT BREAKER ACCESS SWITCH” [14].

3. Press the “BATT START” button (accessible via the control panel, labeled with the Capstone logo) to wake the C30 from sleep mode [14].

4. Verify that the C30 is configured for Stand Alone Operation. If not already in Stand Alone Operation Mode, configure the C30 as described in chapter 3 of reference [14] and in reference [16].

5. Start the CRMS software, previously installed on a laptop with a RS-232 serial port [17].

6. Connect the computer to the C30 and establish communications. Open the Communications Bay to access the User Connection Board and the User Port (J6) in accordance with section 2.1, User Interface [14]. Connect the computer’ RS-232 serial port to the C30 RS-232 serial port using a null modem cable. Attempts to extend the cable by connecting it in series with another modem cable are not recommended.

7. Select the “Display” tab from the options bar in the “Unit_1” window. Select “Strip Chart.”

8. Once the chart labelled “Microturbine Chart, Unit_1” appears, select the desired parameters from the drop down menus. No more than four parameters are recommended to avoid visual clutter unless specifically required for real-time observation. All parameters will have data collected and may be charted/graphed later. The recommended parameters are “Turbine Exit Temperature,” “Battery SOC,” “Compressor Inlet Temperature”, and “Engine Speed” for a no-load run. Adjust the number of points to cover the expected runtime of the turbine. Beneath each parameter, select the upper and lower bounds. The y-axis ranges from 0 to 1, with each parameter
being charted as a decimal percentage of its upper bound [17]. Recommend zero to above maximum value achieved. Avoid setting expected values such that multiple parameters chart at similar values (i.e., 0.8 for both TET and Bat SOC).

9. Select “Control Mode” from the mode drop-down menu. If prompted for a password, enter the default user port user password <USR123P> or the selected user port user password [17].

10. Select the save/”File Manager” button in the top ribbon. The toggle button “Recording” should be set to manual within the “Data Recording” pane. Click the radio button “Start Recording” within the same pane; when it appears green and says “ON,” close the window. The file location may also be changed to user preference.

11. Manually open the H₂ tank valve and the manual shutoff valve.

12. Adjust the regulator to the desired fuel supply pressure.

13. Evacuate the area. (One of the test cells at the TPL was used to provide a safe barrier between the C30 and the user in the event of uncontrolled combustion.)

14. Open solenoid valve 1 remotely.

15. Open solenoid valve 2 remotely and vent for 2-4 seconds to flush the supply system with H₂ and reduce the chance of flashback.


17. Click “START” under “Turbine Start” and allow the C30 to start up and run [17].

18. Observe data collection/conduct experiment.

19. Click “STOP” under “Turbine Start” and allow the C30 to run its shutdown procedure. In the event of an automatic shutdown and an error message, allow the C30 to safely stop on its own [17].

20. Verify that the C30 has stopped.


22. Vent the remaining H₂ in the supply line by actuating solenoid valve 2 remotely.
23. Close the manual shutoff valve and the H₂ tank valve.

24. Turn off the control panel by moving the battery isolation switch into the OFF position, accessible via the panel labeled “BATTERY CIRCUIT BREAKER ACCESS SWITCH” [14].

25. Save the collected data and disconnect the computer from the C30.
APPENDIX F. FUEL HEATING VALUES

Using the ideal gas law, a fuel’s molar mass, and a fuel’s heating value on a per unit mass basis, the fuel’s heating value per unit volume was calculated. H₂ requires a volume flow rate over three times that of natural gas to provide the same thermal energy at a constant pressure and temperature.

\[
pV = nRT \\
\frac{p}{RT} = \frac{n \cdot MM}{V} \\
\rho = \frac{p}{RT} \\
HHV_{vol} = \frac{HHV_{mass}}{\rho} \\
HHV_{vol} = HHV_{mass} \cdot \frac{RT}{\rho}
\]

<table>
<thead>
<tr>
<th>Molar Mass [g/mol]</th>
<th>HHV [kJ/kg] [12]</th>
<th>LHV [kJ/kg] [12]</th>
<th>Density at 20°C, 379 kPa</th>
<th>HHV [kJ/m³]</th>
<th>LHV[kJ/m³]</th>
</tr>
</thead>
<tbody>
<tr>
<td>2.016 (H₂)</td>
<td>141781</td>
<td>119953</td>
<td>0.3138</td>
<td>44492</td>
<td>37642</td>
</tr>
<tr>
<td>16.043 (CH₄)</td>
<td>55496</td>
<td>50010</td>
<td>2.497</td>
<td>138578</td>
<td>124879</td>
</tr>
<tr>
<td>44.094 (C₃H₈)</td>
<td>50343</td>
<td>46352</td>
<td>6.862</td>
<td>345471</td>
<td>218084</td>
</tr>
</tbody>
</table>
LIST OF REFERENCES


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1. Defense Technical Information Center
   Ft. Belvoir, Virginia

2. Dudley Knox Library
   Naval Postgraduate School
   Monterey, California